## Access Management Plan <br> US-36 Corridor

## Marysville, Kansas

August 2018 - FINAL REPORT
KDOT Project Number: 36-58 KA-4386-01


## ACKNOWLEDGEMENTS

## CITY OF MARYSVILLE

Carla Grund: Mayor
Austin St. John: City Administrator
Gina Graham: Council Member (Ward I)
Bobbi Pippia: Council Member (Ward I)
Terry Hughes: Council Member (Ward II)
Darlene Boss: Council Member (Ward II)
Jason Barnes: Council Member (Ward III)
Kevin Throm: Council Member (Ward III)
Todd Frye: Council Member (Ward IV)
Diane Schroller: Council Member (Ward IV)
David Richardson: Planning \& Zoning Administrator

# KANSAS DEPARTMENT OF TRANSPORTATION 

Nelda A. Buckley, P.E.: Special Projects Engineer
Leroy Koehn, P.E.: District One Engineer
Mark Karolevitz, P.E.: Area Five Engineer

## BG CONSULTANTS

Jason Hoskinson, P.E., PTOE: Vice President
Matthew Kohls, P.E.: Principal
Diane Rosebaugh, P.E.: Design Engineer
Dylan Medlock, I.E.: Design Engineer
A special thank you needs to be extended to all of the citizens, business owners, special interest groups, City Council Members, and KDOT staff providing invaluable input that helped shape the recommendations in this report.

## TABLE OF CONTENTS

## Contents

Acknowledgements ..... 1
City of Marysville ..... 1
Kansas Department of Transportation ..... 1
BG Consultants ..... 1
Table of Contents ..... 2
Executive Summary ..... 6
Purpose ..... 6
Public Involvement ..... 6
Access Management ..... 6
Traffic Analysis and Recommendations ..... 6
Short-Term Recommendations ..... 7
Development Driven/Continual Recommendations ..... 7
Long-Term Recommendations. ..... 10
CHAPTER 1: Introduction ..... 11
1.1 Corridor Location ..... 11
1.2 Study Limits ..... 11
1.3 Boundary Limits ..... 12
1.4 Existing Typical Sections ..... 12
CHAPTER 2: Public Involvement ..... 15
2.1 Public Involvement Summary ..... 15
2.2 Stakeholder Agency Coordination ..... 15
2.3 Business, Land Owner and Developer Group Input ..... 16
2.4 Public Input ..... 16
CHAPTER 3: KDOT's Access Management Policy ..... 19
3.1 Route Classification ..... 19
3.2 Area Type ..... 19
3.3 Route Access Control Designation. ..... 20
3.4 Access Point Location Considerations ..... 21
3.4.1 Intersection Influence Areas ..... 21
3.4.2 Access Spacing (Unsignalized and Signalized) ..... 26
3.4.3 Sight Distance (Stopping and Intersection) ..... 32
CHAPTER 4: Traffic Analysis ..... 34
4.1 Regional Growth Rates ..... 34
4.2 Traffic Operations (Existing Conditions) ..... 36
4.3 Traffic Volumes (Existing) ..... 37
4.4 Traffic Analysis Summary ..... 40
4.5 Pedestrian/Bicycle Accommodations ..... 41
4.5.1 Pedestrian Accommodations ..... 41
4.5.2 Bicycle Accommodations ..... 43
4.6 Crash Data ..... 43
4.7 Traffic Signal Analysis ..... 46
4.7.1 KDOT's Road Safety Audit Results ..... 46
4.7.2 US-36 and $8^{\text {th }}$ Street ..... 47
CHAPTER 5: Transportation Recommendations ..... 49
5.1 Access Management ..... 49
5.2 Geometric Improvements ..... 51
5.2.1 US-36 Between $4^{\text {th }}$ and 5th Streets ..... 51
5.2.2 US-36 and 7th Street ..... 51
5.2.3 US-36 and US-77 (10th Street) ..... 52
5.2.4 US-36 and 11th Road ..... 53
5.2.5 US-36 and 11th Drive ..... 54
5.2.6 US-36 and 11th Terrace ..... 55
5.2.7 US-36 and Wal-Mart Entrance/"Street A" ..... 56
5.2.8 US-36 and $12^{\text {th }}$ Road ..... 57
5.2.9 US-36 and $12^{\text {th }}$ Terrace/"Street B" ..... 58
5.2.10 US-36 and 13th Road ..... 59
5.3 Traffic Signals ..... 60
5.4 Pedestrian/Bicycle Facilities ..... 60
5.4.1 Pedestrian Facilities ..... 60
5.4.2 Bicycle Facilities ..... 60
CHAPTER 6: Implementation ..... 64
Appendix A - Public Involvement ..... 65
Appendix B - Calculations ..... 66
Appendix C - Synchro Models ..... 69
List of Figures
Figure 1: Recommended Improvements Location Map ..... 8
Figure 2: Corridor Location ..... 11
Figure 3: Study Area ..... 11
Figure 4: City of Marysville Zoning Map ..... 13
Figure 5: Long-term Street Classification Map ..... 14
Figure 6: Area Type ..... 20
Figure 7: Intersection Influence Area Diagram (Source: KDOT's Access Management Policy, Figure 4-16) ..... 22
Figure 8: Intersection Functional Lengths (Source: KDOT's Access Management Policy,
Figure 4-17) ..... 22
Figure 9: Intersection Influence Areas (1 of 3) ..... 23
Figure 10: Intersection Influence Areas (2 of 3) ..... 24
Figure 11: Intersection Influence Areas (3 of 3) ..... 25
Figure 12: US-36 Corridor Speed Limits ..... 26
Figure 13: Long-term Access Changes (1 of 3) ..... 28
Figure 14: Long-term Access Changes (2 of 3) ..... 29
Figure 15: Long-term Access Changes (3 of 3) ..... 30
Figure 16: AADT Traffic Flow (Source: KanPlan) ..... 35
Figure 17: Existing Intersection Configuration ..... 37
Figure 18: Peak Hour Turning Movements ..... 39
Figure 19: Right-in/Right-out Access (Source: KDOT's Access Management's Policy) ..... 50
Figure 20: Three-quarter Access (Source: KDOT's Access Management Policy) ..... 50
Figure 21: Proposed Improvements along US-36 between $4^{\text {th }}$ and $5^{\text {th }}$ Streets ..... 51
Figure 22: US-36 and $7^{\text {th }}$ Street Proposed Improvements ..... 51
Figure 23: US-36 and US-77 (10 ${ }^{\text {th }}$ Street) Proposed Improvements ..... 52
Figure 24: US-36 and $11^{\text {th }}$ Road Proposed Improvements ..... 53
Figure 25: US-36 and $11^{\text {th }}$ Drive Proposed Improvements ..... 54
Figure 26: US-36 and $11^{\text {th }}$ Terrace Proposed Improvements ..... 55
Figure 27: US-36 and Wal-Mart Entrance ("Street A") Proposed Improvements ..... 56
Figure 28: US-36 and $12^{\text {th }}$ Road Proposed Improvements ..... 57
Figure 29: US-36 and $12^{\text {th }}$ Terrace ("Street B") Proposed Improvements ..... 58
Figure 30: US-36 and $13^{\text {th }}$ Road Proposed Improvements ..... 59
Figure 31: Pedestrian Infrastructure (1 of 3) ..... 61
Figure 32: Pedestrian Infrastructure (2 of 3) ..... 62
Figure 33: Pedestrian Infrastructure (3 of 3) ..... 63
List of Tables
Table 1: Corner Clearance Distances (Source: KDOT's Access Management Policy) ..... 26
Table 2: Unsignalized Access Spacing ..... 27
Table 3: Signalized Access Spacing. ..... 32
Table 4: Existing Signal Cycles and Spacing ..... 32
Table 5: Stopping Sight Distance on Level Terrain (Source: KDOT's Access Management Policy) ..... 33
Table 6: Stopping Sight Distance on Grades (Source: KDOT's Access Management Policy)33
Table 7: Level of Service Criteria ..... 34
Table 8: AM Peak LOS (Existing Operating Conditions) ..... 40
Table 9: PM Peak LOS (Existing Operating Conditions) ..... 40
Table 10: US-36 Corridor Characteristics (Source: KDOT's RSA, 2013) ..... 44
Table 11: US-36 Intersection Characteristics (Source: KDOT's RSA, 2013) ..... 45
Table 12: Traffic Signal Warrant Analysis (from KDOT's RSA, 2013) ..... 47
Table 13: Traffic Signal Warrant Analysis (US-36 \& $8^{\text {th }}$ Street) ..... 48
Table 14: US-36 and 8 ${ }^{\text {th }}$ Street Synchro Analysis ..... 48
Table 15: US-36 and $11^{\text {th }}$ Road LOS ..... 53

## EXECUTIVE SUMMARY

## PURPOSE

Marysville, Kansas has experienced steady urban growth over the last 100 years. This access management plan is intended to assist the City in making informed growth decisions along the US-36 corridor over the next 20 years. By analyzing existing traffic patterns, the Level of Service (LOS) for various intersections, existing crash patterns, current location of traffic signals, current access control and public input, the following represents corridor strategies and recommendations to improve the public's travel experience and reduce congestion.

## PUBLIC INVOLVEMENT

Public outreach and public involvement is a vital part of involving stakeholders, developers and property owners, special interest groups, and governmental entities into the decisionmaking process and was a critical part of developing this access management plan.

The following is a list of key stakeholders who were involved with the process:

- City of Marysville government
- Marshall County officials
- Various Businesses and Property Owners

Public involvement efforts included the following approach:

- Focused agency stakeholder meetings
- Focused land owner and business meetings
- Public open houses
- Plan summary presentations to the Plan Partners


## ACCESS MANAGEMENT

Planning for future growth requires an understanding of the existing property access along the US-36 corridor. The existing corridor was examined by comparing the existing conditions to the requirements as defined by The Kansas Depart of Transportation's (KDOT's) Access Management Policy. Both short-term and long-term recommendations are included in this plan to help improve traffic movement, reduce crashes, and better manage vehicle conflict points.

## TRAFFIC ANALYSIS AND RECOMMENDATIONS

Having a good understanding of supply versus demand for a given transportation facility also helps shape the proposed recommendations. Demand for a given facility is quantified through traffic flow or traffic volumes. The US-36 corridor was analyzed by reviewing the existing and future estimated Level-of-Service (LOS) at intersections where traffic volume data was available. LOS assigns the facility a grade between A (good) and F (poor) depending on capacity and performance. The existing US-36 corridor is operating at an LOS A or B. With an expected growth of $1.5 \%$ per year for the Central Business District and
3.0\% per year for the developed region east of the Central Business District over the next 20 years, the LOS service for the facility is expected to operate between an LOS A and C.

The following is a summary of the recommendations of this access management plan. The recommendations are classified into three categories: Short-Term, Development Driven/Continual, and Long-Term Recommendations. Each of them are explained in greater detail throughout the report. Refer to Figure 1: Recommended Improvements Location Map to see a general overview of where the improvements are located. Note that KanPlan's 2016 AADT (Annual Average Daily Traffic) was included for quick reference only.

## SHORT-TERM RECOMMENDATIONS

- Signal Upgrades: Video Detection and Accessible Pedestrian Signal upgrades at all existing signals (except at $20^{\text {th }}$ Street).
- US-36 \& $7^{\text {th }}$ Street Geometric Improvements: Geometric improvements at $7^{\text {th }}$ Street to allow for better vehicular movement while maintaining access radii to accommodate larger turning vehicles. Extend the shared-use path along $7^{\text {th }}$ Street to the north.
- US-36 \& US-77 (10 ${ }^{\text {th }}$ Street) Geometric Improvements: Consider a property acquisition in the southeast corner of US-36 and US-77 (10 ${ }^{\text {th }}$ Street) to improve sight lines, turning movements and storage length.
- US-36 \& 11 $1^{\text {th }}$ Road Geometric Improvements: Signalize the intersection, add eastbound and westbound right-turn lanes on US-36, and add both northbound and southbound dedicated left- and right-turn lanes on $11^{\text {th }}$ Road.
- Pedestrian Facilities: Provide pedestrian facilities on the north side of US-36 from $20^{\text {th }}$ Street to $11^{\text {th }}$ Road.
- Existing Pedestrian Facility Upgrades: Replace old and deteriorating sections of sidewalk along the US-36 corridor.


## DEVELOPMENT DRIVEN/CONTINUAL RECOMMENDATIONS

- Access Consolidations/Closures:
- Access closures/consolidations along the US-36 corridor as properties change owners and businesses change types.
- Restripe the "Central Business District" to include more on-street parking as accesses are consolidated/closed.
- Long-term Street Network Upgrades:
- It is assumed that all "Arterial" and "Collector" streets will be constructed with at least 3 -lane sections approaching the highway and all "Local" streets will be constructed as 2-lane sections (unless noted otherwise).
- $20^{\text {th }}$ Street: Between US-36 and Spring Street/Keystone Road
- Existing roadway does not exist
- Future "Arterial" street
- $11^{\text {th }}$ Road: Between Jayhawk Road and Keystone Road
- Existing roadway is a 2-lane section with partial bicycle facilities
- Future "Arterial" street
- To be constructed as a 3-lane section with on-street bicycle lanes


LEGEND
-Existing Arterial Street - Existing Collector Street ---Future Arterial Street ---Future Collector Stree Fruture Local Street (3) Proposed Traffic Signal Existing Traffic Signal

RECOMMENDED
PROJ ECTS
Short-Term:
1: 7th Street Geometric
D. \#2. mprovements

Geometric
Improvements
I.D. \#3: 11th Road Geometric

Improvements
Long-Term:
.D. \#4: 4th to 5th Streets Geometric
Improvements
D. \#5: 12th Road Geometric
D. Improvements
.D. \#6: 13th Road Geometric Improvements

Other Projects:
Access Consolidations and
Closures

- City Street Netw ork

Upgrades

- Existing Signal Upgrades
- Pedestrian Facility Upgrades
- Sidew alk Gaps
- $11^{\text {th }}$ Drive: Between North Street and Keystone Road
- Existing roadway is a partially constructed, 2-lane, private drive north of US-36
- Future "Local" street between North Street and Juniper Road and between "Street C" and Keystone Road
- Future "Collector" street between Juniper Road and "Street C"
- $11^{\text {th }}$ Terrace: Between North Street and Keystone Road
- Existing roadway does not exist
- Future "Collector" street
- "Street A": Between US-36 and Keystone Road
- Existing roadway does not exist
- Future "Collector" street between US-36 and "Street C"
- Future "Local" street between "Street C" and Keystone Road
- $12^{\text {th }}$ Road: Between Jayhawk Road and Keystone Road
- Existing roadway is a 2-lane section
- Future "Arterial" street
- "Street B": Between Jayhawk Road and Limestone Road
- Existing roadway does not exist
- Future "Collector" street
- $13^{\text {th }}$ Road: Between Jayhawk Road and Limestone Road
- Existing roadway is a 2-lane section
- Future "Arterial" street
- Jayhawk Road: Between $11^{\text {th }}$ Road and $13^{\text {th }}$ Road
- Existing roadway is a 2-lane section
- Future "Arterial" street
- North Road: Between $20^{\text {th }}$ Street and $13^{\text {th }}$ Road
- Existing roadway is a 2 -lane section between $20^{\text {th }}$ Street and $11^{\text {th }}$ Road and does not exist between $11^{\text {th }}$ Road and $13^{\text {th }}$ Road
- Future "Collector" street
- To be constructed as a 3-lane section with on-street bicycle lanes between $20^{\text {th }}$ Street and $11^{\text {th }}$ Road
- Juniper Road: Between 20 ${ }^{\text {th }}$ Street and North Street
- Existing roadway does not exist
- Future "Local" street
- "Street C": Between Spring Street and $12^{\text {th }}$ Road
- Existing roadway does not exist
- Future "Local" street
- Keystone Road: Between $20^{\text {th }}$ Street and $12^{\text {th }}$ Road
- Existing roadway is a 2-lane section
- Future "Arterial" street
- "Street D": Between $12^{\text {th }}$ Road and $13^{\text {th }}$ Road
- Existing roadway does not exist
- Future "Collector" street
- Limestone Road: Between $12^{\text {th }}$ Road and $13^{\text {th }}$ Road
- Existing roadway is a 2-lane section
- Future "Arterial" street


## LONG-TERM RECOMMENDATIONS

- Sidewalk Gap Project: New sidewalk is recommended on the south side of US-36 from N. $11^{\text {th }}$ Street to $N .20^{\text {th }}$ Street.
- US-36 Geometric Improvements between $4^{\text {th }}$ and $5^{\text {th }}$ Streets: Extend the three-lane section west to $4^{\text {th }}$ Street (accesses should be closed to accommodate the street widening).
- US-36 \& $11^{\text {th }}$ Drive Geometric Improvements: Once development occurs, build $11^{\text {th }}$ Drive to meet US-36, modify pavement markings on US-36 to add dedicated left-turn lanes, and add both northbound and southbound dedicated left-turn lanes on $11^{\text {th }}$ Drive.
- US-36 \& $11^{\text {th }}$ Terrace Geometric Improvements Once development occurs, build $11^{\text {th }}$ Terrace to meet US-36, add eastbound and westbound right- and left-turn lanes on US-36, and add both northbound and southbound dedicated left -turn lanes on $11^{\text {th }}$ Terrace.
- US-36 \& Walmart Geometric Improvements: Once development occurs, build "Street $A^{\prime \prime}$ to meet US-36, modify pavement markings on US-36 to add dedicated left-turn lanes, and add northbound dedicated left-turn lanes on "Street A".
- US-36 \& $12^{\text {th }}$ Road Geometric Improvements: Once signal warrants are met at US36 and $12^{\text {th }}$ Road, signalize the intersection, add eastbound and westbound right-turn lanes on US-36, and add both northbound and southbound dedicated left- and rightturn lanes on $11^{\text {th }}$ Road.
- US-36 \& 12 ${ }^{\text {th }}$ Terrace ("Street B") Geometric Improvements: Once development occurs, build $12^{\text {th }}$ Terrace ("Street B") to meet US-36, add eastbound and westbound right- and left-turn lanes on US-36, and add both northbound and southbound dedicated left- and right-turn lanes on $12^{\text {th }}$ Terrace ("Street B").
- US-36 \& $13^{\text {th }}$ Road Geometric Improvements: Once signal warrants are met at US36 and $13^{\text {th }}$ Road, signalize the intersection, add eastbound and westbound right-turn lanes on US-36, and add both northbound and southbound dedicated left- and rightturn lanes on $11^{\text {th }}$ Road.

For clarification, it is worth noting that " $11^{\text {th }}$ Drive" is sometimes labeled " $11^{\text {th }}$ Terrace" when using web-based maps. The street signs located in the field reflect how the streets are labelled within this report.

## CHAPTER 1: INTRODUCTION

### 1.1 CORRIDOR LOCATION

Marysville, Kansas is located in Marshall County in the north-central portion of the state. US-36 highway runs east/west through the center of town and US-77 highway runs northsouth following on US-36 for about one mile through town. See Figure 2: Corridor Location for project location.


Figure 2: Corridor Location

### 1.2 STUDY LIMITS

The limits of the study area include US-36 highway from $4^{\text {th }}$ Street to $13^{\text {th }}$ Road. Figure 3: Study Area shows the limits of the study area as outlined in the red shading.


Figure 3: Study Area

### 1.3 BOUNDARY LIMITS

Also important to the further development of the US-36 corridor is the future development of Marysville. The City of Marysville provided a zoning map which was created in 2013 and is shown in Figure 4: City of Marysville Zoning Map. A long-term street classification map was established by comparing the zoning map to the recommendations from the "20052025 Comprehensive Plan" for the City of Marysville. Figure 5: Long-term Street Classification Map shows these street classifications.

In general, the hierarchy of roads moves people from the smaller 'local streets' (which provide property access) to the midrange 'collector streets' to the larger 'arterial streets' and highways where more focus is given to mobility rather than property access. The intersection of arterial roadways may be good places to install signals (if warranted).

Figure 5: Long-term Street Classification Map shows US-36, US-77 and $20^{\text {th }}$ Street as existing arterial streets. As the area develops, $11^{\text {th }}$ Road, $12^{\text {th }}$ Road, $13^{\text {th }}$ Road, Jayhawk Road, Keystone Road, and Limestone Road should all be considered arterial streets. $8^{\text {th }}$ Street (north of US-36) and North Street (west of $16^{\text {th }}$ Street) have been identified as existing collector streets. In the future, North Street (east of $20^{\text {th }}$ Street), "Street D", $11^{\text {th }}$ Drive, $11^{\text {th }}$ Terrace, "Street A" (north of "Street C"), and "Street B" should be considered future collector streets. Juniper Road, "Street C", $11^{\text {th }}$ Drive (south of "Street C"), and "Street A" (south of "Street C ") should be considered future local streets.

Figure 5: Long-term Street Classification Map also shows the approximate AADT (as identified by KDOT's 2017 Traffic Flow Map), the location of existing signals, and the proposed location of future signals (which will be discussed in detail later in this report).

### 1.4 EXISTING TYPICAL SECTIONS

The typical section along US-36 varies through the study limits. In general, the downtown region consists of a three lane section (an eastbound driving lane, and westbound driving lane, and a two-way left-turn or dedicated left-turn lane) with on-street parallel parking. The driving lanes and central turn lane are approximately 12 ft . wide with an approximate 9 ft . wide parallel parking region for a total street width of approximately 54 ft . The curb and gutter section that is consistent through downtown gives way to shoulders and open ditches just east of $20^{\text {th }}$ Street. A center turn-lane is present for some of but not all of the region from $20^{\text {th }}$ Street to $13^{\text {th }}$ Road. In this section, the driving lanes and center turn lane (where present) are approximately 12 ft . wide and the shoulders are approximately 8 ft . wide. Sidewalks are inconsistent along the study corridor and are described in greater detail later in this report.


Figure 4: City of Marysville Zoning Map


## CHAPTER 2: PUBLIC INVOLVEMENT

### 2.1 PUBLIC INVOLVEMENT SUMMARY

A critical path to developing this corridor plan included reaching out to the public and getting the public involved. Getting stakeholders and community members on the same page helps create partnerships, can strengthen the community, encourages understanding of the plan needs and requirements, builds trust and helps reduce the likelihood of future conflicts. The exchange of ideas and sharing of information helps build public consensus and develops a more successful plan.

The following is a list of key stakeholders who were involved with the process:

- City of Marysville government
- Marshall County officials
- Various Businesses and Property Owners

Public involvement efforts included the following approach:

- Focused agency stakeholder meetings
- Focused land owner and business meetings
- Public open houses
- Plan summary presentations to the Plan Partners

The following core messages were developed and shared with the community about this plan:

- KDOT and the City of Marysville have partnered to develop a plan that recommends future improvements to better handle traffic demands and supports future economic growth in the area.
- The need for access consolidation/closures will help improve traffic movement, reduce crashes, and create fewer vehicle conflict points.
- The corridor has significant future development possibilities (particularly on the east end) that have the potential to increase traffic volume along US-36.


### 2.2 STAKEHOLDER AGENCY COORDINATION

Several progress meetings were held throughout the development of this plan. Progress meetings were held with BG Consultants, Marysville City Staff and governing bodies, and KDOT Staff. Meetings were held on:

- December 6 $6^{\text {th }}, 2016$
- September $5^{\text {th }}, 2017$
- November 20 ${ }^{\text {th }}, 2017$
- December $14^{\text {th }}, 2017$ - Marysville Planning Commission
- December $27^{\text {th }}, 2017$ - Marysville City Council

The objective of these meetings was to provide the stakeholders information as to how the plan was developing and for the stakeholders to provide input in the decision-making process. Comments received form these meetings assisted in identifying the analysis needs and
prioritizing key transportation improvement projects. The following list summarizes some of the key comments to come from the progress meetings:

- Majority of the turning movement counts were to come from KDOT's Road Safety Audit for Marshall County that was published in January 2013.
- BG was to collect turning movement data at the intersections of US-36 and $7^{\text {th }}$ Street, $8^{\text {th }}$ Street, and $11^{\text {th }}$ Road.
- Existing city information including zoning maps, future growth maps, crash reports, and traffic signal timing were to be provided to BG from the City of Marysville.
- Future development areas were identified south of US-36 between $11^{\text {th }}$ Road and $12^{\text {th }}$ Road as well as north of US-36 between $11^{\text {th }}$ Terrace and Walmart.
- One-on-one stakeholder meetings with local land owners and area business owners were to be coordinated through BG.
- Areas of local concern included the intersection of US-36 and $11^{\text {th }}$ Road, collector access to US-36 between $11^{\text {th }}$ Road and $12^{\text {th }}$ Road, possible future development sites, and the transload facility.


### 2.3 BUSINESS, LAND OWNER AND DEVELOPER GROUP INPUT

A number of local businesses, property owners, and development groups with interests in the study corridor were engaged through the development of this plan. The purpose of engaging these groups was to identify how the corridor is currently being used by some of the major traffic generators and to gain a better understanding of potential near term private investments that may impact the future needs of the corridor.

In addition to the public input collected in public forums, the following list of interest groups were asked to provide their experience, knowledge, and input regarding the corridor land uses and the level of transportation service provided by US-36.

- Paula Landoll - Landoll Corporation
- Valley Vet Supply
- Union Pacific Railroad
- Rob Peschel, P.S. and Tony Duever, P.E. - CES Group P.A.
- Marshall County Connection, Inc. - Blue River Rail Trail
- Ellen Barber - Marshall County Partnership for Growth


### 2.4 PUBLIC INPUT

An open house format public meeting was held on November $30^{\text {th }}, 2017$ at 6:00pm to gain valuable input from the public. A survey form was developed, and BG Staff was available to answer questions and discuss a general overview of how the access management plan was developing. The meeting was attended by eleven (11) people of which eight (8) filled out the survey. The following is a summary of the survey questions and responses:

1. "How do you feel about the existing number of driveway connections to US-36 within the Planning Area?"
(4) Too many
(4) Just right
(0) There's room for more

- One respondent commented that the number of connections is Just Right "from what I see."
- One
respondent commented that the number of connections is


2. "Do you LIKE / DISLIKE the on-street parking on US-36 between $5^{\text {th }}$ St. and $12^{\text {th }}$ St.?"
(5) Like
(2) Dislike
(1) Marked through with a question mark

- One respondent commented that they Dislike the on-street parking "because of the semis speeding nearby."

3. "Do you feel like the pedestrian/bicycle needs are being met within the Planning Area?"
(2) Yes
(6) No

The comments included:

- No - "Love to see bike trails part of the process! Would like to see more along corridor. People would like to ride, but can't."
- No - "There needs to be more pedestrian walkways."
- No - "particularly pedestrian needs"
- No - "Feel the bicycle needs are now met; I do bike and feel more than sufficient and safe. Pedestrian would be more important."
- No - "We have enough trail and bike paths."
- Yes - "It's a private thing."

4. "List the top (2) two US-36 improvements you would like to see implemented in the future:"

- The $12^{\text {th }}$ Road turning improvements.
- The $11^{\text {th }}$ Terrace road improvements with the future collector street that goes into North Street behind KanEquip to the East. This area is designated for a business park and can't develop without road infrastructure.
-     - Stop light at $11^{\text {th }}$ Road intersection.
- Bigger turning area for stop light at $10^{\text {th }}$ and Center.
-     - Get rid of $8^{\text {th }}$ St. stoplight.
- $11^{\text {th }} \mathrm{Rd}$ stoplight.
-     - Stoplight at $11^{\text {th }}$ Road.
- Buried utility lines.
-     - If a change, do not feel streets need to be widened but could limit parking along highway when possible.
-     - The $12^{\text {th }}$ Road turning improvements
- The $11^{\text {th }}$ Terrace road improvements with the future collector street that goes into North Street behind KanEquip to the East. This area is designated for a business park and can't develop without road infrastructure.
-     - Imp. $12^{\text {th }}$ Rd access to so.
- Light at $11^{\text {th }}$ Rd.
- $11^{\text {th }}$ Road south and stoplight
- Synchronize stoplights.

5. Additional comments or concerns:

- Thank you for opening this up to the public.
- Current businesses need their driveways but empty lots could be looked at.
- Remove $8^{\text {th }}$ stoplight - put stoplight at $11^{\text {th }}$ Road.
- One way turns only have to be way in the future.
- Matthew and Jason very helpful and informative

Reviewing the comments from the survey indicate the most advocated for improvement was the proposed improvements at $11^{\text {th }}$ Road, followed by $12^{\text {th }}$ Road improvements, and improvements at $11^{\text {th }}$ Terrace. Signal warrants were reviewed for the existing signal at $8^{\text {th }}$ Street as part of this study as a result of the survey.

Pictures from the public meeting are shown in Picture 1: Public Meeting at City Hall, Picture 3: Public Meeting at City Hall, and Picture 2: Public Meeting at City Hall.


Picture 3: Public Meeting at City Hall


Picture 2: Public Meeting at City Hall

## CHAPTER 3: KDOT'S ACCESS MANAGEMENT POLICY

It is important to understand key characteristics of the highway as defined by The Kansas Department of Transportation's (KDOT's) Access Management Policy to properly manage highway access.

### 3.1 ROUTE CLASSIFICATION

KDOT has developed a Route Classification System to better manage and describe the more than 10,000 state highway miles. The system classifies routes based on daily traffic, route continuity, access to major cities, trip length, and route spacing. There are five classification categories: classes A through E. Class A routes describe interstate routes that are fully access-controlled and permit high-speed travel. Class E routes are the lowest classification that describe routes that connect rural residents with other routes. They generally have low traffic volumes and fewer trucks. It is worth noting that any route that is also part of the National Highway system or a designated planned corridor, shall be analyzed as a Class B route regardless of the route classification.

According to KDOT's Access Permit Map (https://www.ksdot.org/accessmanagement/), US36 is a Class B route and part of the National Highway System through the study area. Class $B$ routes are those that are non-interstate routes with limited access, high-speed travel, long distance truck traffic and have statewide significance. US-77 is a Class C route and part of the National Highway System. Any analysis of US-77 will be based on Class B route parameters.

### 3.2 AREA TYPE

Another key aspect in determining appropriate access placement is the Area Type. KDOT has three distinct Area Types:

- Central Business District (CBD): Central Business Districts are areas that are defined by high concentration of businesses, with limited access, on-street parking, and higher volumes of pedestrian/bicycle traffic. See Picture 4: CBD IUS-36 \& 9th Street looking East along US36) for an example of the CBD within Marysville.
- Developed: Developed areas must meet one of the three following criteria: (1) within the corporate limits of a municipality, (2) the speed


Picture 4: CBD (US-36 \& $9^{\text {th }}$ Street looking East along US-36)
at least $50 \%$ of the frontages abutting the highway have been developed with residences, businesses, and/or industry for a distance of a quarter mile or more. Picture 5: Developed Area (US-36 at Pizza Hut looking West) and Picture 6: Developed Area (US-36 at Walmart looking West) show developed areas within Marysville.


Picture 5: Developed Area (US-36 at Pizza Hut looking West)


Picture 6: Developed Area (US-36 at Walmart looking West)

- Undeveloped: Undeveloped areas are those that don't meet the criteria for CBD's or Developed areas.

Multiple area types are represented throughout the corridor along US-36 and US-77 due to the length of the study area. Figure 6: Area Type summarizes these conditions.


Figure 6: Area Type

### 3.3 ROUTE ACCESS CONTROL DESIGNATION

Access control designations have been identified by KDOT to represent KDOT's vision of access control along a highway system. Access control designations range from Full Access Control (meaning access to the highway is only allowed via grade-separated interchanges) to Partial Access Control (as defined in the Access Management Policy) to No Access Control (meaning that any accesses should adhere to the access spacing criteria as found in KDOT's Access Management Policy).

US-36 is defined with a Partial Access Control 3 classification through the study area as shown in Chapter 8.4 of KDOT's Access Management Policy. This access control
designation applies to arterial highways within or approaching an urban area or rural, twolane highways that are likely to remain two-lane highways for the foreseeable future. Partial Access Control 3 routes are to be described by the following access characteristics:

- Access points should be kept to a minimum (either public roads or private entrances). New private access to the highway should not be allowed if the property has reasonable access or reasonable opportunity to gain access from a nearby, lower function roadway.
- Existing access spacing should be preserved or spacing criteria from the Access Management Policy should be used, whichever is greater.
- Existing lawful connections and median openings are not required to meet spacing criteria from the Access Management Policy. These access points will usually be allowed to remain but should be brought into conformance with the spacing criteria in the Access Management Policy when significant change occurs or as changes to the roadway allow. As design projects occur, existing access points between intersections should be removed or relocated.
- When there are existing passing lanes or passing lanes are added, access points should be limited or eliminated within the limits of the passing lane. Public roads and private entrances may need to be closed to minimize conflict points if other reasonable means of access are available.

These characteristics represent the vision KDOT would like to achieve along the US-36 corridor. Meeting this criteria, however, can often be difficult in an existing urban environment due to development patterns that have occurred prior to the implementation of KDOT's Access Management Policy.

### 3.4 ACCESS POINT LOCATION CONSIDERATIONS

### 3.4.1 INTERSECTION INFLUENCE AREAS

The intersection influence area, as defined by KDOT's Access Management Policy, contains both the physical area and functional area of an intersection as depicted in Figure 7: Intersection Influence Area Diagram (Source: KDOT's Access Management Policy, Figure 416). By defining upstream and downstream influence areas for each intersection, preferable access locations can be identified in locations outside of the defined influence areas.

Intersection influence areas are determined by defining the following distances (which are shown in Figure 8: Intersection Functional Lengths (Source: KDOT's Access Management Policy, Figure 4-17):

- $\mathrm{d}_{1}=$ distance traveled during perception reaction time
- $\mathrm{d}_{2}=$ distance traveled during deceleration when coming to a stop
- $\mathrm{d}_{3}=$ the actual queue storage length
- $d_{4}=$ downstream functional distance


Figure 7: Intersection Influence Area Diagram (Source: KDOT's Access Management Policy, Figure 4-16)


Figure 8: Intersection Functional Lengths (Source: KDOT's Access Management Policy, Figure 4-17)
Influence areas along the US-36 corridor have been estimated according to KDOT's Access Management Policy. Individual d1, d2, d3, and d4 lengths have been listed in Appendix B for each intersection along US-36 from $4^{\text {th }}$ Street to $12^{\text {th }}$ Road. The influence areas are also shown in Figure 9: Intersection Influence Areas (1 of 3), Figure 10: Intersection Influence Areas (2 of 3), and Figure 11: Intersection Influence Areas (3 of 3).

Intersection influence area calculations indicate:

- there are no available opportunities to access US-36 between $4^{\text {th }}$ Street and $15^{\text {th }}$ Street and between $17^{\text {th }}$ Street and $18^{\text {th }}$ Street.
- between $15^{\text {th }}$ Street and $17^{\text {th }}$ Street there is an opportunity for access to US-36 of about 335 ft .
- between $18^{\text {th }}$ Street and $20^{\text {th }}$ Street there is a short access window of about 200 ft .
- between $20^{\text {th }}$ Street and $11^{\text {th }}$ Road there is an opportunity for access to US-36 of about $3,300 \mathrm{ft}$.
- between $11^{\text {th }}$ Road and $11^{\text {th }}$ Drive there is an access window of about 720 ft .
- between $11^{\text {th }}$ Drive and $12^{\text {th }}$ Road there is an opportunity for access to US-36 of about 3,200ft.

INTERSECTION INFLUENCE AREAS


$\qquad$

LOCATION KEY



INTERSECTION INFLUENCE AREAS



OCATION KEY


Figure 10: Intersection Influence Areas (2 of 3)

## aghust 2018

INTERSECTION INFLUENCE AREAS



LOCATION KEY


Influence areas were considered along several of the local side streets but due to the relatively long influence areas compared to the short distances between the highway and parallel streets/alleyways, it was determined that corner clearance may be better measure to restrict local side street accesses that are nearing US-36 in some areas. It should be noted that every effort should be made to meet influence area requirements but at a minimum corner clearance can help keep new accesses from encroaching upon the highway. In developed areas, corner clearance is measured from the edge of curb line of the highway to the edge or curb line of the access. Minimum distances are shown in Table 1: Corner Clearance Distances (Source: KDOT's Access Management Policy).

Table 1: Corner Clearance Distances (Source: KDOT's Access Management Policy)

| Highway Area Type | Design Distance |
| :---: | :---: |
| [ft] |  |
| Undeveloped | 155 |
| Developed | 115 |
| CBD | 85 |

Because US-36 serves an existing, well-developed urban environment, some flexibility will need to be considered for existing access points. Further analysis of access spacing will be discussed to help identify places where existing access points can be eliminated or consolidated.

### 3.4.2 ACCESS SPACING (UNSIGNALIZED AND SIGNALIZED)

Reviewing access spacing criteria as set forth in KDOT's Access Management Policy will help establish a starting point for acceptable access locations (both entrances and side streets). The Access Management Policy identifies separate criteria for signalized and unsignalized accesses. Access spacing takes into account the route classification, area type, and the posted speed limit. Figure 12: US-36 Corridor Speed Limits shows the various speed limits throughout the US-36 corridor through Marysville.


When access is provided to properties on opposite sides of a highway, it is preferable for the driveways to be aligned across from one another. Consideration for appropriate offsets can be applied when aligning driveways cannot be achieved. KDOT's Access Management Policy outlines minimum offset distances for accesses on opposite sides of the roadway. Minimum offset distances are dependent upon access type and posted speed limit (see Table

4-9 in KDOT's Access Management Policy). Realigning offset accesses can help with safety and traffic flow issues and eliminate overlapping turning movements.

The US-36 corridor is a crowded corridor. Meeting both access spacing requirements and intersection influence areas will be challenging.

## Unsignalized Spacing

Unsignalized access spacing is shown in Table 2: Unsignalized Access Spacing. By identifying the route classification, area type and speed limit the appropriate spacing between accesses can be determined (distances between access points are measured from the centerline of one access to the centerline of another access).

Table 2: Unsignalized Access Spacing

| Access Route | Area Type | Speed Limit |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Classification |  | 30 mph | 45 mph | 50 mph | 65 mph |
| B |  | $515^{\prime}$ | $610^{\prime}$ | $955^{\prime}$ |  |
|  | Developed | $225^{\prime}$ | $450^{\prime}$ | $535^{\prime}$ | $\mathrm{n} / \mathrm{a}$ |
|  | CBD | $155^{\prime}$ | $\mathrm{n} / \mathrm{a}$ | $\mathrm{n} / \mathrm{a}$ | $\mathrm{n} / \mathrm{a}$ |

Within the Central Business District, from $4^{\text {th }}$ Street to $15^{\text {th }}$ Street, both intersection influence areas and current access spacing requirements as set forth by KDOT's Access Management Policy indicate no access should be allowed between the intersections. It is the recommendation of this report that all accesses between street intersections within the Central Business District be removed. Figure 13: Long-term Access Changes (1 of 3) shows how the corridor could look if all access points are removed. Existing access locations that are recommended to be removed or relocated are represented by blue cross-hatched regions. Pavement markings should be modified so that all left-turn lanes and two-way left-turn lanes can be maximized and on-street parking can be added from intersection to intersection. Pavement markings shown on the following figures are schematic in nature and will need to be designed to meet current Manual on Uniform Traffic Control Devices (MUTCD) standards when they are implemented, this includes but is not limited to the parking spacing, lane markings, turn lane lengths, crosswalk marking, and symbols.

From $15^{\text {th }}$ Street to $17^{\text {th }}$ Street, accesses should be limited to the region outside of the intersection influence areas with an access spacing of at least 225'. Eliminating several of the access points and allowing for shared accesses which are aligned on both sides of US36 (as shown on Figure 13: Long-term Access Changes (1 of 3)) can maintain access to current and future businesses.

From $17^{\text {th }}$ Street to $18^{\text {th }}$ Street, all accesses should be eliminated as shown on Figure 13 : Long-term Access Changes (1 of 3) and on Figure 14: Long-term Access Changes (2 of 3). A shared access should be built that aligns with $18^{\text {th }}$ Street for the businesses on the south side to have access. An example of what this shared access could look like is shown on Figure 14: Long-term Access Changes (2 of 3).


LEGEND
-Existing Arterial Street -Existing Collector Street --Future Arterial Street -- Future Collector Stree $=$ Future Local Street Consolidated/Relocated Entrance New Entrance Location Existing Pavement Improvement


OCATION KEY:


Figure 13: Long-term Access Changes (1 of 3)

LONG-TERM ACCESS CHANGES


(e) $\qquad$

LOCATION KEY


Figure 14: Long-term Access Changes (2 of 3)

## LONG-TERM ACCESS CHANGES




LOCATION KEY


Figure 15: Long-term Access Changes (3 of 3)

Between $18^{\text {th }}$ Street and $20^{\text {th }}$ Street, intersection influence areas and spacing requirements indicate there is room for only one aligned access location half way between the intersections. All other accesses should be removed. This is shown on Figure 14: Longterm Access Changes (2 of 3).

Consolidating and realigning access points will also be important between $20^{\text {th }}$ Street and $11^{\text {th }}$ Road. Accesses should be limited to outside the intersection influence areas. Within the 30 mph speed zone access spacing should be a minimum of $225^{\prime}$ and within the 45 mph speed zone spacing should be at least 450'. Possible consolidation reconfiguration for the various access locations is shown on Figure 14: Long-term Access Changes (2 of 3).

Between $11^{\text {th }}$ Road and $11^{\text {th }}$ Drive, consolidating accesses to align at the one-third points should allow accesses to remain outside of the intersection influence areas while maintaining an access spacing of greater than 450'. This will require property owners to share accesses. A possible arrangement is shown in Figure 14: Long-term Access Changes (2 of 3) and in Figure 15: Long-term Access Changes (3 of 3).

From $11^{\text {th }}$ Drive to $11^{\text {th }}$ Terrace, realigned access to the halfway point would keep them outside of the intersection influence areas and meet spacing requirements. This configuration is shown in Figure 15: Long-term Access Changes (3 of 3).

The section between $11^{\text {th }}$ Terrace and $12^{\text {th }}$ Road will be more challenging to meet access spacing requirements due to the mix of existing residential properties and existing commercial properties. It will be important to implement good access management practices and engineering judgement as properties are redeveloped. Figure 15: Long-term Access Changes (3 of 3) shows an example access layout that consolidates and realigns many of the accesses to meet the 535 ft . spacing requirement.

## Signalized Spacing

Signalized spacing, which is dependent upon the signal cycle length and the route speed limit, is shown in Table 3: Signalized Access Spacing. Where adjacent signals have different cycle lengths, it is appropriate to use the longer cycle length for analysis. Because traffic signals introduce interrupted traffic flow along the US-36 corridor, extensive delays can be avoided by synchronizing the signals. In addition, traffic signal spacing should also consider turning treatments, roadway functional classification and purpose, and adequate storage lengths for traffic queues.

The US-36 corridor has four existing intersections that are traffic signal controlled: $8^{\text {th }}$ Street, US-77 ( $10^{\text {th }}$ Street), $14^{\text {th }}$ Street, and $20^{\text {th }}$ Street. Marysville Staff provided the existing signal cycle lengths for each of these intersections. Table 4: Existing Signal Cycles and Spacing summarizes the cycle lengths for each traffic signal as well as the distance between signals. Currently, the only traffic signal controlled intersection that meets the spacing requirements set forth by KDOT's Access Management Policy is the intersection of US-36 and $20^{\text {th }}$ Street.

Table 3: Signalized Access Spacing

| Cycle Length [sec] | Speed Limit |  |  |
| :---: | :---: | :---: | :---: |
|  | 30 mph | 45 mph | 50 mph |
| 60 | 1,320 | 1,980 | 2,200 |
| 70 | 1,540 | 2,310 | 2,590 |
| 80 | 1,760 | 2,640 | 2,940 |
| 90 | 1,980 | 2,970 | 3,300 |
| 100 | 2,200 | 3,300 | 3,670 |
| 110 | 2,420 | 3,630 | 4,040 |
| 120 | 2,640 | 3,960 | 4,400 |

Table 4: Existing Signal Cycles and Spacing

| Intersection | Speed <br> Limit <br> [mph] | Min. <br> Cycle <br> Length <br> [sec] | Max. <br> Cycle <br> Length <br> [sec] | Distance <br> between <br> Signals <br> [ft] | Req'd <br> Distance <br> between <br> Signals [ft] | Meets Req'd <br> Spacing? |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: |
| US-36 \& 8 ${ }^{\text {th }}$ St. | 30 | n/a | 60 |  |  | ( |

### 3.4.3 SIGHT DISTANCE (STOPPING AND INTERSECTION)

Sight distance is an important aspect for driveway placement. Driver's need a clear view of an access from the highway to allow time to slow down or stop (stopping sight distance) if required. Driver's also need a clear view of the highway from an access in order to select an appropriate gap in traffic to cross or turn (intersection sight distance). KDOT's Access Management Policy outlines the proceed for measuring both stopping sight distance and intersection sight distance.

After a driver perceives the need to stop, stopping sight distance is the distance required for a vehicle on the highway to come to a complete stop at a comfortable deceleration rate. It is dependent upon the grade of the surrounding terrain and is calculated by adding together the perception-reaction distance and the braking distance. The perception-reaction distance is the distance traveled by a vehicle between the time the driver perceives an object that requires the driver to stop to when the driver applies the brakes. The braking distance is the distance required by a vehicle to come to a stop once the brakes have been applied. The required stopping sight distance on level terrain is shown in Table 5: Stopping Sight Distance on Level Terrain (Source: KDOT's Access Management Policy). The required stopping sight distance for uphill or downhill grades is shown in Table 6: Stopping Sight Distance on Grades (Source: KDOT's Access Management Policy).

Table 5: Stopping Sight Distance on Level Terrain (Source: KDOT's Access Management Policy)

| Posted Speed <br> $[m p h]$ | Design Distance <br> $[f t]$ |
| :---: | :---: |
| 20 | 115 |
| 25 | 155 |
| 30 | 200 |
| 35 | 250 |
| 40 | 305 |
| 45 | 360 |
| 50 | 425 |
| 55 | 495 |
| 60 | 570 |
| 65 | 645 |
| 70 | 730 |

Table 6: Stopping Sight Distance on Grades (Source: KDOT's Access Management Policy)

| Posted <br> Speed <br> [mph] | Downgrades |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $3 \%$ | $6 \%$ | $9 \%$ | $3 \%$ | $6 \%$ | $9 \%$ |
|  | 116 | 120 | 126 | 109 | 107 | 104 |
| $\mathbf{2 5}$ | 158 | 165 | 173 | 147 | 143 | 140 |
| $\mathbf{3 0}$ | 205 | 215 | 227 | 200 | 184 | 179 |
| $\mathbf{3 5}$ | 257 | 271 | 287 | 237 | 229 | 222 |
| $\mathbf{4 0}$ | 315 | 333 | 354 | 289 | 278 | 269 |
| $\mathbf{4 5}$ | 378 | 400 | 427 | 344 | 331 | 320 |
| $\mathbf{5 0}$ | 446 | 474 | 507 | 405 | 388 | 375 |
| $\mathbf{5 5}$ | 520 | 553 | 593 | 469 | 450 | 433 |
| $\mathbf{6 0}$ | 598 | 638 | 686 | 538 | 515 | 495 |
| $\mathbf{6 5}$ | 682 | 728 | 785 | 612 | 584 | 561 |
| $\mathbf{7 0}$ | 771 | 825 | 891 | 690 | 658 | 631 |

The required sight distances shown in the above tables represent the minimum sight distance that must be available for all new access points. If the distance is not available, relocation of the access needs to be evaluated.

Achieving appropriate access placement and spacing throughout the US-36 corridor will take time. There are other short-term improvements that could be implemented as an intermediate step to improve traffic movement, reduce crashes, and create fewer vehicle conflict points. These options include changing or limiting accesses to one-way entrances, restricting left-turning movements by installing right-in/right-out accesses controlled by islands or implementing a three-quarter access that uses a restrictive median island to eliminate left-turns out of an access.

It should be noted that when executing any part of this corridor plan, accesses should be designed by a professional engineer licensed to practice in the State of Kansas and all new/relocated access points will need approval through KDOT's access permitting process.

## CHAPTER 4: TRAFFIC ANALYSIS

It is important to have a good understanding of supply versus demand for a given transportation facility. In transportation engineering, demand is quantified through traffic flow or traffic volumes. Supply is characterized by the capacity of the infrastructure and the operating condition(s) describes how well the capacity serves the demand. By comparing the existing and projected traffic demands for US-36 infrastructure deficiencies, recommendations can be made to improve the operating condition of the corridor.

Analysis of the corridor was primarily focused on reviewing the existing and future expected Level-of-Service (LOS) at intersections where traffic volume data was available. The traffic analysis was based on the 2010 Highway Capacity Manual. Using performance measures like speed, traffic density, driver experienced delay, etc., the LOS assigns the facility a grade between A (good) and F (poor) depending on capacity and performance.

The LOS for at-grade intersections can be defined as a function of the average delay (in seconds per vehicle) experienced by individual drivers as shown in Table 7: Level of Service Criteria.

Table 7: Level of Service Criteria

| Level of Service (LOS) | Signalized Intersections | Unsignalized Intersections |
| :---: | :---: | :---: |
|  | $\leq 10$ | $\leq 10$ |
| B | $10-15$ | $10-15$ |
| C | $20-35$ | $15-25$ |
| D | $35-55$ | $25-35$ |
| E | $55-80$ | $35-50$ |
| F | $>80$ | $>50$ |

### 4.1 REGIONAL GROWTH RATES

KDOT's 2017 Traffic Flow Map establishes the Annual Average Daily Traffic (AADT) for traffic counts recorded in calendar year 2016 (which can be found on KDOT's Access Permit Map). This data is shown in Figure 16: AADT Traffic Flow.

The future estimated 20-year growth for through the Central Business District region east to $11^{\text {th }}$ Road, has been estimated to be $1.5 \%$ per year by comparing the existing 2016 Traffic Flow Map to those published by KDOT over the last 20 years. Because this region is heavily developed already, this growth will be mainly characterized by background traffic growth through the region. The 7,850 daily traffic volume may grow to an estimated 10,575 by 2036 and the 680 Heavy Commercial Vehicles may grow to an estimated 916 by 2036. If traffic volumes should increase beyond 15,000 vehicles per day, the criteria for on-street parking and the corridor crash data should be reevaluated. On-street, parallel parking can become more difficult for drivers to navigate at these higher traffic volumes. Between $20^{\text {th }}$ Street and $11^{\text {th }}$ Road the 10,400 daily traffic volume may grow to an estimated 14,008 by 2036 and the 640 Heavy Commercial Vehicles may grow to an estimated 863 by 2036.


Figure 16: AADT Traffic Flow (Source: KanPlan)
The 20-year estimated growth rate for the Developed region east of $11^{\text {th }}$ Road has been estimated to be 3\% per year. It is estimated that the 5,030 daily traffic volume may grow to an estimated 9,085 by 2036 and the 640 Heavy Commercial Vehicles may grow to an estimated 1,157 by 2036. This growth will be influenced by not only background traffic growth through the region but also the expected economic development in the areas identified in Marysville's future zoning map (Figure 4: City of Marysville Zoning Map). There are still a few undeveloped commercial lots between $11^{\text {th }}$ Road and $12^{\text {th }}$ Road while the region between $12^{\text {th }}$ Road and $13^{\text {th }}$ Road has yet to develop commercially. There is also a lot of space that has been dedicated to residential construction between $11^{\text {th }}$ Road and $13^{\text {th }}$ Road.

### 4.2 TRAFFIC OPERATIONS (EXISTING CONDITIONS)

Current intersection configurations are show in Figure 17: Existing Intersection Configuration.



Figure 17: Existing Intersection Configuration

### 4.3 TRAFFIC VOLUMES (EXISTING)

Existing peak hour traffic volumes at key intersections were obtained from KDOT's Road Safety Audit for Marshall County that was published in January 2013. Peak hour turning movements were collected between July 2011 and October 2011 at the intersections of $6^{\text {th }}$ Street, $8^{\text {th }}$ Street, US-77 ( $10^{\text {th }}$ Street), $11^{\text {th }}$ Street, $14^{\text {th }}$ Street, $15^{\text {th }}$ Street, $17^{\text {th }}$ Street and $20^{\text {th }}$ Street with US-36. The peak hour counts were taken between 6:00am and 8:00am and between $4: 00 \mathrm{pm}$ and $6: 00 \mathrm{pm}$. Since the traffic counts were obtained in 2011, the traffic volumes have been adjusted by using the estimated growth rates that were established previously. The intersections of $6^{\text {th }}$ Street, $8^{\text {th }}$ Street, US-77 (10 ${ }^{\text {th }}$ Street), $11^{\text {th }}$ Street and $14^{\text {th }}$ Street were adjusted from the 2011 traffic volumes to 2017 traffic volumes using an estimated growth rate of $1.5 \%$ per year. The intersections of $15^{\text {th }}$ Street, $17^{\text {th }}$ Street and $20^{\text {th }}$ Street were adjusted from the 2011 traffic volumes to 2017 traffic volumes using an estimated growth rate of $3.0 \%$ per year.

Current peak hour turning movements for the intersection of $11^{\text {th }}$ Road and US-36 were taken on September $21^{\text {st }}, 2017$ as a part of this study.

See Figure 18: Peak Hour Turning Movements for a summary of the projected 2017 and 2037 Peak Hour Volumes. Note that any information that was not available was left blank.

[PROJECTED 2017 DATA]
[PROJECTED 2037 DATA]

[PROJECTED 2017 DATA]
[PROJECTED 2037 DATA]


Figure 18: Peak Hour Turning Movements

### 4.4 TRAFFIC ANALYSIS SUMMARY

Several Synchro models were made to analyze the existing US-36 corridor using the regional growth rates, the existing traffic operating conditions, and exiting traffic volumes. A comparison can be made for how the corridor operates under 2017 traffic volumes versus 2037 traffic volumes if no improvements are made along the US-36 corridor. Table 8: AM Peak LOS (Existing Operating Conditions) compares the LOS and delay for the major intersections along US-36 during the AM Peak Hour under 2017 traffic volumes to 2037 traffic volumes.

Table 8: AM Peak LOS (Existing Operating Conditions)

| 으웅00 |  | $\stackrel{\vdots}{\stackrel{\circ}{\circ}}$ |  |  | ㅇ00000$\ddot{0}$$\ddot{3}$ |  | O$\vdots$00©33 |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | LOS | Delay | LOS | Delay | LOS | Delay | LOS | Delay | LOS | Delay |
| $8^{\text {th }} \mathrm{St}$. | Signal | 2017 | A | 9.5 | A | 9.6 | A | 8.5 | B | 13.1 | B | 11.7 |
|  |  | 2037 | B | 10.4 | B | 10.9 | A | 9.1 | B | 13.0 | B | 11.8 |
| $11^{\text {th }}$ | Stop | 2017 | - | $\bigcirc$ | A | <1 | A | <1 | B | 10.7 | B | 11.6 |
| St. |  | 2037 | $\bigcirc$ | $\bigcirc$ | A | <1 | A | <1 | B | 11.9 | B | 13.2 |
| $14^{\text {th }}$ | Signal | 2017 | A | 9.5 | A | 9.2 | A | 9.4 | B | 14.0 | B | 12.6 |
| St. |  | 2037 | B | 10.8 | B | 10.6 | B | 10.7 | B | 14.1 | B | 12.8 |
| $20^{\text {th }}$ | Signal | 2017 | A | 6.0 | A | 6.0 | A | 5.6 | n/a | n/a | A | 7.8 |
| St. |  | 2037 | A | 6.7 | A | 6.7 | A | 6.2 | n/a | n/a | A | 8.6 |
| $11^{\text {th }}$ | Stop | 2017 | A | $\bigcirc$ | A | <1 | A | <1 | B | 11.8 | B | 10.7 |
| Rd. |  | 2037 |  |  | A | <1 | A | <1 | C | 18.1 | B | 13.5 |

Table 9: PM Peak LOS (Existing Operating Conditions) compares the LOS and delay for the major intersections along US-36 during the PM Peak Hour under 2017 traffic volumes to 2037 traffic volumes.

Table 9: PM Peak LOS (Existing Operating Conditions)

| 5 <br> 0 <br> 0.0 <br> 0 <br> 0 |  | $\begin{aligned} & \text { ஃ } \\ & \stackrel{y}{\infty} \end{aligned}$ |  |  |  |  | $\begin{aligned} & \text { ס } \\ & \overline{1} \\ & 0 \\ & 0 \\ & \frac{0}{8} \\ & 3 \\ & 3 \end{aligned}$ |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | LOS | Delay | LOS | Delay | LOS | Delay | LOS | Delay | LOS | Delay |
| $6^{\text {th }} \mathrm{St}$. | Stop | 2017 | $\times$ | $3<$ | A | <1 | A | <1 | B | 14.8 | C | 18.0 |
|  |  | 2037 | > | > | A | <1 | A | 1.1 | C | 23.1 | D | 29.9 |
| $8^{\text {th }}$ St. | Signal | 2017 | A | 10.0 | A | 9.9 | B | 10.1 | A | 9.3 | B | 10.2 |
|  |  | 2037 | B | 11.3 | B | 11.2 | B | 11.8 | A | 9.4 | B | 11.2 |
| $\begin{aligned} & 10^{\mathrm{th}} \\ & \mathrm{St} . \end{aligned}$ | Signal | 2017 | B | 17.7 | B | 19.9 | B | 18.3 | B | 12.1 | B | 15.3 |
|  |  | 2037 | C | 23.4 | C | 25.7 | C | 24.3 | B | 17.5 | B | 14.8 |
| $\begin{aligned} & 14^{\text {th }} \\ & \text { St. } \end{aligned}$ | Signal | 2017 | B | 12.0 | B | 11.6 | B | 12.3 | B | 11.1 | B | 13.8 |
|  |  | 2037 | B | 16.2 | B | 15.5 | B | 17.5 | B | 11.0 | B | 14.0 |
| $\begin{aligned} & 15^{\mathrm{th}} \\ & \mathrm{St} \end{aligned}$ | Stop | 2017 | - | $\bigcirc$ | A | <1 | A | <1 | B | 14.5 | B | 13.8 |
|  |  | 2037 | $\bigcirc$ | $\bigcirc$ | A | <1 | A | <1 | C | 19.6 | C | 18.5 |
| $\begin{aligned} & 17^{\text {th }} \\ & \text { St. } \end{aligned}$ | Stop | 2017 | $\bigcirc$ | $>$ | A | <1 | A | <1 | B | 14.1 | B | 13.5 |
|  |  | 2037 | - | $\bigcirc$ | A | <1 | A | <1 | C | 18.8 | C | 16.9 |
| $\begin{aligned} & 11^{\text {th }} \\ & \text { Rd. } \end{aligned}$ | Stop | 2017 | < | $\bigcirc$ | A | <1 | A | $<1$ | B | 11.9 | B | 12.2 |
|  |  | 2037 |  | , | A | <1 | A | <1 | C | 18.1 | C | 18.5 |

A summary of the Synchro model reports have been included in Appendix C- Synchro Models.

### 4.5 PEDESTRIAN/BICYCLE ACCOMMODATIONS

The continued development of the US-36 corridor through Marysville presents challenges and opportunities for improving bicycle and pedestrian access and safety. The following section outlines the needs and solutions that will provide a roadmap for systematically integrating bicycle and pedestrian infrastructure improvements in the US-36 corridor. The following information is based on field observations, public input, and guidance from City officials. Physical and environmental constraints are incorporated as well as existing bicycle and pedestrian infrastructure and relevant design standards.

### 4.5.1 PEDESTRIAN ACCOMIMODATIONS

## General Pedestrian Accommodations

$4^{\text {th }}$ Street marks the beginning of the existing sidewalks along the US-36 corridor. The region from $4^{\text {th }}$ Street to $17^{\text {th }}$ Street experiences regular pedestrian traffic, is more populated, and has the greatest concentration of sidewalks along the corridor. The sidewalks on the north side of US-36 in this region are generally continuous with approximately 20 curb cuts and 11 intersecting streets. The quality of these sidewalks varies greatly. The sidewalks along the south side are mostly located along the backside of commercial buildings and are not as continuous - while there are significantly less curb cuts, there are still many intersecting streets and large parking lots.

The area east of $17^{\text {th }}$ Street is not as developed but does contain many commercial businesses, a golf course, and a large shopping center. Although there is a short section of sidewalks that extend along the north side of US-36 between $17^{\text {th }}$ Street and $20^{\text {th }}$ Street, very few other sidewalks extend through this region. Most pedestrians walk along the shoulder of US-36, in landscaped borders where available, or in the adjacent business parking lots. The Wal-Mart on the north side of US-36 does have a short section of sidewalk running parallel to the highway. There are no sidewalks along the south side of US-36 from $15^{\text {th }}$ Street to the Wal-Mart, approximately 1.9 miles. The potential to improve pedestrian accommodations still exists as properties are redeveloped or as public infrastructure is rehabilitated. Improvements to the corridor can be made by establishing sidewalk policies and standards and by identifying and prioritizing the sidewalk improvements that are needed.

There are a few marked crosswalks across US-36 and all of these are in areas with the highest populations, employers, service providers, and retail destinations. The following signalized intersections along US-36 through Marysville contain marked crosswalks:

- $8^{\text {th }}$ Street
- US-77 (10 ${ }^{\text {th }}$ Street)
- $14^{\text {th }}$ Street

The following intersections have marked crosswalks but are not signalized:

- $4^{\text {th }}$ Street
- $11^{\text {th }}$ Street
- $12^{\text {th }}$ Street

One area of pedestrian significance is the intersection of $7^{\text {th }}$ Street and US-36. This is a 3way intersection with traffic moving uncontrolled east/west and is stop controlled for southbound $7^{\text {th }}$ Street traffic. $7^{\text {th }}$ Street does not continue south past US-36. Instead, this area contains a public park with a statue that serves as a point of interest. This park also acts as the focal point in the City's downtown district. This area has regular pedestrian traffic and currently does not have crosswalks for pedestrians to cross US-36 - pedestrians would need to go a block east to the signalized intersection at $8^{\text {th }}$ for the nearest crosswalk.

It is important to note the plan for a multi-use trail north of US-36 - The Blue River Trail. This trail was converted from an old railroad bed as part of the Kansas Rails-to-Trails plan and extends from Jayhawk Road to the Nebraska border and beyond. Continuing this trail into the downtown area can enhance connectivity of transportation infrastructure. There is also a paved multi-use path going south from downtown toward the intersection of Jackson and $10^{\text {th }}$ Street.

## Pedestrian Gap Study at $7^{\text {th }}$ Street

A pedestrian gap study was used to determine the size and number of gaps in vehicular traffic in which a pedestrian could cross the street during peak hours at US-36 and $7^{\text {th }}$ Street. This area is of particular interest given that it is the proposed location for the Blue River Trail to connect into downtown Marysville.

On September 19 ${ }^{\text {th }}, 2017,24$ hour traffic counts were collected at $7^{\text {th }}$ Street and US-36 through the use of a video camera. The AM peak hour was determined to be between 7:15am-8:15am and the PM peak hour was determined to be between 4:30pm-5:30pm.

Using the 2010 Highway Capacity Manual the critical headway gap can be determined using Equation 19-69. The critical headway gap is the minimum amount of time that a single pedestrian needs to perceive in order to attempt a crossing. The equation is as follows:

$$
t_{c}=\frac{L}{S_{p}}+t_{s}
$$

where:
$t_{c}=$ critical headway for a single pedestrian (s)
$L=$ crosswalk length (ft)
$S_{p}=$ average pedestrian walking speed ( $\mathrm{ft} / \mathrm{s}$ ), and
$t_{s}=$ pedestrian start-up time and end clearance time (s)
US-36 is roughly 42 ft wide where $7^{\text {th }}$ Street intersects the highway. The on-street parking is observed to be about 6 ft wide. Using an assumed crosswalk length of 42 ft (street width less the on-street parking), an average pedestrian walking speed of $3.5 \mathrm{ft} / \mathrm{s}$, and a default pedestrian start-up time and end clearance time of 3s, the critical headway gap was determined to be 15 s .

The number of gaps (defined as the time duration in seconds measured between the rear bumper of one vehicle and the front bumper of a consecutive vehicle across the same point in space) were observed during both the AM Peak Hour and the PM Peak Hour. Of the 503 gaps observed during the AM Peak Hour, only 61 gaps (12\%) were observed as having an adequate amount of time for a single pedestrian to attempt a crossing. Of the 710 gaps observed during the PM Peak hour, only 79 gaps (11\%) were observed as having an adequate amount of time for a single pedestrian to attempt a crossing.

If the crosswalk length were limited 24 ft (two 12 ft lanes) through the installation of sidewalk "bulb-outs" and using the same walking speed, and end clearance time, the headway gap decreases to 10 s . This would increase the number of adequate gaps during the AM Peak hour to 115 ( $23 \%$ ) and 138 ( $14 \%$ ) adequate gaps during the PM Peak hour.

At this time, the intersection does not warrant the installation of a pedestrian-hybrid beacon. This warrant analysis, however, should be revaluated if the shared-use path/extension of Blue River Trail into downtown is completed.

Appropriate pedestrian accommodations will need to be made at the intersection of US-36 and $7^{\text {th }}$ Street at the time at which the Blue River Trail is extended to meet downtown Marysville, All accommodations should be designed to meet current Manual on Uniform Traffic Control Devices (MUTCD) standards when they are implemented.

### 4.5.2 BICYCLE ACCOMMODATIONS

Few bicycle accommodations, such as bicycle lanes, bicycle paths or bicycle routes, have been established along the US-36 study corridor. Bicyclists can ride on US-36, but few were observed doing so. Travel via bicycle on US-36 must occur primarily in the vehicular driving lanes or on shoulders, where shoulders exist, presenting an obstacle to this mode of travel for bicyclists not comfortable with travelling among a significant number of commercial vehicles and turning vehicles. The City of Marysville has implemented an on-street bike lane system on the west side of $11^{\text {th }}$ Road to the north of US-36.

## Origins and Destinations

There are many origins and destinations within and surrounding the US-36 corridor. These areas include the adjacent housing developments and apartments that feed into the corridor from adjoining streets and driveways, commercial zones such as schools, institutions, recreational facilities, major employers, and other public and private facilities that are within a short walk or bicycle ride of the corridor. Providing adequate infrastructure for all modes of travel is important to consider with improvement projects.

### 4.6 CRASH DATA

Crash data was provided through KDOT's Road Safety Audit for Marshall County (RSA) that was published in January 2013. Crash data along the US-36 corridor within the study limits are shown in Table 10: US-36 Corridor Characteristics (Source: KDOT's_RSA, 2013).

Table 10: US-36 Corridor Characteristics (Source: KDOT's RSA, 2013)

| From | To | Length (m) | Speed (mph) | Lanes | Edge of Travel (ft) | Crashes (crash/mvmi) |  |  |  | Notes |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  |  | ADT | $\begin{aligned} & \text { Crashes } \\ & (08-10) \end{aligned}$ | Rate | Critical Rate |  |
| $4^{\text {th }}$ Street | $8^{\text {th }}$ Street | 0.259 | 30 | 2 | Curb \& Gutter | 6,332 | 3 | 1.67 | 5.96 | 1,3 |
| $8^{\text {th }}$ Street | End of Parallel Parking (70ft W of $12^{\text {th }} \mathrm{St}$ ) | 0.236 | 30 | 3 | Curb \& Gutter | 7,481 | 31 | 16.04 | 5.85 | 1,4 |
| End of Parallel Parking (70ft W of $12^{\text {th }} \mathrm{St}$ ) | $15^{\text {th }}$ Street | 0.219 | 30 | 3 | Curb \& Gutter | 9,310 | 11 | 4.93 | 5.64 | 5 |
| $15^{\text {th }}$ Street | 110 ft E of $20^{\text {th }}$ Street | 0.341 | 30 | 2 | $\begin{aligned} & \text { Curb } \\ & \text { \& } \\ & \text { Gutter } \end{aligned}$ | 9,883 | 11 | 2.98 | 5.04 | 6 |
| 110 ft E of $20^{\text {th }}$ Street | 400 ft E of $20^{\text {th }}$ Street | 0.060 | 45 | 2 |  <br> Gutter | 8,910 | 3 | 5.12 | 8.47 | 7 |
| 400 ft E of $20^{\text {th }}$ Street | $\begin{aligned} & 0.35 \text { mile } E \\ & \text { of } 20^{\text {th }} \mathrm{St} . \end{aligned}$ | 0.265 | 45 | 2 | $\begin{gathered} 10 \\ \text { paved } \end{gathered}$ | 8,910 | 1 | 0.39 | 5.44 | 8 |
| $\begin{aligned} & 0.35 \text { mile } \mathrm{E} \\ & \text { of } 20^{\text {th }} \\ & \text { Street } \end{aligned}$ | 185 ft W of Marysville Christian Fellowship Church Ent. | 0.715 | 45 | 3 | 10 paved | 7,458 | 8 | 1.37 | 4.62 | 9 |
| 185 ft W of Marysville Christian Fellowship Church Ent. | $12^{\text {th }}$ Road | 0.672 | 50 | 3 | 10 paved | 5,670 | 2 | 0.48 | 4.91 | 10 |
| $12^{\text {th }}$ Road | ECL Maryville | 0.066 | 50 | 2 | $\begin{gathered} 10 \\ \text { paved } \end{gathered}$ | 4,950 | 3 | 8.39 | 10.28 | 11 |

Notes:

1. Curb \& Gutter with parallel parking on both sides of the road.
2. Not used.
3. The crashes included 1 rear-end, 1 angle, and 1 pedestrian.
4. The crashes included 4 angle, 2 backed into, 18 rear-end, 3 sideswipe (same direction), 2 parked vehicle, 1 pedestrian and 1 fixed object.
5. The crashes included 1 animal ( $9 \%$ ), 3 angle, 6 rear-3nd, and 1 fixed object.
6. The crashes included 1 animal ( $9 \%$ ), 2 angle, 2 sideswipe (opposite), 5 rear-end, and 1 fixed object.
7. The crashes included 3 animal ( $100 \%$ ) crashes.
8. 1 fixed object crash.
9. The crashes included 1 animal ( $13 \%$ ), 4 angle, 2 rear-end, and 1 sideswipe (opposite).
10. The crashes included 1 animal ( $50 \%$ ) and 1 sideswipe (same direction).
11. The crashes included 2 animal ( $67 \%$ ) and 1 angle.

The Kansas Department of Transportation publishes five-year statistics for crash data on both public roadways and highways. The five-year (2012-2016) crash rate for urban, 2lane, undivided highways with partial access control was found to be 1.516. The five-year (2012-2016) crash rate for urban, 2-lane, undivided highways with no access control was found to be 2.218. The average crash rate for rural and urban intersections is 5 and 10,
respectively. These numbers represent the statewide average crash rate as the number of crashes per 1,000,000 vehicle miles.

Crash data along for intersections along the US-36 corridor within the study limits are shown in Table 11: US-36 Intersection Characteristics (Source: KDOT's RSA, 2013).

Table 11: US-36 Intersection Characteristics (Source: KDOT's RSA, 2013)

| Intersection | Signing |  | Crashes (crash/mvmi) |  |  |  | Notes |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | North Leg | South Leg | ADT | Crashes (08-10) | Rate | Critical Rate |  |
| $4^{\text {th }}$ Street | R1-1 | R1-1 | 5,702 | 0 | 0.00 | 18.64 | 1 |
| $5^{\text {th }}$ Street | R1-1 | R1-1 | 6,152 | 0 | 0.00 | 18.29 | 2 |
| $6^{\text {th }}$ Street | R1-1 | R1-1 | 8,508 | 0 | 0.00 | 16.96 |  |
| $7^{\text {th }}$ Street | R1-1 |  | 6,581 | 0 | 0.00 | 18.00 | 3 |
| $8^{\text {th }}$ Street | Traffic Signal |  | 12,889 | 2 | 1.42 | 15.57 |  |
| $9^{\text {th }}$ Street | R1-1 | R1-1 | 5,892 | 2 | 3.10 | 18.49 | 4 |
| $10^{\text {th }}$ St/US-77 | Traffic Signal |  | 16,085 | 17 | 9.65 | 14.95 |  |
| $11^{\text {th }}$ Street | R1-1 | R1-1 | 7,872 | 3 | 3.48 | 17.26 |  |
| $12^{\text {th }}$ Street | R1-1 | R1-1 | 9,352 | 2 | 1.95 | 16.61 |  |
| $13^{\text {th }}$ Street | R1-1 | R1-1 | 9,352 | 0 | 0.00 | 16.61 |  |
| $14^{\text {th }}$ Street | Traffic Signal |  | 17,083 | 2 | 1.07 | 14.80 |  |
| $15^{\text {th }}$ Street | R1-1 | R1-1 | 12,324 | 4 | 2.96 | 15.71 |  |
| $17^{\text {th }}$ Street | R1-1 | R1-1 | 12,096 | 1 | 0.75 | 15.76 |  |
| Masonic Temple Entrance |  | R1-1 | 10,100 | 0 | 0.00 | 16.35 |  |
| $19^{\text {th }}$ Street | R1-1 |  | 10,121 | 1 | 0.90 | 16.34 |  |
| 20 ${ }^{\text {th }}$ Street | R1-1 |  | 15,390 | 0 | 0.00 | 15.07 | 5 |
| $11^{\text {th }}$ Road | R1-1 | R1-1 | 14,539 | 5 | 3.14 | 15.23 |  |
| Walmart Ent. | R1-1 |  | 12,053 | 1 | 0.76 | 15.77 |  |
| $12^{\text {th }}$ Road | $\begin{aligned} & \text { R1-1 } \\ & \text { W3-1 } \end{aligned}$ | R1-1 W3-1 <br> (worded) | 6,070 | 2 | 3.01 | 18.35 |  |
| Notes: <br> 1. Pedestrian crossing on <br> 2. Parallel parking on the <br> 3. $\quad 7^{\text {th }}$ Street is very wide was no traffic control the correct travel path roadway. The city was entity (the city or railroad has only installed a temp Pacific Railroad to det traffic control devices <br> 4. TWLTL starts here and <br> 5. Right and left turn lane | t leg of ulder st to the stop sig It was sked to still ow rary st ne the ded at th tinue $20^{\text {th }}$ | tersection and cont oval of rai at the inte o observe tall a stop the prope sign. Disc rect own intersection. to $15^{\text {th }}$ St t. | th signs es to the ad tracks ction or that veh ign at th that th sions ha hip of th <br> t. | marking st to $11^{\text {th }}$ d at field vement m s were b ocation a ailroad tra been star property | resent. eet. <br> ew it ngs to park due to were with to de | bserved ide guid the mid usion as ved from the city the a | at there e as to of the which the city Union ropriate |

The critical crash rate, as shown in the tables, is a function of the average crash rate, the traffic volume, and a desired level of confidence. The critical crash rate can be used to determine whether an intersection or roadway segment is experiencing a number of crashes that are above the statistical range of crashes that could occur. This generally is an indicator of potential safety concerns for a given region.

An area of potential concern along US-36 highway is the region between $8^{\text {th }}$ Street and the End of the Parallel Parking (70ft west of $12^{\text {th }}$ Street). Comparing the data between Table

10 and Table 11 it is suspected that majority of the reported 31 crashes are happening at the intersection of US-36 and $10^{\text {th }}$ Street/US-77. Recommendations for this intersection are presented later in this report. Crash rates along all other regions with the study area are below the critical crash rate and are comparable to the average crash rates within the state of Kansas.

### 4.7 TRAFFIC SIGNAL ANALYSIS

The Manual on Uniform Traffic Control Devices (MUTCD) establishes criteria for traffic signal installation based on traffic conditions, pedestrian characteristics, and physical characteristics. Nine warrants are included in the MUTCD in which a traffic signal may improve the traffic operations at an intersection. A traffic signal should not be installed unless1 or more of these warrants is satisfied. Also, satisfaction of one or more of the 9 traffic signal warrants shall not in itself require the installation of a traffic control signal.

- Warrant 1, Eight-Hour Vehicular Volume
- Warrant 2, Four-Hour Vehicular Volume
- Warrant 3, Peak Hour
- Warrant 4, Pedestrian Volume
- Warrant 5, School Crossing
- Warrant 6, Coordinated Signal System
- Warrant 7, Crash Experience
- Warrant 8, Roadway Network
- Warrant 9, Intersection Near a Grade Crossing


### 4.7.1 KDOT'S ROAD SAFETY AUDIT RESULTS

Traffic signal warrant analyses were performed as part of KDOT's Road Safety Audit for Marshall County (RSA) that was published in January 2013. The 2013 RSA evaluated traffic signal warrants for the intersections of US-36 and $6^{\text {th }}$ Street, $8^{\text {th }}$ Street, US-77 (10 ${ }^{\text {th }}$ Street), $11^{\text {th }}$ Street, $14^{\text {th }}$ Street, $20^{\text {th }}$ Street, the Wal-Mart Entrance, and at $11^{\text {th }}$ Road.

Table 12: Traffic Signal Warrant Analysis (from KDOT's RSA, 2013) shows the results from the traffic warrant analysis.

The following recommendations regarding traffic signals along US-36 were included in the 2013 RSA:

- Reduced signal warrant criteria were satisfied at the intersections of US-36 and $20^{\text {th }}$ Street, $11^{\text {th }}$ Road, and the Wal-Mart entrance. However, the crash rates are below the statewide average and the intersections appears to be operating safely, BTST is not recommending installation of signals at these locations at this time.
- Long-term Recommendation:
- Based on the results of the data, the city might consider the following for future signal prioritization, provided it fits within city plans:

1. US-36 and $11^{\text {th }}$ Road (has most number of crashes and meets most warranting criteria based on volume among the 3 intersections)
2. US-36 and Wal-Mart Entrance ( $2^{\text {nd }}$ in volume warranting criteria)
3. US-36 and $20^{\text {th }}$ Street (resubmit Geometric Improvement (GI) and include signal system with next GI opportunity)**
**At the time of this study, a geometric improvement project had already been completed at this intersection based on the recommendations from the RSA.

Table 12: Traffic Signal Warrant Analysis (from KDOT's RSA, 2013)

| Location | Date | Signal Warrants Satisfied (Yes/No) and Hours Met |  |  |  |  | Notes |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | 1A | 1B | 1 Combined | 2 | 3 |  |
| $6^{\text {th }}$ <br> Street | 2/6/2007 | No, 0 hours | No, 3 hours | No, 3 hours (Condition A) and 7 hours (Condition B) | No, 1 <br> hour | No, 0 hours |  |
| $8^{\text {th }}$ <br> Street | 8/17/2011 | No, 2 <br> hours | No, 7 <br> hours | No, 7 hours (Condition A) and 12 hours (Condition B) | No, 2 <br> hours | No, 0 hours | 1, 3 |
| $\begin{gathered} \text { US-77 } \\ \left(10^{\text {th }} \text { St. }\right) \end{gathered}$ | 8/17/2011 | Yes, 12 hours | Yes, 12 hours | Yes, 12 hours (Condition A) and 12 hours (Condition B) | Yes, 12 hours | Yes, 4 hours | 1 |
| $\begin{aligned} & 11^{\text {th }} \\ & \text { Street } \end{aligned}$ | 2/7/2007 | No, 0 hours | No, 0 hours | No, O hours (Condition A) and 2 hours (Condition B) | No, 0 hours | No, 0 hours |  |
| $\begin{aligned} & 14^{\text {th }} \\ & \text { Street } \end{aligned}$ | 8/17/2011 | No, 0 hours | No, 5 hours | No, O hours (Condition A) and 7 hours (Condition B) | No, 1 hour | No, 0 hours | 1, 4 |
| $\begin{aligned} & 20^{\mathrm{th}} \\ & \text { Street } \end{aligned}$ | 8/10/2011 | No, 2 <br> hours | Yes, 9 hours | No, 6 hours (Condition A) and 12 hours (Condition B) | Yes, 7 hours | Yes, 2 hours | 2, 5 |
| Wal- <br> Mart <br> Entrance | 8/10/2011 | Yes, 9 hours | No, 1 hour | Yes, 11 hours (Condition A) and 8 hours (Condition B) | Yes, 8 hours | Yes, 2 hours | 2 |
| $\begin{aligned} & 11^{\text {th }} \\ & \text { Road } \end{aligned}$ | 10/27/2011 | Yes, 11 hours | Yes, 9 hours | Yes, 13 hours (Condition A) and 12 hours (Condition B) | Yes, 8 hours | Yes, 2 hours | 2 |
| Notes: <br> 1. Existing <br> 2. Signal satisfie <br> 3. Warran <br> 4. Installed <br> 5. Has bee | Signal <br> Warrant Criteria <br> criteria close in past for sc n installed sin | Satisfied <br> being sa <br> ol/pedest <br> the $R S A$ | for vehic <br> sfied ians was publis | ar volumes, however, warra | 7 (cra | experi | is not |

### 4.7.2 US-36 AND $8^{\text {TH }}$ STREET

An updated traffic signal warrant analysis was performed at US-36 and $8^{\text {th }}$ Street after receiving public input during the public involvement stages of this study. The results are shown below in Table 13: Traffic Signal Warrant Analysis (US-36 \& 8th Street).

Table 13: Traffic Signal Warrant Analysis (US-36 \& 8 ${ }^{\text {th }}$ Street)

| Location | Date | Signal Warrants Satisfied (Yes/No) |  |  |  |  | Notes |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | 1A | 1B | 1 Combined | 2 | 3 |  |
| $\begin{gathered} 8^{\text {th }} \\ \text { Street } \end{gathered}$ | 8/17/2011 | No | No | No | No | n/a | 1 |
| Notes: <br> 1. Existing Signal |  |  |  |  |  |  |  |

The intersection of US-36 and $8^{\text {th }}$ Street currently does not meet signal warrant criteria based solely on traffic volume. A Synchro analysis was also performed to compare LOS and expected delay at the intersection if the existing signals were removed and replaced with stop signs on $8^{\text {th }}$ Street (keeping US-36 free flowing). The results of the analysis are shown in Table 14: US-36 and 8th Street Synchro Analysis.

Table 14: US-36 and $8^{\text {th }}$ Street Synchro Analysis

|  |  | $\stackrel{\text { じ }}{\stackrel{1}{\star}}$ |  |  |  |  | 0000033 |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | LOS | Delay | LOS | Delay | LOS | Delay | LOS | Delay | LOS | Delay |
| AM | Signal | 2017 | A | 9.5 | A | 9.6 | A | 8.5 | B | 13.1 | B | 11.7 |
| Peak |  | 2037 | B | 10.4 | B | 10.9 | A | 9.1 | B | 13.0 | B | 11.8 |
| PM | Signal | 2017 | A | 10.0 | A | 9.9 | B | 10.1 | A | 9.3 | B | 10.2 |
| Peak |  | 2037 | B | 11.3 | B | 11.2 | B | 11.8 | A | 9.4 | B | 11.2 |
| AM | Stop | 2017 | - | - | A | <1 | A | <1 | B | 11.7 | B | 11.6 |
| Peak |  | 2037 | - | $\bigcirc$ | A | <1 | A | <1 | B | 13.2 | B | 13.3 |
| PM Peak | Stop | 2017 | - | $\bigcirc$ | A | $<1$ | A | <1 | B | 13.1 | B | 13.9 |
|  |  | 2037 | > | - | A | <1 | A | <1 | C | 17.3 | C | 20.0 |

A preliminary analysis of replacing the existing signal at US-36 and $8^{\text {th }}$ Street with stop signs on $8^{\text {th }}$ Street would indicate that the intersection would still operate at a LOS A or LOS B as it currently does with a LOS C along the side street by 2037. The delay experienced by drivers on US-36 would greatly decrease with the removal of the signal and stay the same or increase on $8^{\text {th }}$ Street. Replacing the signal with stop signs is one option to improve the current delay experienced by drivers on US-36. If the existing traffic signal remains in operation, installing a vehicle detection system is an option to improve the efficiency of the intersection and reduce delay experienced by drivers.

## CHAPTER 5: TRANSPORTATION RECOMMENDATIONS

### 5.1 ACCESS MANAGEMENT

The following recommendations are provided based on the analysis included in this study. The recommendations are made as a general guideline to be implemented where possible for new and existing accesses.

- Within the Central Business District, from 4th Street to 15 th Street, all accesses between street intersections within the Central Business District be removed. Pavement markings should be modified so that all left-turn lanes and two-way leftturn lanes can be maximized and on-street parking is added from intersection to intersection (see Figure 13: Long-term Access Changes (1 of 3)).
- From 15 th Street to 17 th Street, accesses should be limited to the region outside of the intersection influence areas with an access spacing of at least $225^{\prime}$ between access locations. Eliminating access points and creating shared access points which are aligned on both sides of US-36 will be key to ensuring current and future businesses still have access to the highway.
- From 17 th Street to 18 th Street, all accesses should be eliminated. A shared access should be built that aligns with 18th Street for the businesses on the south side to have access.
- Between 18th Street and 20th Street, intersection influence areas and spacing requirements would indicate there is room for only one aligned access location half way between the intersections. All other accesses should be removed.
- Consolidating and realigning accesses points will be key between 20th Street and 11 th Road. Accesses should be limited to outside the intersection influence areas. Within the 30 mph speed zone access spacing should be a minimum of $225^{\prime}$ and within the 45 mph speed zone spacing should be at least 450'.
- Between 11th Road and 11th Drive, consolidating accesses to align at the one-third points should allow accesses to remain outside of the intersection influence areas while maintaining an access spacing of greater than 450'. This will require property owners to share accesses.
- From 11th Drive to 11 th Terrace, accesses should be realigned at the halfway point.
- The section between 11th Terrace and 12th Road will be more challenging to meet access spacing requirements due to the mix of existing residential properties and commercial properties. An example layout that consolidates and realigns many of the access points to meet the required 535 ' spacing was shown earlier in this report.

Due to relatively consistent truck traffic along the US-36 corridor, all new driving and turn lanes should be designed to a $12^{\prime}$ width to accommodate a WB-67 truck.

Achieving appropriate access spacing throughout the US-36 corridor will take time. There are other short-term improvements that could be implemented as an intermediate step to improve traffic movement, reduce crashes, and create fewer vehicle conflict points. These options include:

- Changing or limiting accesses to one-way entrances
- Restricting left-turning movements by installing right-in/right-out accesses controlled by islands (as shown in Figure 19: Right-in/Right-out Access (Source: KDOT's Access Management's Policy))


Figure 19: Right-in/Right-out Access (Source: KDOT's Access Management's Policy)

- Implementing a three-quarter access (as shown in Figure 20: Three-quarter Access (Source: KDOT's Access Management Policy)) that uses a restrictive median island to eliminate left-turns out of an access.


Figure 20: Three-quarter Access (Source: KDOT's Access Management Policy)
It should be noted that when executing any part of this corridor plan, accesses should be designed by licensed engineer. Accesses will need to be designed taking into account intersection sight distance, stopping sight distance, pavement thickness, access width and radii, etc.

### 5.2 GEOMETRIC IMPROVEMENTS

Several areas have been identified along the US-36 corridor that are in need of various levels of geometric improvements. These areas/intersections include US-36 between $4^{\text {th }}$ and $5^{\text {th }}$ Streets, $7^{\text {th }}$ Street, US-77 ( $10^{\text {th }}$ Street), $11^{\text {th }}$ Road, $11^{\text {th }}$ Drive, $11^{\text {th }}$ Terrace, Wal-Mart Entrance, $12^{\text {th }}$ Road, $12^{\text {th }}$ Terrace, and $13^{\text {th }}$ Road.

### 5.2.1 US-36 BETWEEN $4{ }^{\text {TH }}$ AND 5TH STREETS



Figure 21: Proposed Improvements along US-36 between $4^{\text {th }}$ and $5^{\text {th }}$ Streets
Marysville Central Business District should be extended to include the segment of road between $4^{\text {th }}$ and $5^{\text {th }}$ Streets along US-36. This will require the extension of the existing three lane section west to $4^{\text {th }}$ Street. Accesses should be removed and on-street parking should be included. Figure 21: Proposed Improvements along US-36 between 4th and 5th Streets shows these improvements.

Estimated Cost of Improvements: \$300,000

### 5.2.2 US-36 AND 7TH STREET



Figure 22: US-36 and $7^{\text {th }}$ Street Proposed Improvements
$7^{\text {th }}$ Street has been identified as a possible truck route for large turning vehicles. $7^{\text {th }}$ Street should be reconfigured so as limit the street width for non-commercial vehicles while making use of decorative concrete aprons to allow for the turning movements of larger commercial vehicles. The multi-use path from downtown could be extended to the north to provide a
link to the Blue River Trail at the time of construction. Accommodations for pedestrians will need to be considered if the rail trail is to be extension is built. Nearby accesses on US-36 should be removed and the pavement markings should be modified to extend the center twoway left-turn lanes and to include more on-street parking. $7^{\text {th }}$ Street should remain a stopcontrolled intersection. Figure 22: US-36 and 7th Street Proposed Improvements shows these improvements.

Estimated Cost of Intersection Improvements: \$550,000


Figure 23: US-36 and US-77 (10 th Street) Proposed Improvements
The intersection US-36 and $10^{\text {th }}$ Street (US-77 south of US-36) currently has very tight turning movement restrictions east of $10^{\text {th }}$ Street. Turning movements paths and left-turn storage lengths could be greatly improved by acquiring the property in the southeast corner. The removal of this building would allow for better sight lines and larger corner radii. Pavement markings should be modified accordingly. Figure 23: US-36 and US-77 (10th Street) Proposed Improvements shows the location of proposed building to be acquired.

Estimated Cost of Intersection Improvements: \$850,000

### 5.2.4 US-36 AND 11TH ROAD



Figure 24: US-36 and $11^{\text {th }}$ Road Proposed Improvements
$11^{\text {th }}$ Road should be considered a future Arterial Street. $11^{\text {th }}$ Road should be constructed as a three-lane section with bicycle lanes. Once signal warrants are met the intersection should be signalized. Eastbound and westbound right-turn lanes should be added to US-36. At the intersection, $11^{\text {th }}$ Road should include both dedicated left- and right-turn lanes. Accommodations for bicycle facilities should be incorporated. Long-term accommodations should include bicycle lanes on $11^{\text {th }}$ Road. Short-term bicycle facilities should include a shared-use path and crosswalks at the intersection. Figure 24: US-36 and 11th Road Proposed Improvements shows the recommendations with the short-term bicycle accommodations.

Table 15: US-36 and $11^{\text {th }}$ Road LOS

|  | $\begin{aligned} & \text { ঈ. } \\ & \stackrel{y}{*} \end{aligned}$ |  |  |  |  | 0$\vdots$00$\stackrel{0}{8}$$\$$3 |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | LOS | Delay | LOS | Delay | LOS | Delay | LOS | Delay | LOS | Delay |
| Prior to | 2017 | $\bigcirc$ | $\bigcirc$ | A | <1 | A | <1 | B | 11.9 | B | 12.2 |
| Improvements | 2037 | $\bigcirc$ | > | A | $<1$ | A | $<1$ | C | 18.1 | C | 18.5 |
| After | 2017 | B | 14.5 | B | 15.0 | B | 15.8 | A | 6.1 | A | 7.9 |
| Improvements | 2037 | A | 9.7 | B | 10.1 | A | 8.2 | B | 13.4 | B | 16 |

Estimated Cost of Intersection Improvements: \$1,500,000

### 5.2.5 US-36 AND 11TH DRIVE



Figure 25: US-36 and $11^{\text {th }}$ Drive Proposed Improvements
$11^{\text {th }}$ Drive is to be considered a future Collector Street. $11^{\text {th }}$ Drive should be constructed as a two-lane section. The intersection should be stop-controlled on $11^{\text {th }}$ Drive. Pavement markings on US-36 highway should be modified to include left-turn lanes. Nearby accesses should be relocated and consolidated in accordance to the recommendations of this report. Figure 25: US-36 and 11th Drive Proposed Improvements shows these recommendations.

Estimated Cost of Intersection Improvements: \$650,000

### 5.2.6 US-36 AND 11TH TERRACE



Figure 26: US-36 and $11^{\text {th }}$ Terrace Proposed Improvements
$11^{\text {th }}$ Terrace is to be considered a future Collector Street and should be constructed as a 3lane section. The intersection should be stop-controlled along $11^{\text {th }}$ Terrace with dedicated left-turn lanes. US-36 should be modified to include dedicated right-turn lanes. Figure 26: US-36 and 11th Terrace Proposed Improvements shows these improvements.

Estimated Cost of Intersection Improvements: \$1,300,000

### 5.2.7 US-36 AND WAL-MART ENTRANCE/"STREET A"



Figure 27: US-36 and Wal-Mart Entrance ("Street A") Proposed Improvements
When future development drives the need for the extension of a street south of Wal-Mart, the future street, "Street A" is to be considered a future Collector Street. This street should be constructed as a three-lane section approaching US-36. The intersection should be stopcontrolled along the side street. Pavement markings on US-36 highway should be modified to include dedicated left-turn lanes. Nearby accesses should be relocated and consolidated in accordance to the recommendations of this report. Figure 27: US-36 and Wal-Mart Entrance ("Street A") Proposed Improvements shows these recommendations.

Estimated Cost of Intersection Improvements: \$400,000

### 5.2.8 US-36 AND $12^{\text {TH }}$ ROAD



Figure 28: US-36 and $12^{\text {th }}$ Road Proposed Improvements
$12^{\text {th }}$ Road should be considered a future Arterial Street. $12^{\text {th }}$ Road should be constructed as a three-lane section. Once signal warrants are met the intersection should be signalized. Eastbound and westbound right-turn lanes should be added to US-36. At the intersection, $12^{\text {th }}$ Road should include both dedicated left- and right-turn lanes. Figure 28: US-36 and 12th Road Proposed Improvements shows these recommendations.

Estimated Cost of Intersection Improvements: \$1,700,000

### 5.2.9 US-36 AND $12^{\text {TH }}$ TERRACE/"STREET B"



Figure 29: US-36 and $12^{\text {th }}$ Terrace ("Street B") Proposed Improvements
$12^{\text {th }}$ Terrace ("Street B") is to be considered a future Collector Street and should be constructed as a 3 -lane section. The intersection should be stop-controlled along $12^{\text {th }}$ Terrace ("Street B") with dedicated left- and right-turn lanes. US-36 should be modified to include dedicated right-turn lanes. Figure 29: US-36 and 12th Terrace ("Street B") Proposed Improvements shows these improvements.

Estimated Cost of Intersection Improvements: \$1,350,000

### 5.2.10 US-36 AND 13TH ROAD



Figure 30: US-36 and $13^{\text {th }}$ Road Proposed Improvements
$13^{\text {th }}$ Road should be considered a future Arterial Street. $13^{\text {th }}$ Road should be constructed as a three-lane section. Once signal warrants are met the intersection should be signalized. Eastbound and westbound right-turn lanes should be added to US-36. At the intersection, $13^{\text {th }}$ Road should include both dedicated left- and right-turn lanes. Figure 30: US-36 and 13th Road Proposed Improvements shows these recommendations.

Estimated Cost of Intersection Improvements: \$1,700,000

### 5.3 TRAFFIC SIGNALS

Three of the four existing traffic signals along the US-36 corridor (located at $8^{\text {th }}$ Street, $10^{\text {th }}$ Street, and $14^{\text {th }}$ Street) need to be upgraded. Upgrading these signals will make use of intersection detection reducing the delay experienced by US-36 travelers, allow for signal timing optimization and coordination through the central business district, incorporate an emergency vehicle prioritization, and allow for pushbutton activated pedestrian crossings. The $10^{\text {th }}$ Street signal upgrade is included with the recommended $10^{\text {th }}$ Street geometric improvements.

Estimated Cost of $8^{\text {th }}$ Street and $14^{\text {th }}$ Street Signal Upgrades: $\$ 50,000$ Each

### 5.4 PEDESTRIAN/BICYCLE FACILITIES

### 5.4.1 PEDESTRIAN FACILITIES

Improvements to pedestrian access throughout the corridor primarily involve constructing new sidewalk or replacing old and deteriorating sections of sidewalk. The following maps (Figure 31: Pedestrian Infrastructure (1 of 3), Figure 32: Pedestrian Infrastructure (2 of 3), and Figure 33: Pedestrian Infrastructure (3 of 3) indicate the areas throughout the corridor with existing sidewalk in good condition, existing sidewalk needing replaced, and areas where new sidewalk is suggested. In summary, there is approximately 650' of existing sidewalk that needs replaced. New sidewalk is recommended on the south side of US-36 from N. $11^{\text {th }}$ Street to $\mathrm{N} .20^{\text {th }}$ Street and on the north side of US-36 from N. $20^{\text {th }}$ Street east to connect to the existing sidewalk in front of the Wal-Mart.

Estimated Cost of Sidewalk Improvements: \$500,000

### 5.4.2 BICYCLE FACILITIES

Cycling facilities throughout the city are generally abundant. Bicyclists have good access throughout the residential areas where there is primarily local traffic. Bicyclists are encouraged to use Broadway Street as a primary means of east/west traffic within the downtown district. Adding designated "Bike Route" signs will help focus cycling traffic to Broadway Street. Both the shared used path south of Broadway and the Blue River Trail north of Broadway are excellent means of accessing the downtown district. Utilizing residential streets that cross US-36 at signalized intersections are also good ways for north/south bicycling traffic. Access to the east side of Marysville's more industrialized area by means of bicycle is best done by taking North Street or Keystone Road. $11^{\text {th }}$ Road north of US-36 already contains a bike lane on the west side of the street. Currently, cycling traffic in both the north and south direction utilizes this bike lane. Adding designated bicycling lanes to both sides of $11^{\text {th }}$ Road and North Street or constructing a 10' wide shareduse path would help improve bicycling safety. Bicycling on sidewalks is generally undesirable due to decreased visibility with turning traffic - but at times this is still safer than riding on a busy street, especially if the bicyclist is uncomfortable with traveling on the street. Bicyclists accessing businesses on US-36 should be encouraged to utilize future sidewalk, as there is currently no sidewalk east of $\mathrm{N} .20^{\text {th }}$ Street.

Estimated Cost of "Bike Route" signage: \$10,000

PEDESTRIAN INFRASTRUCTURE


LEGEND
= Existing Sidew alk

- Existing Sidew alk - Construct New Sidew alk

LOCATION KEY


Figure 31: Pedestrian Infrastructure (1 of 3)

## PEDESTRIAN INFRASTRUCTURE




LOCATION KEY


Figure 32: Pedestrian Infrastructure (2 of 3)


LEGEND
Existing Sidew alk

- Existing Sidew alk
- Construct New Sidew alk


LOCATION KEY


Figure 33: Pedestrian Infrastructure (3 of 3

## CHAPTER 6: IMPLEMENTATION

| No. | Project Description | Timing | Trigger | Project Cost [in millions | Agency |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 1. | Access Consolidations/Closures | Continual | As redevelopment occurs |  | $\begin{gathered} \text { City } \\ \text { KDOT } \\ \text { Private } \end{gathered}$ |
| 2. | Street Network Upgrades | Continual | As redevelopment occurs |  | City |
| 3. | Pedestrian Facilities Improvements | Short/Long Term | As redevelopment occurs | \$0.50 | City Private |
| 4. | Signal Upgrades | Short Term |  | \$0.05 | City |
| 5. | US-36 between $4^{\text {th }}$ and $5^{\text {th }}$ Streets Geometric Improvements | Long Term |  | \$0.30 | $\begin{gathered} \text { City } \\ \text { KDOT } \end{gathered}$ |
| 6. | US-36 \& $7^{\text {th }}$ Street Geometric Improvements | Short Term |  | \$0.55 | $\begin{gathered} \text { City } \\ \text { KDOT } \end{gathered}$ |
| 7. | US-36 \& US-77 (10 ${ }^{\text {th }}$ Street) Geometric Improvements | Short Term |  | \$0.85 | $\begin{aligned} & \text { City } \\ & \text { KDOT } \end{aligned}$ |
| 8. | US-36 \& $11^{\text {th }}$ Road Geometric Improvements | Short Term |  | \$1.50 | $\begin{gathered} \text { City } \\ \text { KDOT } \end{gathered}$ |
| 9. | US-36 \& $11^{\text {th }}$ Drive Geometric Improvements | Long Term | As development occurs | \$0.65 | $\begin{gathered} \text { City } \\ \text { KDOT } \end{gathered}$ |
| 10. | US-36 \& $11^{\text {th }}$ Terrace Geometric Improvements | Long Term | As development occurs | \$1.30 | $\begin{gathered} \text { City } \\ \text { KDOT } \end{gathered}$ |
| 11. | US-36 \& Walmart Geometric Improvements | Long Term | As development occurs | \$0.40 | $\begin{gathered} \text { City } \\ \text { KDOT } \end{gathered}$ |
| 12. | US-36 \& $12^{\text {th }}$ Road Geometric Improvements | Long Term | Once signal warrants are met | \$1.70 | $\begin{aligned} & \text { City } \\ & \text { KDOT } \end{aligned}$ |
| 13. | US-36 \& $12^{\text {th }}$ Terr. Geometric Improvements | Long Term | As development occurs | \$1.35 | $\begin{gathered} \text { City } \\ \text { KDOT } \end{gathered}$ |
| 14. | US-36 \& $13^{\text {th }}$ Road Geometric Improvements | Long Term | Once signal warrants are met | \$1.70 | $\begin{gathered} \text { City } \\ \text { KDOT } \end{gathered}$ |

APPENDIX A - PUBLIC INVOLVEMENT
A. 1 MEETINGS

PUBLIC MEETING SIGN-IN SHEET
6:00 p.m., November 30, 2017
US-36 Access Management Plan

$\frac{\text { Darlene Boss }}{\text { Name }} \frac{785-5 b 2-2942}{\text { Phone }} \frac{\text { darlencbosseati.net }}{\text { Email }}$


$\frac{\text { BOb }}{\text { Name }}$ CONNELL $\frac{785-5625554}{\text { Phone }} \frac{\text { BC ZIPPY AT GMALL }}{\text { Email }}$.COM Slew Raveler 785-207-7598 chasemarshallcountyksagmail.con Tony Suever $\frac{785-562-6915}{\text { Phone }} \frac{\text { tdueves@cesengineesing.com }}{\text { Email }}$


## APPENDIX B - CALCULATIONS

## B. 1 INTERSECTION INFLUENCE AREAS

| US-36 \& N. 4th Street |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | $\begin{aligned} & \hline \text { Speed } \\ & {[\mathrm{mph}]} \end{aligned}$ | Area Type | Lateral Shift? | $\begin{gathered} \text { Stop } \\ \text { Control } \end{gathered}$ | Peak Hour <br> [vph] | Vehicle Width [ft] | 95\% Queue [ft] | d1 <br> [ft] | d2 <br> [ft] | d3 <br> [ft] | d4 <br> [ft] | U.S. <br> [ft] | $\begin{gathered} \hline \text { D.S. } \\ {[\mathrm{ft]}} \end{gathered}$ |
| US-36 | West Leg | 30 | Developed/CBD | N | None |  |  |  | 65 | 87 | 0 | 155 | 152 | 155 |
|  | East Leg | 30 | Developed/CBD | N | None |  |  |  | 65 | 87 | 0 | 155 | 152 | 155 |


| US-36 \& N. 5th Street |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Speed <br> [mph] | Area Type | Lateral Shift? | $\begin{aligned} & \text { Stop } \\ & \text { Control } \end{aligned}$ | Peak Hour <br> [vph] | Vehicle Width [ft] | 95\% Queue [ft] | d1 [ft] | d2 <br> [ft] | d3 <br> [ft] | d4 [ft] | U.S. <br> [ft] | D.S. <br> [ft] |
| US-36 | West Leg | 30 | Developed/CBD | N | None |  |  |  | 65 | 87 | 0 | 155 | 152 | 155 |
|  | East Leg | 30 | Developed/CBD | N | None |  |  |  | 65 | 87 | 0 | 155 | 152 | 155 |


| US-36 \& N. 6th Street |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Speed <br> [mph] | Area Type | Lateral Shift? | Stop Control | Peak Hour <br> [vph] | Vehicle Width <br> [ft] | 95\% Queue <br> [ft] | d1 <br> [ft] | d2 <br> [ft] | d3 <br> [ft] | d4 <br> [ft] | U.S. <br> [ft] | D.S. <br> [ft] |
| US-36 | West Leg | 30 | Developed/CBD | N | None |  |  |  | 65 | 87 | 0 | 155 | 152 | 155 |
|  | East Leg | 30 | Developed/CBD | N | None |  |  |  | 65 | 87 | 0 | 155 | 152 | 155 |


| US-36 \& N. 7th Street |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Speed <br> [mph] | Area Type | Lateral Shift? | $\begin{aligned} & \text { Stop } \\ & \text { Control } \end{aligned}$ |  |  | Vehicle Width <br> [ft] | 95\% Queue [ft] | d1 <br> [ft] | d2 <br> [ft] | d3 <br> [ft] | d4 <br> [ft] | U.S. <br> [ft] | D.S. <br> [ft] |
| US-36 | West Leg | 30 | Developed/CBD | N | None |  |  |  |  | 65 | 87 | 0 | 155 | 152 | 155 |
|  | East Leg | 30 | Developed/CBD | N | None |  |  |  |  | 65 | 87 | 0 | 155 | 152 | 155 |
| $7^{\text {th }}$ St. | North Leg | 20 | Developed/CBD | N | Stop Sign | 20 | * | 25 |  | 45 | 39 | 60 | 85 | 144 | 85 |
| *Assum |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |


| US-36 \& N. 8th Street |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Speed | Area Type | Lateral Shift? | $\begin{aligned} & \text { Stop } \\ & \text { Control } \end{aligned}$ | Peak Hour <br> [vph] |  | Vehicle Width [ft] | $95 \%$ Queue <br> [ft] | d1 <br> [ft] | $\mathrm{d} 2$ | d3 <br> [ft] | d4 <br> [ft] | U.S. <br> [ft] | D.S. <br> [ft] |
| US-36 | West Leg | 30 | Developed/CBD | N | Signal |  |  |  | 78 | 65 | 87 | 78 | 155 | 230 | 155 |
|  | East Leg | 30 | Developed/CBD | N | Signal |  |  |  | 138 | 65 | 87 | 138 | 155 | 290 | 155 |
| N. 8th St. | South Leg | 20 | Developed/CBD | N | Signal | 77 | * | 30 | 31 | 45 | 39 | 60 | 85 | 144 | 85 |
|  | North Leg | 20 | Developed/CBD | N | Signal | 94 | * | 30 | 38 | 45 | 39 | 60 | 85 | 144 | 85 |
| *PM Peak |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |


| US-36 \& N. 9th Street |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Speed <br> [mph] | Area Type | Lateral Shift? | $\begin{aligned} & \text { Stop } \\ & \text { Control } \end{aligned}$ | Peak Hour <br> [vph] | Vehicle Width [ft] | 95\% Queue [ft] | d1 <br> [ft] | $\mathrm{d} 2$ <br> [ft] | d3 <br> [ft] | d4 <br> [ft] | U.S. <br> [ft] | D.S. <br> [ft] |
| US-36 | West Leg | 30 | Developed/CBD | N | None |  |  |  | 65 | 87 | 0 | 155 | 152 | 155 |
|  | East Leg | 30 | Developed/CBD | N | None |  |  |  | 65 | 87 | 0 | 155 | 152 | 155 |


| US-36 \& US-77 (N. 10th Street) |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | $\begin{aligned} & \hline \text { Speed } \\ & {[\mathrm{mph}]} \end{aligned}$ | Area Type | Lateral Shift? | $\begin{aligned} & \text { Stop } \\ & \text { Control } \end{aligned}$ | Peak [vp |  | Vehicle Width [ft] | 95\% Queue [ft] | d1 <br> [ft] | d2 <br> [ft] | d3 <br> [ft] | d4 <br> [ft] | U.S. <br> [ft] | $\begin{aligned} & \hline \text { D.S. } \\ & {[\mathrm{ft]}} \end{aligned}$ |
| US-36 | West Leg | 30 | Developed/CBD | N | Signal |  |  |  | 83 | 65 | 87 | 83 | 155 | 235 | 155 |
|  | East Leg | 30 | Developed/CBD | N | Signal |  |  |  | 157 | 65 | 87 | 157 | 155 | 309 | 155 |
| N. 10th St. | South Leg | 20 | Developed/CBD | N | Signal | 131 | * | 30 | 46 | 45 | 39 | 60 | 85 | 144 | 85 |
|  | North Leg | 20 | Developed/CBD | N | Signal | 18 | * | 30 | 14 | 45 | 39 | 60 | 85 | 144 | 85 |
| *PM Peak |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |


| US-36 \& N. 11th Street |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Speed <br> [mph] | Area Type | Lateral Shift? | $\begin{aligned} & \text { Stop } \\ & \text { Control } \end{aligned}$ | Peak Hour [vph] | Vehicle Width [ft] | 95\% Queue [ft] | d1 <br> [ft] | $\mathrm{d} 2$ <br> [ft] | d3 <br> [ft] | d4 <br> [ft] | U.S. <br> [ft] | D.S. <br> [ft] |
| US-36 | West Leg | 30 | Developed/CBD | N | None |  |  |  | 65 | 87 | 0 | 155 | 152 | 155 |
|  | East Leg | 30 | Developed/CBD | N | None |  |  |  | 65 | 87 | 0 | 155 | 152 | 155 |


| US-36 \& N. 12th Street |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Speed <br> [mph] | Area Type | Lateral Shift? | $\begin{gathered} \text { Stop } \\ \text { Control } \end{gathered}$ | Peak Hour <br> [vph] | Vehicle Width <br> [ft] | 95\% Queue <br> [ft] | d1 <br> [ft] | d2 <br> [ft] | d3 <br> [ft] | d4 <br> [ft] | U.S. <br> [ft] | D.S. <br> [ft] |
| US-36 | West Leg | 30 | Developed/CBD | N | None |  |  |  | 65 | 87 | 0 | 155 | 152 | 155 |
|  | East Leg | 30 | Developed/CBD | N | None |  |  |  | 65 | 87 | 0 | 155 | 152 | 155 |


| US-36 \& N. 13th Street |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Speed <br> [mph] | Area Type | Lateral Shift? | $\begin{aligned} & \text { Stop } \\ & \text { Control } \end{aligned}$ | Peak Hour <br> [vph] | Vehicle Width <br> [ft] | 95\% Queue <br> [ft] | d1 <br> [ft] | d2 <br> [ft] | d3 <br> [ft] | d4 <br> [ft] | U.S. <br> [ft] | D.S. <br> [ft] |
| US-36 | West Leg | 30 | Developed/CBD | N | None |  |  |  | 65 | 87 | 0 | 155 | 152 | 155 |
|  | East Leg | 30 | Developed/CBD | N | None |  |  |  | 65 | 87 | 0 | 155 | 152 | 155 |


| US-36 \& N. 14th Street |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Speed <br> [mph] | Area Type | Lateral Shift? | $\begin{aligned} & \hline \text { Stop } \\ & \text { Control } \end{aligned}$ | Peak |  | Vehicle Width [ft] | 95\% <br> Queue <br> [ft] | d1 <br> [ft] | d2 <br> [ft] | d3 <br> [ft] | d4 [ft] | U.S. <br> [ft] | $\begin{gathered} \hline \text { D.S. } \\ {[\mathrm{ft]}} \end{gathered}$ |
| US-36 | West Leg | 30 | Developed/CBD | N | Signal |  |  |  | 168 | 65 | 87 | 168 | 155 | 320 | 155 |
|  | East Leg | 30 | Developed/CBD | N | Signal |  |  |  | 186 | 65 | 87 | 186 | 155 | 338 | 155 |
| N. 14th St. | South Leg | 20 | Developed/CBD | N | Signal | 37 | * | 30 | 23 | 45 | 39 | 60 | 85 | 144 | 85 |
|  | North Leg | 20 | Developed/CBD | N | Signal | 40 | * | 30 | 27 | 45 | 39 | 60 | 85 | 144 | 85 |
| *PM Peak |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |


| US-36 \& N. 15th Street |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Speed <br> [mph] | Area Type | Lateral Shift? | $\begin{gathered} \text { Stop } \\ \text { Control } \end{gathered}$ | Peak Hour <br> [vph] | Vehicle Width [ft] | 95\% Queue [ft] | d1 <br> [ft] | d2 [ft] | d3 <br> [ft] | d4 <br> [ft] | U.S. <br> [ft] | D.S. <br> [ft] |
| US-36 | West Leg | 30 | Developed/CBD | N | None |  |  |  | 65 | 87 | 0 | 155 | 152 | 155 |
|  | East Leg | 30 | Developed/CBD | N | None |  |  |  | 65 | 87 | 0 | 155 | 152 | 155 |


| US-36 \& N. 17th Street |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Speed <br> [mph] | Area Type | Lateral Shift? | Stop Control | Peak Hour <br> [vph] | Vehicle Width <br> [ft] | 95\% Queue [ft] | d1 <br> [ft] | d2 <br> [ft] | d3 <br> [ft] | d4 <br> [ft] | U.S. <br> [ft] | D.S. <br> [ft] |
| US-36 | West Leg | 30 | Developed/CBD | N | None |  |  |  | 65 | 87 | 0 | 155 | 152 | 155 |
|  | East Leg | 30 | Developed/CBD | N | None |  |  |  | 65 | 87 | 0 | 155 | 152 | 155 |


| US-36 \& N. 18th Street |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Speed <br> [mph] | Area Type | Lateral Shift? | Stop Control | Peak Hour <br> [vph] | Vehicle Width <br> [ft] | 95\% Queue <br> [ft] | d1 <br> [ft] | d2 <br> [ft] | d3 <br> [ft] | d4 <br> [ft] | U.S. <br> [ft] | D.S. <br> [ft] |
| US-36 | West Leg | 30 | Developed/CBD | N | None |  |  |  | 65 | 87 | 0 | 155 | 152 | 155 |
|  | East Leg | 30 | Developed/CBD | N | None |  |  |  | 65 | 87 | 0 | 155 | 152 | 155 |


| US-36 \& N. 20th Street |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Speed <br> [mph] | Area Type | Lateral Shift? | $\begin{aligned} & \text { Stop } \\ & \text { Control } \end{aligned}$ |  |  | Vehicle Width [ft] | 95\% Queue [ft] | d1 <br> [ft] | d2 <br> [ft] | d3 <br> [ft] | d4 <br> [ft] | $\begin{aligned} & \hline \text { U.S. } \\ & {[\mathrm{ft]}} \end{aligned}$ | $\begin{gathered} \hline \text { D.S. } \\ {[\mathrm{ft}]} \end{gathered}$ |
| US-36 | West Leg | 30 | Developed/CBD | N | Signal |  |  |  | 33 | 65 | 87 | 33 | 155 | 185 | 155 |
|  | East Leg | 30 | Developed/CBD | N | Signal |  |  |  | 31 | 65 | 87 | 31 | 155 | 183 | 155 |
| N. 20th St. | North Leg | 30 | Developed/CBD | N | Signal | 34 | * | 30 | 10 | 65 | 87 | 60 | 155 | 212 | 155 |
| *PM Peak |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |


| US-36 \& 11th Road |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | $\begin{aligned} & \hline \text { Speed } \\ & \text { [mph] } \end{aligned}$ | Area Type | Lateral Shift? | Stop Control | Peak Hour <br> [vph] |  | Vehicle Width [ft] | 95\% Queue [ft] | d1 <br> [ft] | d2 <br> [ft] | d3 <br> [ft] | d4 [ft] | U.S. <br> [ft] | D.S. <br> [ft] |
| US-36 | West Leg | 45 | Developed/CBD | N | None |  |  |  |  | 100 | 195 | 0 | 295 | 295 | 295 |
|  | East Leg | 45 | Developed/CBD | N | None |  |  |  |  | 100 | 195 | 0 | 295 | 295 | 295 |
| 11th Road | South Leg | 30 | Developed/CBD | N | Stop Sign | 50 | * | 32 |  | 65 | 87 | 64 | 155 | 216 | 155 |
|  | North Leg | 30 | Developed/CBD | N | Stop Sign | 50 | * | 32 |  | 65 | 87 | 64 | 155 | 216 | 155 |


| US-36 \& 11th Drive |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Speed <br> [mph] | Area Type | Lateral Shift? | Stop Control | Peak Hour <br> [vph] | Vehicle Width <br> [ft] | 95\% Queue [ft] | d1 <br> [ft] | d2 <br> [ft] | d3 <br> [ft] | d4 <br> [ft] | U.S. <br> [ft] | D.S. <br> [ft] |
| US-36 | West Leg | 45 | Developed/CBD | N | None |  |  |  | 100 | 195 | 0 | 295 | 295 | 295 |
|  | East Leg | 45 | Developed/CBD | N | None |  |  |  | 100 | 195 | 0 | 295 | 295 | 295 |


| US-36 \& 11th Terrace |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Speed <br> [mph] | Area Type | Lateral Shift? | $\begin{gathered} \text { Stop } \\ \text { Control } \end{gathered}$ | Peak Hour <br> [vph] | Vehicle Width [ft] |  | d1 <br> [ft] | $\mathrm{d} 2$ | d3 <br> [ft] | d4 [ft] | U.S. [ft] | D.S. [ft] |
| US-36 | West Leg | 45 | Developed/CBD | N | None |  |  |  | 100 | 195 | 0 | 295 | 295 | 295 |
|  | East Leg | 45 | Developed/CBD | N | None |  |  |  | 100 | 195 | 0 | 295 | 295 | 295 |


| US-36 \& 12th Road |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | $\begin{aligned} & \hline \text { Speed } \\ & {[\mathrm{mph}]} \end{aligned}$ | Area Type | Lateral Shift? | Stop Control | Peak Hour <br> [vph] |  | Vehicle Width [ft] | 95\% Queue [ft] | d1 <br> [ft] | d2 <br> [ft] | d3 <br> [ft] | d4 <br> [ft] | U.S. <br> [ft] | $\begin{aligned} & \hline \text { D.S. } \\ & {[\mathrm{ft]}} \end{aligned}$ |
| US-36 | West Leg | 50 | Developed/CBD | N | None |  |  |  |  | 110 | 240 | 0 | 355 | 350 | 355 |
|  | East Leg | 50 | Developed/CBD | N | None |  |  |  |  | 110 | 240 | 0 | 355 | 350 | 355 |
| 12th Road | South Leg | 30 | Developed/CBD | N | Stop Sign | 50 | * | 32 |  | 65 | 87 | 64 | 155 | 216 | 155 |
|  | North Leg | 30 | Developed/CBD | N | Stop Sign | 50 | * | 32 |  | 65 | 87 | 64 | 155 | 216 | 155 |
| *Assumed |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |


| US-36 \& 13th Road |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | $\begin{gathered} \hline \text { Speed } \\ {[\mathrm{mph}]} \\ \hline \end{gathered}$ | Area Type | Lateral Shift? | $\begin{gathered} \text { Stop } \\ \text { Control } \end{gathered}$ |  |  | Vehicle Width <br> [ft] |  | d1 <br> [ft] | d2 <br> [ft] | d3 <br> [ft] | d4 <br> [ft] | U.S. <br> [ft] | D.S. <br> [ft] |
| US-36 | West Leg | 65 | Undeveloped | N | None |  |  |  |  | 110 | 406 | 0 | 645 | 516 | 645 |
|  | East Leg | 65 | Undeveloped | N | None |  |  |  |  | 110 | 406 | 0 | 645 | 516 | 645 |
| 12th Road | South Leg | 30 | Undeveloped | N | Stop Sign | 50 | * | 32 |  | 65 | 87 | 64 | 155 | 216 | 155 |
|  | North Leg | 30 | Undeveloped | N | Stop Sign | 50 | * | 32 |  | 65 | 87 | 64 | 155 | 216 | 155 |

## APPENDIX C - SYNCHRO MODELS

## C. 12017 AM PEAK HOUR (EXISTING OPERATING CONDITIONS)

| Synchro Model 6: US-36 \& N. 8th |  |  |  |  | 2017 AM Peak (Existing Operating Conditions) Lanes, Volumes, Timings |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 4 |  |  |  |  | 4 | 4 | $\uparrow$ | $p$ |  | $\downarrow$ | 4 |
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL. | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | ${ }^{*}$ | $\hat{\beta}$ |  | \% | $\uparrow$ | 7 |  | $\pm$ |  |  | ¢ |  |
| Traffic Volume (vph) | 33 | 248 | 30 | 16 | 172 | 12 | 7 | 11 | 2 | 21 | 22 | 16 |
| Future Volume (vph) | 33 | 248 | 30 | 16 | 172 | 12 | 7 | 11 | 2 | 21 | 22 | 16 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Storage Length (ft) | 85 |  | 0 | 75 |  | 75 | 0 |  | 0 | 0 |  | 0 |
| Storage Lanes | 1 |  | 0 | 1 |  | 1 | 0 |  | 0 | 0 |  | 0 |
| Taper Length (ft) | 25 |  |  | 25 |  |  | 25 |  |  | 25 |  |  |
| Lane Util. Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Fit |  | 0.984 |  |  |  | 0.850 |  | 0.988 |  |  | 0.964 |  |
| Flt Protected | 0.950 |  |  | 0.950 |  |  |  | 0.982 |  |  | 0.982 |  |
| Satd. Flow (prot) | 1770 | 1833 | 0 | 1770 | 1863 | 1583 | 0 | 1807 | 0 | 0 | 1763 | 0 |
| Flt Permitted | 0.640 |  |  | 0.555 |  |  |  | 0.932 |  |  | 0.920 |  |
| Satd. Flow (perm) | 1192 | 1833 | 0 | 1034 | 1863 | 1583 | 0 | 1715 | 0 | 0 | 1652 | 0 |
| Right Tum on Red |  |  | Yes |  |  | Yes |  |  | Yes |  |  | Yes |
| Satd. Flow (RTOR) |  | 15 |  |  |  | 36 |  | 2 |  |  | 17 |  |
| Link Speed (mph) |  | 30 |  |  | 30 |  |  | 20 |  |  | 20 |  |
| Link Distance (ft) |  | 694 |  |  | 680 |  |  | 497 |  |  | 526 |  |
| Travel Time (s) |  | 15.8 |  |  | 15.5 |  |  | 16.9 |  |  | 17.9 |  |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Adj. Flow (vph) | 36 | 270 | 33 | 17 | 187 | 13 | 8 | 12 | 2 | 23 | 24 | 17 |
| Shared Lane Traffic (\%) |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane Group Flow (vph) | 36 | 303 | 0 | 17 | 187 | 13 | 0 | 22 | 0 | 0 | 64 | 0 |
| Turn Type | Perm | NA |  | Perm | NA | Perm | Perm | NA |  | Perm | NA |  |
| Protected Phases |  | 4 |  |  | 8 |  |  | 2 |  |  | 6 |  |
| Permitted Phases | 4 |  |  | 8 |  | 8 | 2 |  |  | 6 |  |  |
| Minimum Split (s) | 23.0 | 23.0 |  | 23.0 | 23.0 | 23.0 | 23.0 | 23.0 |  | 23.0 | 23.0 |  |
| Total Split (s) | 35.0 | 35.0 |  | 35.0 | 35.0 | 35.0 | 25.0 | 25.0 |  | 25.0 | 25.0 |  |
| Total Split (\%) | 58.3\% | 58.3\% |  | 58.3\% | 58.3\% | 58.3\% | 41.7\% | 41.7\% |  | 41.7\% | 41.7\% |  |
| Yellow Time (s) | 4.0 | 4.0 |  | 4.0 | 4.0 | 4.0 | 3.0 | 3.0 |  | 3.0 | 3.0 |  |
| All-Red Time (s) | 1.0 | 1.0 |  | 1.0 | 1.0 | 1.0 | 2.0 | 2.0 |  | 2.0 | 2.0 |  |
| Lost Time Adjust (s) | 0.0 | 0.0 |  | 0.0 | 0.0 | 0.0 |  | 0.0 |  |  | 0.0 |  |
| Total Lost Time (s) | 5.0 | 5.0 |  | 5.0 | 5.0 | 5.0 |  | 5.0 |  |  | 5.0 |  |
| Lead/Lag |  |  |  |  |  |  |  |  |  |  |  |  |
| Lead-Lag Optimize? |  |  |  |  |  |  |  |  |  |  |  |  |
| Act Effct Green (s) | 30.0 | 30.0 |  | 30.0 | 30.0 | 30.0 |  | 20.0 |  |  | 20.0 |  |
| Actuated g/C Ratio | 0.50 | 0.50 |  | 0.50 | 0.50 | 0.50 |  | 0.33 |  |  | 0.33 |  |
| v/c Ratio | 0.06 | 0.33 |  | 0.03 | 0.20 | 0.02 |  | 0.04 |  |  | 0.11 |  |
| Control Delay | 8.2 | 9.7 |  | 7.9 | 9.1 | 1.2 |  | 13.1 |  |  | 11.7 |  |
| Queue Delay | 0.0 | 0.0 |  | 0.0 | 0.0 | 0.0 |  | 0.0 |  |  | 0.0 |  |
| Total Delay | 8.2 | 9.7 |  | 7.9 | 9.1 | 1.2 |  | 13.1 |  |  | 11.7 |  |
| LOS | A | A |  | A | A | A |  | B |  |  | B |  |
| Approach Delay |  | 9.6 |  |  | 8.5 |  |  | 13.1 |  |  | 11.7 |  |
| Approach LOS |  | A |  |  | A |  |  | B |  |  | B |  |
| Queue Length 50th (fi) | 6 | 57 |  | 3 | 35 | 0 |  | 5 |  |  | 11 |  |
| Queue Length 95th (ft) | 18 | 102 |  | 11 | 66 | 3 |  | 18 |  |  | 34 |  |
| Internal Link Dist (ft) |  | 614 |  |  | 600 |  |  | 417 |  |  | 446 |  |
| Turn Bay Length (ft) | 85 |  |  | 75 |  | 75 |  |  |  |  |  |  |
| Base Capacity (vph) | 596 | 924 |  | 517 | 931 | 809 |  | 573 |  |  | 562 |  |
| Starvation Cap Reductn | 0 | 0 |  | 0 | 0 | 0 |  | 0 |  |  | 0 |  |
| Baseline |  |  |  |  |  |  |  |  |  | Synchr | 10 Ligh | Report $\text { Page } 2$ |



| Synchro Model 12: US-36 \& N. 11th S |  |  |  |  | 2017 AM Peak (Existing Operating Conditions) HCM Unsignalized Intersection Capacity Analysis |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $\rangle$ | $\rightarrow$ |  | $\checkmark$ |  |  |  | $\uparrow$ |  |  | $\downarrow$ | $\downarrow$ |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | 7 | 今 |  | \% | 今 |  |  | ¢ |  |  | ¢ |  |
| Traffic Volume (veh/h) | 12 | 291 | 2 | 25 | 321 | 27 | 2 | 2 | 12 | 8 | 3 | 11 |
| Future Volume (Veh/h) | 12 | 291 | 2 | 25 | 321 | 27 | 2 | 2 | 12 | 8 | 3 | 11 |
| Sign Control |  | Free |  |  | Free |  |  | Stop |  |  | Stop |  |
| Grade |  | 0\% |  |  | 0\% |  |  | 0\% |  |  | 0\% |  |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Hourly flow rate (vph) | 13 | 316 | 2 | 27 | 349 | 29 | , | 2 | 13 | 9 | 3 | 12 |
| Pedestrians |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane Width (fi) |  |  |  |  |  |  |  |  |  |  |  |  |
| Walking Speed (t/s) |  |  |  |  |  |  |  |  |  |  |  |  |
| Percent Blockage |  |  |  |  |  |  |  |  |  |  |  |  |
| Right turn flare (veh) |  |  |  |  |  |  |  |  |  |  |  |  |
| Median type |  | None |  |  | TWLTL |  |  |  |  |  |  |  |
| Median storage veh) |  |  |  |  | 2 |  |  |  |  |  |  |  |
| Upstream signal (ft) |  | 349 |  |  | 1029 |  |  |  |  |  |  |  |
| pX, platoon unblocked |  |  |  |  |  |  |  |  |  |  |  |  |
| VC , conflicting volume | 378 |  |  | 318 |  |  | 760 | 775 | 317 | 774 | 762 | 364 |
| VC1, stage 1 conf vol |  |  |  |  |  |  | 343 | 343 |  | 418 | 418 |  |
| vC2, stage 2 conf vol |  |  |  |  |  |  | 416 | 432 |  | 356 | 344 |  |
| vCu , unblocked vol | 378 |  |  | 318 |  |  | 760 | 775 | 317 | 774 | 762 | 364 |
| IC, single (s) | 4.1 |  |  | 4.1 |  |  | 7.1 | 6.5 | 6.2 | 7.1 | 6.5 | 6.2 |
| IC, 2 stage (s) |  |  |  |  |  |  | 6.1 | 5.5 |  | 6.1 | 5.5 |  |
| IF (s) | 2.2 |  |  | 2.2 |  |  | 3.5 | 4.0 | 3.3 | 3.5 | 4.0 | 3.3 |
| poqueve free \% | 99 |  |  | 98 |  |  | 100 | 100 | 98 | 98 | 99 | 98 |
| cM capacity (veh/h) | 1180 |  |  | 1242 |  |  | 497 | 486 | 724 | 493 | 489 | 681 |
| Direction, Lane\# | EB 1 | EB2 | WB 1 | WB2 | NB 1 | SB1 |  |  |  |  |  |  |
| Volume Total | 13 | 318 | 27 | 378 | 17 | 24 |  |  |  |  |  |  |
| Volume Left | 13 | 0 | 27 | 0 | 2 | 9 |  |  |  |  |  |  |
| Volume Right | , | 2 | 0 | 29 | 13 | 12 |  |  |  |  |  |  |
| CSH | 1180 | 1700 | 1242 | 1700 | 651 | 571 |  |  |  |  |  |  |
| Volume to Capacity | 0.01 | 0.19 | 0.02 | 0.22 | 0.03 | 0.04 |  |  |  |  |  |  |
| Queue Length 95th (f) | 1 | 0 | 2 | 0 | 2 | 3 |  |  |  |  |  |  |
| Control Delay (s) | 8.1 | 0.0 | 8.0 | 0.0 | 10.7 | 11.6 |  |  |  |  |  |  |
| Lane LOS | A |  | A |  | B | B |  |  |  |  |  |  |
| Approach Delay (s) | 0.3 |  | 0.5 |  | 10.7 | 11.6 |  |  |  |  |  |  |
| Approach LOS |  |  |  |  | B | B |  |  |  |  |  |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |
| Average Delay |  |  | 1.0 |  |  |  |  |  |  |  |  |  |
| Intersection Capacity Utilization |  |  | 30.8\% |  | CU Level | Service |  |  | A |  |  |  |
| Analysis Period (min) |  |  | 15 |  |  |  |  |  |  |  |  |  |

Baseline | Synchro 10 Light Report |
| ---: |
| Page 2 |

Synchro Model 2017 AM Peak (Existing Operating Conditions)

| Lanes, Volumes, Timings |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $y$ |  |  | $\dagger$ |  | 4 | 4 | $\uparrow$ |  |  | $\downarrow$ | $\downarrow$ |
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | 7 | $\dagger$ |  | ${ }_{7}$ | $\dagger$ |  |  | ¢ |  |  | ¢ |  |
| Traffic Volume (vph) | 3 | 286 | 19 | 4 | 302 | 7 | 5 | 2 | 3 | 21 | 2 | 12 |
| Future Volume (vph) | 3 | 286 | 19 | 4 | 302 | 7 | 5 | 2 | 3 | 21 | 2 | 12 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Storage Length (fi) | 125 |  | 0 | 75 |  | 0 | 0 |  | 0 | 0 |  | 0 |
| Storage Lanes | 1 |  | 0 | 1 |  | 0 | 0 |  | 0 | 0 |  | 0 |
| Taper Length ( $t$ ) | 25 |  |  | 25 |  |  | 25 |  |  | 25 |  |  |
| Lane Util. Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Fit |  | 0.991 |  |  | 0.996 |  |  | 0.959 |  |  | 0.954 |  |
| Flt Protected | 0.950 |  |  | 0.950 |  |  |  | 0.976 |  |  | 0.971 |  |
| Satd. Flow (prot) | 1770 | 1846 | 0 | 1770 | 1855 | 0 | 0 | 1743 | 0 | 0 | 1726 | 0 |
| Fll Permitted | 0.547 |  |  | 0.551 |  |  |  | 0.921 |  |  | 0.874 |  |
| Satd. Flow (perm) | 1019 | 1846 | 0 | 1026 | 1855 | 0 | 0 | 1645 | 0 | 0 | 1553 | 0 |
| Right Tum on Red |  |  | Yes |  |  | Yes |  |  | Yes |  |  | Yes |
| Satd. Flow (RTOR) |  | 8 |  |  | 3 |  |  | 3 |  |  | 13 |  |
| Link Speed (mph) |  | 30 |  |  | 30 |  |  | 20 |  |  | 30 |  |
| Link Distance (t) |  | 1029 |  |  | 341 |  |  | 457 |  |  | 627 |  |
| Travel Time (s) |  | 23.4 |  |  | 7.8 |  |  | 15.6 |  |  | 14.3 |  |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Adj. Flow (vph) | 3 | 311 | 21 | 4 | 328 | 8 | 5 | 2 | 3 | 23 | 2 | 13 |
| Shared Lane Traffic (\%) |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane Group Flow (vph) | 3 | 332 | 0 | 4 | 336 | 0 | 0 | 10 | 0 | 0 | 38 | 0 |
| Turn Type | Perm | NA |  | Perm | NA |  | Perm | NA |  | Perm | NA |  |
| Protected Phases |  | 4 |  |  | 8 |  |  | 2 |  |  | 6 |  |
| Permitted Phases | 4 |  |  | 8 |  |  | 2 |  |  | 6 |  |  |
| Minimum Split (s) | 24.0 | 24.0 |  | 24.0 | 24.0 |  | 23.0 | 23.0 |  | 23.0 | 23.0 |  |
| Total Split (s) | 39.0 | 39.0 |  | 39.0 | 39.0 |  | 23.0 | 23.0 |  | 23.0 | 23.0 |  |
| Total Split (\%) | 62.9\% | 62.9\% |  | 62.9\% | 62.9\% |  | 37.1\% | 37.1\% |  | 37.1\% | 37.1\% |  |
| Yellow Time (s) | 4.0 | 4.0 |  | 4.0 | 4.0 |  | 4.0 | 4.0 |  | 4.0 | 4.0 |  |
| All-Red Time (s) | 2.0 | 2.0 |  | 2.0 | 2.0 |  | 1.0 | 1.0 |  | 1.0 | 1.0 |  |
| Lost Time Adjust (s) | 0.0 | 0.0 |  | 0.0 | 0.0 |  |  | 0.0 |  |  | 0.0 |  |
| Total Lost Time (s) | 6.0 | 6.0 |  | 6.0 | 6.0 |  |  | 5.0 |  |  | 5.0 |  |
| Lead/Lag |  |  |  |  |  |  |  |  |  |  |  |  |
| Lead-Lag Optimize? |  |  |  |  |  |  |  |  |  |  |  |  |
| Act Effit Green (s) | 33.0 | 33.0 |  | 33.0 | 33.0 |  |  | 18.0 |  |  | 18.0 |  |
| Actuatedg/C Ratio | 0.53 | 0.53 |  | 0.53 | 0.53 |  |  | 0.29 |  |  | 0.29 |  |
| vic Ratio | 0.01 | 0.34 |  | 0.01 | 0.34 |  |  | 0.02 |  |  | 0.08 |  |
| Control Delay | 7.0 | 9.2 |  | 7.0 | 9.4 |  |  | 14.0 |  |  | 12.6 |  |
| Queue Delay | 0.0 | 0.0 |  | 0.0 | 0.0 |  |  | 0.0 |  |  | 0.0 |  |
| Total Delay | 7.0 | 9.2 |  | 7.0 | 9.4 |  |  | 14.0 |  |  | 12.6 |  |
| LOS | A | A |  | A | A |  |  | B |  |  | B |  |
| Approach Delay |  | 9.2 |  |  | 9.4 |  |  | 14.0 |  |  | 12.6 |  |
| Approach LOS |  | A |  |  | A |  |  | B |  |  | B |  |
| Queue Length 50th (ti) | 1 | 63 |  | 1 | 65 |  |  | 2 |  |  | 7 |  |
| Queue Length 95th (fi) | 4 | 109 |  | 4 | 112 |  |  | 11 |  |  | 26 |  |
| Internal Link Dist (f) |  | 949 |  |  | 261 |  |  | 377 |  |  | 547 |  |
| Turn Bay Length (ft) | 125 |  |  | 75 |  |  |  |  |  |  |  |  |
| Base Capacity (vph) | 542 | 986 |  | 546 | 988 |  |  | 479 |  |  | 460 |  |
| Starvation Cap Reductn | 0 | 0 |  | 0 | 0 |  |  | 0 |  |  | 0 |  |

## Baseline

Synchro 10 Light Report
Page 7


| Synchro Model 24: US-36 \& 20th |  |  |  |  | 2017 AM Peak (Existing Operating Conditions) |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $\gamma$ | $\rightarrow$ | 7 | 1 | $\leftarrow$ | 4 | 4 | $\uparrow$ |  |  | $\downarrow$ | $\downarrow$ |
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | $\dagger$ | A |  | \% | 今 |  |  | ¢ |  |  | 4 | 7 |
| Traffic Volume (vph) | 35 | 300 | 1 | 0 | 223 | 27 | 0 | 0 | 0 | 37 | 0 | 37 |
| Future Volume (vph) | 35 | 300 | 1 | 0 | 223 | 27 | 0 | 0 | 0 | 37 | 0 | 37 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Storage Length (ft) | 185 |  | 0 | 100 |  | 0 | 0 |  | 0 | 0 |  | 60 |
| Storage Lanes | 1 |  | 0 | 1 |  | 0 | 0 |  | 0 | 0 |  | 1 |
| Taper Length (t) | 25 |  |  | 25 |  |  | 25 |  |  | 25 |  |  |
| Lane Util. Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Fit |  |  |  |  | 0.984 |  |  |  |  |  |  | 0.850 |
| Fll Protected | 0.950 |  |  |  |  |  |  |  |  |  | 0.950 |  |
| Satd. Flow (prot) | 1770 | 1863 | 0 | 1863 | 1833 | 0 | 0 | 1863 | 0 | 0 | 1770 | 1583 |
| Flt Permitted | 0.593 |  |  |  |  |  |  |  |  |  | 0.909 |  |
| Satd. Flow (perm) | 1105 | 1863 | 0 | 1863 | 1833 | 0 | 0 | 1863 | 0 | 0 | 1693 | 1583 |
| Right Tum on Red |  |  | Yes |  |  | Yes |  |  | Yes |  |  | Yes |
| Satd. Flow (RTOR) |  |  |  |  | 14 |  |  |  |  |  |  | 68 |
| Link Speed (mph) |  | 30 |  |  | 30 |  |  | 30 |  |  | 30 |  |
| Link Distance (fi) |  | 971 |  |  | 3848 |  |  | 371 |  |  | 570 |  |
| Travel Time (s) |  | 22.1 |  |  | 87.5 |  |  | 8.4 |  |  | 13.0 |  |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Adj. Flow (vph) | 38 | 326 | 1 | 0 | 242 | 29 | 0 | 0 | 0 | 40 | 0 | 40 |
| Shared Lane Traficic (\%) |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane Group Flow (vph) | 38 | 327 | 0 | 0 | 271 | 0 | 0 | 0 | 0 | 0 | 40 | 40 |
| Turn Type | Perm | NA |  | Perm | NA |  |  |  |  | Perm | NA | Perm |
| Protected Phases |  | 4 |  |  | 8 |  |  | 2 |  |  | 6 |  |
| Permitted Phases | 4 |  |  | 8 |  |  | 2 |  |  | 6 |  | 6 |
| Detector Phase | 4 | 4 |  | 8 | 8 |  | 2 | 2 |  | 6 | 6 | 6 |
| Switch Phase |  |  |  |  |  |  |  |  |  |  |  |  |
| Minimum Initial (s) | 8.0 | 8.0 |  | 6.0 | 6.0 |  | 6.0 | 6.0 |  | 8.0 | 8.0 | 8.0 |
| Minimum Split (s) | 14.0 | 14.0 |  | 12.0 | 12.0 |  | 12.0 | 12.0 |  | 14.0 | 14.0 | 14.0 |
| Total Split (s) | 24.0 | 24.0 |  | 24.0 | 24.0 |  | 24.0 | 24.0 |  | 24.0 | 24.0 | 24.0 |
| Total Split (\%) | 50.0\% | 50.0\% |  | 50.0\% | 50.0\% |  | 50.0\% | 50.0\% |  | 50.0\% | 50.0\% | 50.0\% |
| Yellow Time (s) | 4.0 | 4.0 |  | 4.0 | 4.0 |  | 4.0 | 4.0 |  | 4.0 | 4.0 | 4.0 |
| All-Red Time (s) | 2.0 | 2.0 |  | 2.0 | 2.0 |  | 2.0 | 2.0 |  | 2.0 | 2.0 | 2.0 |
| Lost Time Adjust (s) | 0.0 | 0.0 |  | 0.0 | 0.0 |  |  | 0.0 |  |  | 0.0 | 0.0 |
| Total Lost Time (s) | 6.0 | 6.0 |  | 6.0 | 6.0 |  |  | 6.0 |  |  | 6.0 | 6.0 |
| Lead/Lag |  |  |  |  |  |  |  |  |  |  |  |  |
| Lead-Lag Optimize? |  |  |  |  |  |  |  |  |  |  |  |  |
| Recall Mode | Min | Min |  | Min | Min |  | None | None |  | None | None | None |
| Act Effict Green (s) | 24.1 | 24.1 |  |  | 24.1 |  |  |  |  |  | 8.3 | 8.3 |
| Actuated g/C Ratio | 0.69 | 0.69 |  |  | 0.69 |  |  |  |  |  | 0.24 | 0.24 |
| vic Ratio | 0.05 | 0.26 |  |  | 0.21 |  |  |  |  |  | 0.10 | 0.09 |
| Control Delay | 5.8 | 6.0 |  |  | 5.6 |  |  |  |  |  | 12.6 | 2.9 |
| Queue Delay | 0.0 | 0.0 |  |  | 0.0 |  |  |  |  |  | 0.0 | 0.0 |
| Total Delay | 5.8 | 6.0 |  |  | 5.6 |  |  |  |  |  | 12.6 | 2.9 |
| LOS | A | A |  |  | A |  |  |  |  |  | B | A |
| Approach Delay |  | 6.0 |  |  | 5.6 |  |  |  |  |  | 7.8 |  |
| Approach LOS |  | A |  |  | A |  |  |  |  |  | A |  |
| Queue Length 50th (fi) | 4 | 39 |  |  | 29 |  |  |  |  |  | 9 | 0 |
| Queue Length 95th (ft) | 13 | 77 |  |  | 61 |  |  |  |  |  | 21 | 9 |

Baseline
Synchro 10 Light Report
Page 11


| Synchro Model 27: US-36 \& 11th Rd. |  |  |  |  | 2017 AM Peak (Existing Operating Conditions) HCM Unsignalized Intersection Capacity Analysis |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $y$ |  |  | 7 | $\leftarrow$ |  | 4 | $\uparrow$ | $p$ |  | $\downarrow$ |  |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SRR |
| Lane Configurations | 7 | $\dagger$ |  | $\dagger$ | 今 |  |  | $\dagger$ | 7 |  | 4 | F |
| Traffic Volume (veh'h) | 12 | 245 | 40 | 14 | 258 | 15 | 43 | 12 | 19 | 5 | 8 | 20 |
| Future Volume (Veh/h) | 12 | 245 | 40 | 14 | 258 | 15 | 43 | 12 | 19 | 5 | 8 | 20 |
| Sign Control |  | Free |  |  | Free |  |  | Stop |  |  | Stop |  |
| Grade |  | 0\% |  |  | 0\% |  |  | 0\% |  |  | 0\% |  |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Hourly flow rate (vph) | 13 | 266 | 43 | 15 | 280 | 16 | 47 | 13 | 21 | 5 | 9 | 22 |
| Pedestrians |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane Width (ft) |  |  |  |  |  |  |  |  |  |  |  |  |
| Walking Speed (ff/s) |  |  |  |  |  |  |  |  |  |  |  |  |
| Percent Blockage |  |  |  |  |  |  |  |  |  |  |  |  |
| Right turn flare (veh) |  |  |  |  |  |  |  |  | 3 |  |  | 4 |
| Median type |  | WLTL |  |  | TWLTL |  |  |  |  |  |  |  |
| Median storage veh) |  | 2 |  |  | 2 |  |  |  |  |  |  |  |
| Upstream signal (ft) |  |  |  |  |  |  |  |  |  |  |  |  |
| pX, platoon unblocked |  |  |  |  |  |  |  |  |  |  |  |  |
| vC, conflicting volume | 296 |  |  | 309 |  |  | 639 | 640 | 288 | 627 | 653 | 288 |
| vC1, stage 1 conf vol |  |  |  |  |  |  | 314 | 314 |  | 318 | 318 |  |
| $\mathrm{vC2}$, stage 2 conf vol |  |  |  |  |  |  | 326 | 326 |  | 309 | 335 |  |
| vCu , unblocked vol | 296 |  |  | 309 |  |  | 639 | 640 | 288 | 627 | 653 | 288 |
| tC, single (s) | 4.1 |  |  | 4.1 |  |  | 7.1 | 6.5 | 6.2 | 7.1 | 6.5 | 6.2 |
| tC, 2 stage (s) |  |  |  |  |  |  | 6.1 | 5.5 |  | 6.1 | 5.5 |  |
| tF (s) | 2.2 |  |  | 2.2 |  |  | 3.5 | 4.0 | 3.3 | 3.5 | 4.0 | 3.3 |
| po queue free \% | 99 |  |  | 99 |  |  | 91 | 98 | 97 | 99 | 98 | 97 |
| cM capacity (veh/h) | 1265 |  |  | 1252 |  |  | 549 | 541 | 752 | 553 | 535 | 751 |
| Direction, Lane \# | EB 1 | EB2 | WB 1 | WB 2 | NB1 | SB 1 |  |  |  |  |  |  |
| Volume Total | 13 | 309 | 15 | 296 | 81 | 36 |  |  |  |  |  |  |
| Volume Left | 13 | 0 | 15 | 0 | 47 | 5 |  |  |  |  |  |  |
| Volume Right | 0 | 43 | 0 | 16 | 21 | 22 |  |  |  |  |  |  |
| cSH | 1265 | 1700 | 1252 | 1700 | 739 | 1229 |  |  |  |  |  |  |
| Volume to Capacity | 0.01 | 0.18 | 0.01 | 0.17 | 0.11 | 0.03 |  |  |  |  |  |  |
| Queue Length 95th (ft) | 1 | 0 | 1 | 0 | 9 | 2 |  |  |  |  |  |  |
| Control Delay (s) | 7.9 | 0.0 | 7.9 | 0.0 | 11.8 | 10.7 |  |  |  |  |  |  |
| Lane LOS | A |  | A |  | B | B |  |  |  |  |  |  |
| Approach Delay (s) | 0.3 |  | 0.4 |  | 11.8 | 10.7 |  |  |  |  |  |  |
| Approach LOS |  |  |  |  | B | B |  |  |  |  |  |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |
| Average Delay |  |  | 2.1 |  |  |  |  |  |  |  |  |  |
| Intersection Capacity Utilization |  |  | 32.0\% |  | CU Level | Service |  |  | A |  |  |  |
| Analysis Period (min) |  |  | 15 |  |  |  |  |  |  |  |  |  |


| Baseline | Synchro 10 Light Report |
| ---: | ---: |
| Page 5 |  |

## C. 22017 PM PEAK HOUR (EXISTING OPERATING CONDITIONS)

| Synchro Model 3: US-36 \& N. 6th St. |  |  |  | 2017 PM Peak (Existing Operating Conditions) HCM Unsignalized Intersection Capacity Analysis |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $\rangle$ |  | 7 | 1 | 4 |  | 4 | $\uparrow$ | $p$ |  | $\downarrow$ | $\downarrow$ |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations |  | ¢ |  |  | ¢ |  |  | ¢ |  |  | ¢ |  |
| Traffic Volume (veh/h) | 8 | 215 | 14 | 36 | 370 | 25 | 26 | 15 | 42 | 16 | 3 | 4 |
| Future Volume (Veh/h) | 8 | 215 | 14 | 36 | 370 | 25 | 26 | 15 | 42 | 16 | 3 | 4 |
| Sign Control |  | Free |  |  | Free |  |  | Stop |  |  | Stop |  |
| Grade |  | 0\% |  |  | 0\% |  |  | 0\% |  |  | 0\% |  |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Hourly flow rate (yph) | 9 | 234 | 15 | 39 | 402 | 27 | 28 | 16 | 46 | 17 | 3 | 4 |
| Pedestrians |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane Width (fi) |  |  |  |  |  |  |  |  |  |  |  |  |
| Walking Speed (t/s) |  |  |  |  |  |  |  |  |  |  |  |  |
| Percent Blockage |  |  |  |  |  |  |  |  |  |  |  |  |
| Right tum flare (veh) |  |  |  |  |  |  |  |  |  |  |  |  |
| Median type |  | None |  |  | None |  |  |  |  |  |  |  |
| Median storage veh) |  |  |  |  |  |  |  |  |  |  |  |  |
| Upstream signal (f) |  |  |  |  | 694 |  |  |  |  |  |  |  |
| pX, platoon unblocked | 0.96 |  |  |  |  |  | 0.96 | 0.96 |  | 0.96 | 0.96 | 0.96 |
| vC, conflicting volume | 429 |  |  | 249 |  |  | 758 | 766 | 242 | 807 | 760 | 416 |
| vC1, stage 1 conf vol |  |  |  |  |  |  |  |  |  |  |  |  |
| VC2, stage 2 conf vol |  |  |  |  |  |  |  |  |  |  |  |  |
| VCu , unblocked vol | 385 |  |  | 249 |  |  | 728 | 736 | 242 | 778 | 730 | 370 |
| IC, single (s) | 4.1 |  |  | 4.1 |  |  | 7.1 | 6.5 | 6.2 | 7.1 | 6.5 | 6.2 |
| IC, 2 stage (s) |  |  |  |  |  |  |  |  |  |  |  |  |
| $\mathrm{tF}(\mathrm{s})$ | 2.2 |  |  | 2.2 |  |  | 3.5 | 4.0 | 3.3 | 3.5 | 4.0 | 3.3 |
| po queue free \% | 99 |  |  | 97 |  |  | 91 | 95 | 94 | 94 | 99 | 99 |
| cM capacity (veh/h) | 1127 |  |  | 1317 |  |  | 312 | 320 | 797 | 265 | 323 | 648 |
| Direction, Lane\# | EB 1 | WB1 | NB 1 | SB1 |  |  |  |  |  |  |  |  |
| Volume Total | 258 | 468 | 90 | 24 |  |  |  |  |  |  |  |  |
| Volume Left | 9 | 39 | 28 | 17 |  |  |  |  |  |  |  |  |
| Volume Right | 15 | 27 | 46 | 4 |  |  |  |  |  |  |  |  |
| CSH | 1127 | 1317 | 456 | 302 |  |  |  |  |  |  |  |  |
| Volume to Capacity | 0.01 | 0.03 | 0.20 | 0.08 |  |  |  |  |  |  |  |  |
| Queue Length 95th (ti) | 1 | 2 | 18 | 6 |  |  |  |  |  |  |  |  |
| Control Delay (s) | 0.4 | 0.9 | 14.8 | 18.0 |  |  |  |  |  |  |  |  |
| Lane LOS | A | A | B | c |  |  |  |  |  |  |  |  |
| Approach Delay (s) | 0.4 | 0.9 | 14.8 | 18.0 |  |  |  |  |  |  |  |  |
| Approach LOS |  |  | B | C |  |  |  |  |  |  |  |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |
| Average Delay |  |  | 2.7 |  |  |  |  |  |  |  |  |  |
| Intersection Capacity Utilization |  |  | 48.0\% |  | CULeve | f Service |  |  | A |  |  |  |
| Analysis Period (min) |  |  | 15 |  |  |  |  |  |  |  |  |  |


| Synchro Model 6: US-36 \& N. 8th St. |  |  |  |  | 2017 PM Peak (Existing Operating Conditions) Lanes, Volumes, Timings |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $\gamma$ | $\rightarrow$ |  | $\checkmark$ | $\leftarrow$ |  | 4 | $\uparrow$ |  |  |  | $\downarrow$ |
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | \% | F |  | \% | $\uparrow$ | 7 |  | ¢ |  |  | \$ |  |
| Traffic Volume (vph) | 23 | 265 | 16 | 34 | 331 | 23 | 17 | 34 | 49 | 40 | 28 | 51 |
| Future Volume (vph) | 23 | 265 | 16 | 34 | 331 | 23 | 17 | 34 | 49 | 40 | 28 | 51 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Storage Length (ft) | 85 |  | 0 | 75 |  | 75 | 0 |  | 0 | 0 |  | 0 |
| Storage Lanes | 1 |  | 0 | 1 |  | 1 | 0 |  | 0 | 0 |  | 0 |
| Taper Length (ft) | 25 |  |  | 25 |  |  | 25 |  |  | 25 |  |  |
| Lane Util. Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Fit |  | 0.992 |  |  |  | 0.850 |  | 0.934 |  |  | 0.942 |  |
| Fll Protected | 0.950 |  |  | 0.950 |  |  |  | 0.992 |  |  | 0.983 |  |
| Satd. Flow (prot) | 1770 | 1848 | 0 | 1770 | 1863 | 1583 | 0 | 1726 | 0 | 0 | 1725 | 0 |
| Fit Permitted | 0.501 |  |  | 0.553 |  |  |  | 0.949 |  |  | 0.884 |  |
| Satd. Flow (perm) | 933 | 1848 | 0 | 1030 | 1863 | 1583 | 0 | 1651 | 0 | 0 | 1551 | 0 |
| Right Tum on Red |  |  | Yes |  |  | Yes |  |  | Yes |  |  | Yes |
| Satd. Flow (RTOR) |  | 7 |  |  |  | 36 |  | 53 |  |  | 55 |  |
| Link Speed (mph) |  | 30 |  |  | 30 |  |  | 20 |  |  | 20 |  |
| Link Distance (ft) |  | 694 |  |  | 680 |  |  | 497 |  |  | 526 |  |
| Travel Time (s) |  | 15.8 |  |  | 15.5 |  |  | 16.9 |  |  | 17.9 |  |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Adj. Flow (vph) | 25 | 288 | 17 | 37 | 360 | 25 | 18 | 37 | 53 | 43 | 30 | 55 |
| Shared Lane Trafic (\%) |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane Group Flow (vph) | 25 | 305 | 0 | 37 | 360 | 25 | 0 | 108 | 0 | 0 | 128 | 0 |
| Turn Type | Perm | NA |  | Perm | NA | Perm | Perm | NA |  | Perm | NA |  |
| Protected Phases |  | , |  |  | . |  |  | 2 |  |  | 6 |  |
| Permitted Phases | 4 |  |  | 8 |  | 8 | 2 |  |  | 6 |  |  |
| Minimum Split (s) | 23.0 | 23.0 |  | 23.0 | 23.0 | 23.0 | 23.0 | 23.0 |  | 23.0 | 23.0 |  |
| Total Split (s) | 35.0 | 35.0 |  | 35.0 | 35.0 | 35.0 | 25.0 | 25.0 |  | 25.0 | 25.0 |  |
| Total Split (\%) | 58.3\% | 58.3\% |  | 58.3\% | 58.3\% | 58.3\% | 41.7\% | 41.7\% |  | 41.7\% | 41.7\% |  |
| Maximum Green (s) | 30.0 | 30.0 |  | 30.0 | 30.0 | 30.0 | 20.0 | 20.0 |  | 20.0 | 20.0 |  |
| Yellow Time (s) | 4.0 | 4.0 |  | 4.0 | 4.0 | 4.0 | 3.0 | 3.0 |  | 3.0 | 3.0 |  |
| All-Red Time (s) | 1.0 | 1.0 |  | 1.0 | 1.0 | 1.0 | 2.0 | 2.0 |  | 2.0 | 2.0 |  |
| Lost Time Adjust (s) | 0.0 | 0.0 |  | 0.0 | 0.0 | 0.0 |  | 0.0 |  |  | 0.0 |  |
| Total Lost Time (s) | 5.0 | 5.0 |  | 5.0 | 5.0 | 5.0 |  | 5.0 |  |  | 5.0 |  |
| Lead/Lag |  |  |  |  |  |  |  |  |  |  |  |  |
| Lead-Lag Optimize? |  |  |  |  |  |  |  |  |  |  |  |  |
| Walk Time (s) | 7.0 | 7.0 |  | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 |  | 7.0 | 7.0 |  |
| Flash Dont Walk (s) | 11.0 | 11.0 |  | 11.0 | 11.0 | 11.0 | 11.0 | 11.0 |  | 11.0 | 11.0 |  |
| Pedestrian Calls (\#hr) | 0 | 0 |  | 0 | 0 | 0 | 0 | 0 |  | 0 | 0 |  |
| Act Effct Green (s) | 30.0 | 30.0 |  | 30.0 | 30.0 | 30.0 |  | 20.0 |  |  | 20.0 |  |
| Actuated g/C Ratio | 0.50 | 0.50 |  | 0.50 | 0.50 | 0.50 |  | 0.33 |  |  | 0.33 |  |
| vic Ratio | 0.05 | 0.33 |  | 0.07 | 0.39 | 0.03 |  | 0.18 |  |  | 0.23 |  |
| Control Delay | 8.2 | 10.0 |  | 8.3 | 10.9 | 2.5 |  | 9.3 |  |  | 10.2 |  |
| Queue Delay | 0.0 | 0.0 |  | 0.0 | 0.0 | 0.0 |  | 0.0 |  |  | 0.0 |  |
| Total Delay | 8.2 | 10.0 |  | 8.3 | 10.9 | 2.5 |  | 9.3 |  |  | 10.2 |  |
| LOS | A | B |  | A | B | A |  | A |  |  | B |  |
| Approach Delay |  | 9.9 |  |  | 10.1 |  |  | 9.3 |  |  | 10.2 |  |
| Approach LOS |  | A |  |  | B |  |  | A |  |  | B |  |
| Queue Length 50th (ft) | 4 | 59 |  | 6 | 74 | 0 |  | 13 |  |  | 18 |  |
| Queue Length 95th (ti) | 15 | 105 |  | 19 | 128 | 8 |  | 43 |  |  | 51 |  |

Baseline Synchro 10 Light Report
Page 2


| Synchro Model 9: US-36 \& N. 10th St. |  |  |  |  | 2017 PM Peak (Existing Operating Conditions) Lanes, Volumes, Timings |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $\lambda$ |  |  | $\checkmark$ | $\leftarrow$ |  |  | $\uparrow$ |  |  |  | $\downarrow$ |
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | 7 | $\dagger$ |  | 7 | ¢ |  |  | ¢ |  |  | ¢ |  |
| Traffic Volume (vph) | 7 | 325 | 46 | 112 | 386 |  | 50 | 15 | 126 | 4 | 12 | 11 |
| Future Volume (vph) | 7 | 325 | 46 | 112 | 386 | 8 | 50 | 15 | 126 | 4 | 12 | 11 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Storage Length (ti) | 65 |  | 0 | 60 |  | 0 | 0 |  | 0 | 0 |  | 0 |
| Storage Lanes | 1 |  | 0 | 1 |  | 0 | 0 |  | 0 | 0 |  | 0 |
| Taper Length ( f ) | 25 |  |  | 25 |  |  | 25 |  |  | 25 |  |  |
| Lane Uutil. Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Fit |  | 0.981 |  |  | 0.997 |  |  | 0.911 |  |  | 0.944 |  |
| Fil Protected | 0.950 |  |  | 0.950 |  |  |  | 0.987 |  |  | 0.993 |  |
| Satd. Flow (prot) | 1770 | 1827 | 0 | 1770 | 1857 | 0 | 0 | 1675 | 0 | 0 | 1746 | 0 |
| Fit Permitted | 0.357 |  |  | 0.385 |  |  |  | 0.916 |  |  | 0.963 |  |
| Satd. Flow (perm) | 665 | 1827 | 0 | 717 | 1857 | 0 | 0 | 1554 | 0 | 0 | 1693 | 0 |
| Right Tum on Red |  |  | Yes |  |  | Yes |  |  | Yes |  |  | Yes |
| Satd. Flow (RTOR) |  | 11 |  |  | 2 |  |  | 128 |  |  | 12 |  |
| Link Speed (mph) |  | 30 |  |  | 30 |  |  | 20 |  |  | 30 |  |
| Link Distance ( t ) |  | 680 |  |  | 349 |  |  | 478 |  |  | 553 |  |
| Travel Time (s) |  | 15.5 |  |  | 7.9 |  |  | 16.3 |  |  | 12.6 |  |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Adj. Flow (vph) | 8 | 353 | 50 | 122 | 420 | 9 | 54 | 16 | 137 | 4 | 13 | 12 |
| Shared Lane Traffic (\%) |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane Group Flow (vph) | 8 | 403 | 0 | 122 | 429 | 0 | 0 | 207 | 0 | 0 | 29 | 0 |
| Turn Type | pm+pt | NA |  | pm+pt | NA |  | Perm | NA |  | Perm | NA |  |
| Protected Phases | 7 | 4 |  | 3 | 8 |  |  | 2 |  |  | 6 |  |
| Permitted Phases | 4 |  |  | 8 |  |  | 2 |  |  | 6 |  |  |
| Minimum Split (s) | 10.0 | 23.0 |  | 10.0 | 23.0 |  | 23.0 | 23.0 |  | 23.0 | 23.0 |  |
| Total Split (s) | 15.0 | 35.0 |  | 15.0 | 35.0 |  | 25.0 | 25.0 |  | 25.0 | 25.0 |  |
| Total Split (\%) | 20.0\% | 46.7\% |  | 20.0\% | 46.7\% |  | 33.3\% | 33.3\% |  | 33.3\% | 33.3\% |  |
| Maximum Green (s) | 10.0 | 30.0 |  | 10.0 | 30.0 |  | 20.0 | 20.0 |  | 20.0 | 20.0 |  |
| Yellow Time (s) | 3.0 | 3.0 |  | 3.0 | 3.0 |  | 3.0 | 3.0 |  | 3.0 | 3.0 |  |
| All-Red Time (s) | 2.0 | 2.0 |  | 2.0 | 2.0 |  | 2.0 | 2.0 |  | 2.0 | 2.0 |  |
| Lost Time Adjust (s) | 0.0 | 0.0 |  | 0.0 | 0.0 |  |  | 0.0 |  |  | 0.0 |  |
| Total Lost Time (s) | 5.0 | 5.0 |  | 5.0 | 5.0 |  |  | 5.0 |  |  | 5.0 |  |
| Lead/lag | Lead | Lag |  | Lead | Lag |  |  |  |  |  |  |  |
| Lead-Lag Optimize? | Yes | Yes |  | Yes | Yes |  |  |  |  |  |  |  |
| Walk Time (s) |  | 7.0 |  |  | 7.0 |  | 7.0 | 7.0 |  | 7.0 | 7.0 |  |
| Flash Dont Walk (s) |  | 11.0 |  |  | 11.0 |  | 11.0 | 11.0 |  | 11.0 | 11.0 |  |
| Pedestrian Calls (\#\#hr) |  | 0 |  |  | 0 |  | 0 | 0 |  | 0 | 0 |  |
| Act Efflt Green (s) | 40.0 | 30.0 |  | 40.0 | 30.0 |  |  | 20.0 |  |  | 20.0 |  |
| Actuatedg/C Ratio | 0.53 | 0.40 |  | 0.53 | 0.40 |  |  | 0.27 |  |  | 0.27 |  |
| v/c Ratio | 0.02 | 0.55 |  | 0.23 | 0.58 |  |  | 0.41 |  |  | 0.06 |  |
| Control Delay | 6.3 | 20.2 |  | 7.9 | 21.3 |  |  | 12.1 |  |  | 15.3 |  |
| Queue Delay | 0.0 | 0.0 |  | 0.0 | 0.0 |  |  | 0.0 |  |  | 0.0 |  |
| Total Delay | 6.3 | 20.2 |  | 7.9 | 21.3 |  |  | 12.1 |  |  | 15.3 |  |
| LOS | A | C |  | A | C |  |  | B |  |  | B |  |
| Approach Delay |  | 19.9 |  |  | 18.3 |  |  | 12.1 |  |  | 15.3 |  |
| Approach LOS |  | B |  |  | B |  |  | B |  |  | B |  |
| Queue Length 50th (fit) | 1 | 136 |  | 22 | 150 |  |  | 28 |  |  | 6 |  |
| Queue Length 95th (ft) | 6 | 219 |  | 43 | 239 |  |  | 83 |  |  | 25 |  |
| Baseline |  |  |  |  |  |  |  |  |  | Synchro | 10 Ligh | Report |



| Synchro Model 15: US-36 \& N. 14th St. |  |  |  |  | 2017 PM Peak (Existing Operating Conditions) |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $\gamma$ |  |  | 1 | $\leftarrow$ | 4 |  | $\uparrow$ | $p$ |  |  | $\downarrow$ |
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | 7 | $\hat{\beta}$ |  | 7 | $\dagger$ |  |  | ¢ |  |  | ¢ |  |
| Traffic Volume (vph) | 9 | 456 | 19 | 11 | 500 | 11 | 14 | 7 | 20 | 21 | 12 | 11 |
| Future Volume (vph) | 9 | 456 | 19 | 11 | 500 | 11 | 14 | 7 | 20 | 21 | 12 | 11 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Storage Length (ft) | 125 |  | 0 | 75 |  | 0 | 0 |  | 0 | 0 |  | 0 |
| Storage Lanes | 1 |  | 0 | 1 |  | 0 | 0 |  | 0 | 0 |  | 0 |
| Taper Length ( f ) | 25 |  |  | 25 |  |  | 25 |  |  | 25 |  |  |
| Lane Util. Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Fit |  | 0.994 |  |  | 0.997 |  |  | 0.934 |  |  | 0.966 |  |
| Fit Protected | 0.950 |  |  | 0.950 |  |  |  | 0.984 |  |  | 0.977 |  |
| Satd. Flow (prot) | 1770 | 1852 | 0 | 1770 | 1857 | 0 | 0 | 1712 | 0 | 0 | 1758 | 0 |
| Fit Permitted | 0.361 |  |  | 0.391 |  |  |  | 0.924 |  |  | 0.885 |  |
| Satd. Flow (perm) | 672 | 1852 | 0 | 728 | 1857 | 0 | 0 | 1608 | 0 | 0 | 1592 | 0 |
| Right Tum on Red |  |  | Yes |  |  | Yes |  |  | Yes |  |  | Yes |
| Satd. Flow (RTOR) |  | 5 |  |  | 3 |  |  | 22 |  |  | 12 |  |
| Link Speed (mph) |  | 30 |  |  | 30 |  |  | 20 |  |  | 30 |  |
| Link Distance (ti) |  | 1029 |  |  | 341 |  |  | 457 |  |  | 627 |  |
| Travel Time (s) |  | 23.4 |  |  | 7.8 |  |  | 15.6 |  |  | 14.3 |  |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Adj. Flow (vph) | 10 | 496 | 21 | 12 | 543 | 12 | 15 | 8 | 22 | 23 | 13 | 12 |
| Shared Lane Traficic (\%) |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane Group Flow (vph) | 10 | 517 | 0 | 12 | 555 | 0 | 0 | 45 | 0 | 0 | 48 | 0 |
| Turn Type | Perm | NA |  | Perm | NA |  | Perm | NA |  | Perm | NA |  |
| Prolected Phases |  | 4 |  |  | 8 |  |  | 2 |  |  | 6 |  |
| Permitted Phases | 4 |  |  | 8 |  |  | 2 |  |  | 6 |  |  |
| Minimum Split (s) | 24.0 | 24.0 |  | 24.0 | 24.0 |  | 23.0 | 23.0 |  | 23.0 | 23.0 |  |
| Total Split (s) | 39.0 | 39.0 |  | 39.0 | 39.0 |  | 23.0 | 23.0 |  | 23.0 | 23.0 |  |
| Total Split (\%) | 62.9\% | 62.9\% |  | 62.9\% | 62.9\% |  | 37.1\% | 37.1\% |  | 37.1\% | 37.1\% |  |
| Maximum Green (s) | 33.0 | 33.0 |  | 33.0 | 33.0 |  | 18.0 | 18.0 |  | 18.0 | 18.0 |  |
| Yellow Time (s) | 4.0 | 4.0 |  | 4.0 | 4.0 |  | 4.0 | 4.0 |  | 4.0 | 4.0 |  |
| All-Red Time (s) | 2.0 | 2.0 |  | 2.0 | 2.0 |  | 1.0 | 1.0 |  | 1.0 | 1.0 |  |
| Lost Time Adjust (s) | 0.0 | 0.0 |  | 0.0 | 0.0 |  |  | 0.0 |  |  | 0.0 |  |
| Total Lost Time (s) | 6.0 | 6.0 |  | 6.0 | 6.0 |  |  | 5.0 |  |  | 5.0 |  |
| Lead/Lag |  |  |  |  |  |  |  |  |  |  |  |  |
| Lead-Lag Optimize? |  |  |  |  |  |  |  |  |  |  |  |  |
| Walk Time (s) | 7.0 | 7.0 |  | 7.0 | 7.0 |  | 7.0 | 7.0 |  | 7.0 | 7.0 |  |
| Flash Dont Walk (s) | 11.0 | 11.0 |  | 11.0 | 11.0 |  | 11.0 | 11.0 |  | 11.0 | 11.0 |  |
| Pedestrian Calls (\#\#hr) | 0 | 0 |  | 0 | 0 |  | 0 | 0 |  | 0 | 0 |  |
| Act Efflt Green (s) | 33.0 | 33.0 |  | 33.0 | 33.0 |  |  | 18.0 |  |  | 18.0 |  |
| Actuatedg/C Ratio | 0.53 | 0.53 |  | 0.53 | 0.53 |  |  | 0.29 |  |  | 0.29 |  |
| vic Ratio | 0.03 | 0.52 |  | 0.03 | 0.56 |  |  | 0.09 |  |  | 0.10 |  |
| Control Delay | 7.2 | 11.7 |  | 7.3 | 12.4 |  |  | 11.1 |  |  | 13.8 |  |
| Queue Delay | 0.0 | 0.0 |  | 0.0 | 0.0 |  |  | 0.0 |  |  | 0.0 |  |
| Total Delay | 7.2 | 11.7 |  | 7.3 | 12.4 |  |  | 11.1 |  |  | 13.8 |  |
| LOS | A | B |  | A | B |  |  | B |  |  | B |  |
| Approach Delay |  | 11.6 |  |  | 12.3 |  |  | 11.1 |  |  | 13.8 |  |
| Approach LOS |  | B |  |  | B |  |  | B |  |  | B |  |
| Queue Length 50th (ft) | 2 | 113 |  | 2 | 126 |  |  | 6 |  |  | 10 |  |
| Queue Length 95th (ft) | 8 | 188 |  | 9 | 207 |  |  | 26 |  |  | 31 |  |

Baseline Synchro 10 Light Report Page 7


| Synchro Model 18: US-36 \& N. 15th |  |  |  |  | 2017 PM Peak (Existing Operating Conditions) HCM Unsignalized Intersection Capacity Analysis |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $\rangle$ |  |  | $\checkmark$ |  |  | 4 | $\uparrow$ |  |  | $\downarrow$ | $\downarrow$ |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | 7 | ¢ |  | 7 | $\dagger$ |  |  | ¢ |  |  | ¢ |  |
| Traffic Volume (veh/h) | 49 | 428 | 11 | 20 | 499 | 34 | 3 | 11 | 8 | 9 | 4 | 48 |
| Future Volume (Veh/h) | 49 | 428 | 11 | 20 | 499 | 34 | 3 | 11 | 8 | 9 | 4 | 48 |
| Sign Control |  | Free |  |  | Free |  |  | Stop |  |  | Stop |  |
| Grade |  | 0\% |  |  | 0\% |  |  | 0\% |  |  | 0\% |  |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Hourly flow rate (vph) | 53 | 465 | 12 | 22 | 542 | 37 | 3 | 12 | 9 | 10 | 4 | 52 |
| Pedestrians |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane Width (ft) |  |  |  |  |  |  |  |  |  |  |  |  |
| Walking Speed (t/s) |  |  |  |  |  |  |  |  |  |  |  |  |
| Percent Blockage |  |  |  |  |  |  |  |  |  |  |  |  |
| Right turn flare (veh) |  |  |  |  |  |  |  |  |  |  |  |  |
| Median type |  | WLTL |  |  | TWLTL |  |  |  |  |  |  |  |
| Median storage veh) |  | 2 |  |  | , |  |  |  |  |  |  |  |
| Upstream signal (fi) |  | 341 |  |  |  |  |  |  |  |  |  |  |
| pX, platoon unblocked |  |  |  | 0.83 |  |  | 0.83 | 0.83 | 0.83 | 0.83 | 0.83 |  |
| vC , conflicting volume | 579 |  |  | 477 |  |  | 1217 | 1200 | 471 | 1190 | 1188 | 560 |
| VC1, stage 1 conf vol |  |  |  |  |  |  | 577 | 577 |  | 604 | 604 |  |
| vC2, stage 2 conf vol |  |  |  |  |  |  | 640 | 623 |  | 586 | 583 |  |
| vCu , unblocked vol | 579 |  |  | 273 |  |  | 1161 | 1140 | 266 | 1129 | 1125 | 560 |
| IC, single (s) | 4.1 |  |  | 4.1 |  |  | 7.1 | 6.5 | 6.2 | 7.1 | 6.5 | 6.2 |
| IC, 2 stage (s) |  |  |  |  |  |  | 6.1 | 5.5 |  | 6.1 | 5.5 |  |
| tF (s) | 2.2 |  |  | 2.2 |  |  | 3.5 | 4.0 | 3.3 | 3.5 | 4.0 | 3.3 |
| po queve free \% | 95 |  |  | 98 |  |  | 99 | 96 | 99 | 97 | 99 | 90 |
| cM capacity (veh/h) | 995 |  |  | 1076 |  |  | 302 | 338 | 644 | 346 | 354 | 527 |
| Direction, Lane \# | EB1 | EB 2 | WB 1 | WB2 | NB 1 | S8 1 |  |  |  |  |  |  |
| Volume Total | 53 | 477 | 22 | 579 | 24 | 66 |  |  |  |  |  |  |
| Volume Left | 53 | 0 | 22 | 0 | 3 | 10 |  |  |  |  |  |  |
| Volume Right | 0 | 12 | 0 | 37 | 9 | 52 |  |  |  |  |  |  |
| CSH | 995 | 1700 | 1076 | 1700 | 404 | 475 |  |  |  |  |  |  |
| Volume to Capacity | 0.05 | 0.28 | 0.02 | 0.34 | 0.06 | 0.14 |  |  |  |  |  |  |
| Queue Length 95 th (ti) | 4 | 0 | 2 | 0 | 5 | 12 |  |  |  |  |  |  |
| Control Delay (s) | 8.8 | 0.0 | 8.4 | 0.0 | 14.5 | 13.8 |  |  |  |  |  |  |
| Lane LOS | A |  | A |  | B | B |  |  |  |  |  |  |
| Approach Delay (s) | 0.9 |  | 0.3 |  | 14.5 | 13.8 |  |  |  |  |  |  |
| Approach LOS |  |  |  |  | B | B |  |  |  |  |  |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |
| Average Delay |  |  | 1.6 |  |  |  |  |  |  |  |  |  |
| Intersection Capacity Utilization |  |  | 46.7\% |  | CU Level | Service |  |  | A |  |  |  |
| Analysis Period (min) |  |  | 15 |  |  |  |  |  |  |  |  |  |

Baseline | Synchro 10 Light Report |
| ---: |
| Page 3 |

| Synchro Model <br> 21: US-36 \& N. 17th |  |  |  | 2017 PM Peak (Existing Operating Conditions) HCM Unsignalized Intersection Capacity Analysis |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $\gamma$ |  |  | 7 |  | 4 | 4 | $\uparrow$ | $p$ |  | $\downarrow$ | $\downarrow$ |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | 7 | 今 |  |  | ¢ |  |  | ¢ |  |  | ¢ |  |
| Traffic Volume (veh/h) | 7 | 493 | 10 | 15 | 522 | 5 | 16 | 1 | 12 | 7 | 1 | 13 |
| Future Volume (Veh/h) | 7 | 493 | 10 | 15 | 522 | 5 | 16 | 1 | 12 | 7 | 1 | 13 |
| Sign Control |  | Free |  |  | Free |  |  | Stop |  |  | Stop |  |
| Grade |  | 0\% |  |  | 0\% |  |  | 0\% |  |  | 0\% |  |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Hourly flow rate (vph) | 8 | 536 | 11 | 16 | 567 | 5 | 17 | 1 | 13 | 8 | , | 14 |
| Pedestrians |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane Width (fi) |  |  |  |  |  |  |  |  |  |  |  |  |
| Walking Speed (tts) |  |  |  |  |  |  |  |  |  |  |  |  |
| Percent Blockage |  |  |  |  |  |  |  |  |  |  |  |  |
| Right turn flare (veh) |  |  |  |  |  |  |  |  |  |  |  |  |
| Median type |  | TWLTL |  |  | None |  |  |  |  |  |  |  |
| Median storage veh) |  | 2 |  |  |  |  |  |  |  |  |  |  |
| Upstream signal (ft) |  | 1068 |  |  | 971 |  |  |  |  |  |  |  |
| pX, platoon unblocked |  |  |  | 0.92 |  |  | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |  |
| VC, conflicting volume | 572 |  |  | 547 |  |  | 1174 | 1162 | 542 | 1167 | 1164 | 570 |
| VC1, stage 1 conf vol |  |  |  |  |  |  | 558 | 558 |  | 602 | 602 |  |
| vC2, slage 2 conf vol |  |  |  |  |  |  | 616 | 604 |  | 566 | 563 |  |
| vCu , unblocked vol | 572 |  |  | 462 |  |  | 1144 | 1131 | 456 | 1137 | 1135 | 570 |
| IC, single (s) | 4.1 |  |  | 4.1 |  |  | 7.1 | 6.5 | 6.2 | 7.1 | 6.5 | 6.2 |
| IC, 2 stage (s) |  |  |  |  |  |  | 6.1 | 5.5 |  | 6.1 | 5.5 |  |
| tF (s) | 2.2 |  |  | 2.2 |  |  | 3.5 | 4.0 | 3.3 | 3.5 | 4.0 | 3.3 |
| po queue free \% | 99 |  |  | 98 |  |  | 95 | 100 | 98 | 98 | 100 | 97 |
| cM capacity (veh h ) | 1001 |  |  | 1009 |  |  | 362 | 377 | 555 | 365 | 375 | 521 |
| Direction, Lane\# | EB 1 | EB2 | WB 1 | NB1 | SB 1 |  |  |  |  |  |  |  |
| Volume Total | 8 | 547 | 588 | 31 | 23 |  |  |  |  |  |  |  |
| Volume Left | 8 | 0 | 16 | 17 | 8 |  |  |  |  |  |  |  |
| Volume Right | 0 | 11 | 5 | 13 | 14 |  |  |  |  |  |  |  |
| CSH | 1001 | 1700 | 1009 | 425 | 447 |  |  |  |  |  |  |  |
| Volume to Capacity | 0.01 | 0.32 | 0.02 | 0.07 | 0.05 |  |  |  |  |  |  |  |
| Queue Length 95th (ti) | 1 | 0 | 1 | 6 | 4 |  |  |  |  |  |  |  |
| Control Delay (s) | 8.6 | 0.0 | 0.4 | 14.1 | 13.5 |  |  |  |  |  |  |  |
| Lane LOS | A |  | A | B | B |  |  |  |  |  |  |  |
| Approach Delay (s) | 0.1 |  | 0.4 | 14.1 | 13.5 |  |  |  |  |  |  |  |
| Approach LOS |  |  |  | B | B |  |  |  |  |  |  |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |
| Average Delay |  |  | 0.9 |  |  |  |  |  |  |  |  |  |
| Intersection Capacity Utilization |  |  | 49.9\% |  | CU Level | S Service |  |  | A |  |  |  |
| Analysis Period (min) |  |  | 15 |  |  |  |  |  |  |  |  |  |


| Baseline | Synchro 10 Light Report |
| ---: | ---: |
| Page 4 |  |


| Synchro Model 27: US-36 \& 11th Rd. |  |  |  |  |  | PM F | eak HCN | xistir Unsigne | Ope <br> ed Inte |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 7 |  |  | 1 |  |  | 4 | $\uparrow$ | $p$ |  | $\downarrow$ | $\downarrow$ |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | 7 | $\dagger$ |  | 1 | 今 |  |  | 4 | $\overline{7}$ |  | 4 | 「 |
| Traffic Volume (veh/h) | 14 | 323 | 56 | 17 | 323 | 29 | 27 | , | 25 | 14 | 3 | 6 |
| Future Volume (Veh/h) | 14 | 323 | 56 | 17 | 323 | 29 | 27 | 4 | 25 | 14 | 3 | 6 |
| Sign Control |  | Free |  |  | Free |  |  | Stop |  |  | Stop |  |
| Grade |  | 0\% |  |  | 0\% |  |  | 0\% |  |  | 0\% |  |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Hourly flow rate (vph) | 15 | 351 | 61 | 18 | 351 | 32 | 29 | 4 | 27 | 15 | 3 | 7 |
| Pedestrians |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane Width (ti) |  |  |  |  |  |  |  |  |  |  |  |  |
| Walking Speed (ft/s) |  |  |  |  |  |  |  |  |  |  |  |  |
| Percent Blockage |  |  |  |  |  |  |  |  |  |  |  |  |
| Right turn flare (veh) |  |  |  |  |  |  |  |  | 3 |  |  | 4 |
| Median type |  | TWLTL |  |  | TWLTL |  |  |  |  |  |  |  |
| Median storage veh) |  | 2 |  |  | 2 |  |  |  |  |  |  |  |
| Upstream signal (ft) |  |  |  |  |  |  |  |  |  |  |  |  |
| pX, platoon unblocked |  |  |  |  |  |  |  |  |  |  |  |  |
| vC, conflicting volume | 383 |  |  | 412 |  |  | 804 | 830 | 382 | 800 | 845 | 367 |
| vC1, stage 1 conf vol |  |  |  |  |  |  | 412 | 412 |  | 403 | 403 |  |
| vC2, stage 2 conf vol |  |  |  |  |  |  | 392 | 419 |  | 396 | 442 |  |
| vCu , unblocked vol | 383 |  |  | 412 |  |  | 804 | 830 | 382 | 800 | 845 | 367 |
| tC, single (s) | 4.1 |  |  | 4.1 |  |  | 7.1 | 6.5 | 6.2 | 7.1 | 6.5 | 6.2 |
| tC, 2 stage (s) |  |  |  |  |  |  | 6.1 | 5.5 |  | 6.1 | 5.5 |  |
| tF (s) | 2.2 |  |  | 2.2 |  |  | 3.5 | 4.0 | 3.3 | 3.5 | 4.0 | 3.3 |
| po queue free \% | 99 |  |  | 98 |  |  | 94 | 99 | 96 | 97 | 99 | 99 |
| cM capacity (veh/h) | 1175 |  |  | 1147 |  |  | 487 | 471 | 666 | 478 | 465 | 678 |
| Direction, Lane \# | EB 1 | EB 2 | WB 1 | WB 2 | NB 1 | SB 1 |  |  |  |  |  |  |
| Volume Total | 15 | 412 | 18 | 383 | 60 | 25 |  |  |  |  |  |  |
| Volume Left | 15 | 0 | 18 | 0 | 29 | 15 |  |  |  |  |  |  |
| Volume Right | 0 | 61 | 0 | 32 | 27 | 7 |  |  |  |  |  |  |
| cSH | 1175 | 1700 | 1147 | 1700 | 883 | 660 |  |  |  |  |  |  |
| Volume to Capacity | 0.01 | 0.24 | 0.02 | 0.23 | 0.07 | 0.04 |  |  |  |  |  |  |
| Queue Length 95th (tt) | 1 | 0 | 1 | 0 | 5 | 3 |  |  |  |  |  |  |
| Control Delay (s) | 8.1 | 0.0 | 8.2 | 0.0 | 11.9 | 12.2 |  |  |  |  |  |  |
| Lane LOS | A |  | A |  | B | B |  |  |  |  |  |  |
| Approach Delay (s) | 0.3 |  | 0.4 |  | 11.9 | 12.2 |  |  |  |  |  |  |
| Approach LOS |  |  |  |  | B | B |  |  |  |  |  |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |
| Average Delay |  |  | 1.4 |  |  |  |  |  |  |  |  |  |
| Intersection Capacity Utilization |  |  | 37.1\% |  | Level | Service |  |  | A |  |  |  |
| Analysis Period (min) |  |  | 15 |  |  |  |  |  |  |  |  |  |


| Baseline | Synchro 10 Light Report |
| ---: | ---: |
| Page 5 |  |

## C. 32037 AM PEAK HOUR (EXISTING OPERATING CONDITIONS)

| Synchro Model6: US-36 \& N. 8th St. |  |  |  |  | 2037 AM Peak (Existing Operating Conditions) |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $\gamma$ | $\rightarrow$ |  | 7 | $\leftarrow$ | 4 | 4 | $\uparrow$ |  |  | $\downarrow$ | $\checkmark$ |
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | $\dagger$ | $\dagger$ |  | \% | $\uparrow$ | 7 |  | \$ |  |  | $\dagger$ |  |
| Traffic Volume (vph) | 44 | 334 | 40 | 22 | 232 | 16 | 9 | 15 | 3 | 28 | 30 | 22 |
| Future Volume (vph) | 44 | 334 | 40 | 22 | 232 | 16 | 9 | 15 | 3 | 28 | 30 | 22 |
| \|deal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Storage Length (ft) | 85 |  | 0 | 75 |  | 75 | 0 |  | 0 | 0 |  | 0 |
| Storage Lanes | 1 |  | 0 | 1 |  | 1 | 0 |  | 0 |  |  | 0 |
| Taper Length (fit) | 25 |  |  | 25 |  |  | 25 |  |  | 25 |  |  |
| Lane Util. Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Fit |  | 0.984 |  |  |  | 0.850 |  | 0.986 |  |  | 0.963 |  |
| Fll Protected | 0.950 |  |  | 0.950 |  |  |  | 0.983 |  |  | 0.983 |  |
| Satd. Flow (prot) | 1770 | 1833 | 0 | 1770 | 1863 | 1583 | 0 | 1805 | 0 | 0 | 1763 | 0 |
| Fll Permitted | 0.603 |  |  | 0.458 |  |  |  | 0.926 |  |  | 0.915 |  |
| Satd. Flow (perm) | 1123 | 1833 | 0 | 853 | 1863 | 1583 | 0 | 1701 | 0 | 0 | 1641 | 0 |
| Right Tum on Red |  |  | Yes |  |  | Yes |  |  | Yes |  |  | Yes |
| Satd. Flow (RTOR) |  | 14 |  |  |  | 36 |  | 3 |  |  | 24 |  |
| Link Speed (mph) |  | 30 |  |  | 30 |  |  | 20 |  |  | 20 |  |
| Link Distance (fi) |  | 694 |  |  | 680 |  |  | 497 |  |  | 526 |  |
| Travel Time (s) |  | 15.8 |  |  | 15.5 |  |  | 16.9 |  |  | 17.9 |  |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Adj. Flow (vph) | 48 | 363 | 43 | 24 | 252 | 17 | 10 | 16 | 3 | 30 | 33 | 24 |
| Shared Lane Traficic (\%) |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane Group Flow (vph) | 48 | 406 | 0 | 24 | 252 | 17 | 0 | 29 | 0 | 0 | 87 | 0 |
| Turn Type | Perm | NA |  | Perm | NA | Perm | Perm | NA |  | Perm | NA |  |
| Protected Phases |  | 4 |  |  | 8 |  |  | 2 |  |  | , |  |
| Permitted Phases | 4 |  |  | 8 |  | 8 | 2 |  |  | 6 |  |  |
| Minimum Split (s) | 23.0 | 23.0 |  | 23.0 | 23.0 | 23.0 | 23.0 | 23.0 |  | 23.0 | 23.0 |  |
| Total Split (s) | 35.0 | 35.0 |  | 35.0 | 35.0 | 35.0 | 25.0 | 25.0 |  | 25.0 | 25.0 |  |
| Total Split (\%) | 58.3\% | 58.3\% |  | 58.3\% | 58.3\% | 58.3\% | 41.7\% | 41.7\% |  | 41.7\% | 41.7\% |  |
| Yellow Time (s) | 4.0 | 4.0 |  | 4.0 | 4.0 | 4.0 | 3.0 | 3.0 |  | 3.0 | 3.0 |  |
| All-Red Time (s) | 1.0 | 1.0 |  | 1.0 | 1.0 | 1.0 | 2.0 | 2.0 |  | 2.0 | 2.0 |  |
| Lost Time Adjust (s) | 0.0 | 0.0 |  | 0.0 | 0.0 | 0.0 |  | 0.0 |  |  | 0.0 |  |
| Total Lost Time (s) | 5.0 | 5.0 |  | 5.0 | 5.0 | 5.0 |  | 5.0 |  |  | 5.0 |  |
| Lead/Lag |  |  |  |  |  |  |  |  |  |  |  |  |
| Lead-Lag Optimize? |  |  |  |  |  |  |  |  |  |  |  |  |
| Act Effict Green (s) | 30.0 | 30.0 |  | 30.0 | 30.0 | 30.0 |  | 20.0 |  |  | 20.0 |  |
| Actuated g/C Ratio | 0.50 | 0.50 |  | 0.50 | 0.50 | 0.50 |  | 0.33 |  |  | 0.33 |  |
| vic Ratio | 0.09 | 0.44 |  | 0.06 | 0.27 | 0.02 |  | 0.05 |  |  | 0.15 |  |
| Control Delay | 8.4 | 11.1 |  | 8.3 | 9.7 | 1.6 |  | 13.0 |  |  | 11.8 |  |
| Queue Delay | 0.0 | 0.0 |  | 0.0 | 0.0 | 0.0 |  | 0.0 |  |  | 0.0 |  |
| Total Delay | 8.4 | 11.1 |  | 8.3 | 9.7 | 1.6 |  | 13.0 |  |  | 11.8 |  |
| LOS | A | B |  | A | A | A |  | B |  |  | B |  |
| Approach Delay |  | 10.9 |  |  | 9.1 |  |  | 13.0 |  |  | 11.8 |  |
| Approach LOS |  | B |  |  | A |  |  | B |  |  | B |  |
| Queue Length 50th (fi) | 8 | 83 |  | 4 | 49 | 0 |  | 6 |  |  | 15 |  |
| Queue Length 95th (fi) | 23 | 143 |  | 14 | 87 | 5 |  | 21 |  |  | 42 |  |
| Intemal Link Dist (ft) |  | 614 |  |  | 600 |  |  | 417 |  |  | 446 |  |
| Turn Bay Length ( ft ) | 85 |  |  | 75 |  | 75 |  |  |  |  |  |  |
| Base Capacity (vph) | 561 | 923 |  | 426 | 931 | 809 |  | 569 |  |  | 563 |  |
| Starvation Cap Reductn | 0 | 0 |  | 0 | 0 | 0 |  | - |  |  | 0 |  |
| Baseline |  |  |  |  |  |  |  |  |  | Synchro | 10 Ligh | Report Page 2 |



| Synchro Model 12: US-36 \& N. 11th |  |  |  |  | 2037 AM Peak (Existing Operating Conditions) HCM Unsignalized Intersection Capacity Analysis |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $\lambda$ | $\rightarrow$ |  | $\checkmark$ |  |  | 4 | $\uparrow$ |  |  | $\downarrow$ | $\downarrow$ |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | 7 | 今 |  | \% | 今 |  |  | ¢ |  |  | ¢ |  |
| Traffic Volume (veh/h) | 16 | 392 | 3 | 34 | 432 | 36 | 3 | 3 | 16 | 11 | , | 15 |
| Future Volume (Veh/h) | 16 | 392 | 3 | 34 | 432 | 36 | 3 | 3 | 16 | 11 | , | 15 |
| Sign Control |  | Free |  |  | Free |  |  | Stop |  |  | Stop |  |
| Grade |  | 0\% |  |  | 0\% |  |  | 0\% |  |  | 0\% |  |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Hourly flow rate (vph) | 17 | 426 | 3 | 37 | 470 | 39 | , | 3 | 17 | 12 | 4 | 16 |
| Pedestrians |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane Width (fi) |  |  |  |  |  |  |  |  |  |  |  |  |
| Walking Speed (tts) |  |  |  |  |  |  |  |  |  |  |  |  |
| Percent Blockage |  |  |  |  |  |  |  |  |  |  |  |  |
| Right turn flare (veh) |  |  |  |  |  |  |  |  |  |  |  |  |
| Median type |  | None |  |  | TWLTL |  |  |  |  |  |  |  |
| Median storage veh) |  |  |  |  | 2 |  |  |  |  |  |  |  |
| Upstream signal (ft) |  | 349 |  |  | 1029 |  |  |  |  |  |  |  |
| pX, platoon unblocked | 0.91 |  |  |  |  |  | 0.91 | 0.91 |  | 0.91 | 0.91 | 0.91 |
| VC , conflicting volume | 509 |  |  | 429 |  |  | 1024 | 1044 | 428 | 1042 | 1026 | 490 |
| VC1, stage 1 conf vol |  |  |  |  |  |  | 462 | 462 |  | 564 | 564 |  |
| vC2, stage 2 conf vol |  |  |  |  |  |  | 562 | 583 |  | 478 | 463 |  |
| vCu , unblocked vol | 416 |  |  | 429 |  |  | 979 | 1002 | 428 | 999 | 982 | 395 |
| IC, single (s) | 4.1 |  |  | 4.1 |  |  | 7.1 | 6.5 | 6.2 | 7.1 | 6.5 | 6.2 |
| IC, 2 stage (s) |  |  |  |  |  |  | 6.1 | 5.5 |  | 6.1 | 5.5 |  |
| IF (s) | 2.2 |  |  | 2.2 |  |  | 3.5 | 4.0 | 3.3 | 3.5 | 4.0 | 3.3 |
| poqueve free \% | 98 |  |  | 97 |  |  | 99 | 99 | 97 | 97 | 99 | 97 |
| cM capacity (veh/h) | 1045 |  |  | 1130 |  |  | 396 | 395 | 627 | 389 | 399 | 598 |
| Direction, Lane\# | EB1 | EB2 | WB 1 | WB2 | NB 1 | SB 1 |  |  |  |  |  |  |
| Volume Total | 17 | 429 | 37 | 509 | 23 | 32 |  |  |  |  |  |  |
| Volume Left | 17 | 0 | 37 | 0 | 3 | 12 |  |  |  |  |  |  |
| Volume Right | , | 3 | 0 | 39 | 17 | 16 |  |  |  |  |  |  |
| CSH | 1045 | 1700 | 1130 | 1700 | 544 | 473 |  |  |  |  |  |  |
| Volume to Capacity | 0.02 | 0.25 | 0.03 | 0.30 | 0.04 | 0.07 |  |  |  |  |  |  |
| Queve Length 95th (f) | , | 0 | 3 | 0 | 3 | 5 |  |  |  |  |  |  |
| Control Delay (s) | 8.5 | 0.0 | 8.3 | 0.0 | 11.9 | 13.2 |  |  |  |  |  |  |
| Lane LOS | A |  | A |  | B | B |  |  |  |  |  |  |
| Approach Delay (s) | 0.3 |  | 0.6 |  | 11.9 | 13.2 |  |  |  |  |  |  |
| Approach LOS |  |  |  |  | B | B |  |  |  |  |  |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |
| Average Delay |  |  | 1.1 |  |  |  |  |  |  |  |  |  |
| Intersection Capacity Utilization |  |  | 38.7\% |  | CU Level | Service |  |  | A |  |  |  |
| Analysis Period (min) |  |  | 15 |  |  |  |  |  |  |  |  |  |

Baseline | Synchro 10 Light Report |
| ---: |
| Page 2 |

| Synchro Model 15: US-36 \& N. 14th St. |  |  |  |  | 2037 AM Peak (Existing Operating Conditions) Lanes, Volumes, Timings |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $\lambda$ |  |  | $\checkmark$ |  |  |  | $\uparrow$ |  |  |  | $\downarrow$ |
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | 7 | 今 |  | \% | $\dagger$ |  |  | ¢ |  |  | ¢ |  |
| Traffic Volume (vph) | 4 | 385 | 26 | 5 | 407 |  | 7 | , | 4 | 28 | , | 16 |
| Future Volume (vph) | 4 | 385 | 26 | 5 | 407 | 9 | 7 | 3 | 4 | 28 | 3 | 16 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Storage Length (ft) | 125 |  | 0 | 75 |  | 0 | 0 |  | 0 | 0 |  | 0 |
| Storage Lanes | 1 |  | 0 | 1 |  | 0 | 0 |  | 0 | 0 |  | 0 |
| Taper Length (ft) | 25 |  |  | 25 |  |  | 25 |  |  | 25 |  |  |
| Lane Util. Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Fit |  | 0.991 |  |  | 0.997 |  |  | 0.964 |  |  | 0.954 |  |
| Fil Protected | 0.950 |  |  | 0.950 |  |  |  | 0.974 |  |  | 0.971 |  |
| Sald. Flow (prot) | 1770 | 1846 | 0 | 1770 | 1857 | 0 | 0 | 1749 | 0 | 0 | 1726 | 0 |
| Fll Permitted | 0.445 |  |  | 0.450 |  |  |  | 0.904 |  |  | 0.863 |  |
| Satd. Flow (perm) | 829 | 1846 | 0 | 838 | 1857 | 0 | 0 | 1623 | 0 | 0 | 1534 | 0 |
| Right Tum on Red |  |  | Yes |  |  | Yes |  |  | Yes |  |  | Yes |
| Satd. Flow (RTOR) |  | 8 |  |  | 3 |  |  | 4 |  |  | 17 |  |
| Link Speed (mph) |  | 30 |  |  | 30 |  |  | 20 |  |  | 30 |  |
| Link Distance (fi) |  | 1029 |  |  | 341 |  |  | 457 |  |  | 627 |  |
| Travel Time (s) |  | 23.4 |  |  | 7.8 |  |  | 15.6 |  |  | 14.3 |  |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Adj. Flow (vph) | 4 | 418 | 28 | 5 | 442 | 10 | 8 | 3 | 4 | 30 | 3 | 17 |
| Shared Lane Traffic (\%) |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane Group Flow (vph) | 4 | 446 | 0 | 5 | 452 | 0 | 0 | 15 | 0 | 0 | 50 | 0 |
| Turn Type | Perm | NA |  | Perm | NA |  | Perm | NA |  | Perm | NA |  |
| Protected Phases |  | 4 |  |  | 8 |  |  | 2 |  |  | 6 |  |
| Permitted Phases | 4 |  |  | 8 |  |  | 2 |  |  | 6 |  |  |
| Minimum Split (s) | 24.0 | 24.0 |  | 24.0 | 24.0 |  | 23.0 | 23.0 |  | 23.0 | 23.0 |  |
| Total Split (s) | 39.0 | 39.0 |  | 39.0 | 39.0 |  | 23.0 | 23.0 |  | 23.0 | 23.0 |  |
| Total Split (\%) | 62.9\% | 62.9\% |  | 62.9\% | 62.9\% |  | 37.1\% | 37.1\% |  | 37.1\% | 37.1\% |  |
| Yellow Time (s) | 4.0 | 4.0 |  | 4.0 | 4.0 |  | 4.0 | 4.0 |  | 4.0 | 4.0 |  |
| All-Red Time (s) | 2.0 | 2.0 |  | 2.0 | 2.0 |  | 1.0 | 1.0 |  | 1.0 | 1.0 |  |
| Lost Time Adjust (s) | 0.0 | 0.0 |  | 0.0 | 0.0 |  |  | 0.0 |  |  | 0.0 |  |
| Total Lost Time (s) | 6.0 | 6.0 |  | 6.0 | 6.0 |  |  | 5.0 |  |  | 5.0 |  |
| Lead/Lag |  |  |  |  |  |  |  |  |  |  |  |  |
| Lead-Lag Optimize? |  |  |  |  |  |  |  |  |  |  |  |  |
| Act Efflt Green (s) | 33.0 | 33.0 |  | 33.0 | 33.0 |  |  | 18.0 |  |  | 18.0 |  |
| Actuated g/C Ratio | 0.53 | 0.53 |  | 0.53 | 0.53 |  |  | 0.29 |  |  | 0.29 |  |
| vic Ratio | 0.01 | 0.45 |  | 0.01 | 0.46 |  |  | 0.03 |  |  | 0.11 |  |
| Control Delay | 7.0 | 10.6 |  | 7.0 | 10.8 |  |  | 14.1 |  |  | 12.8 |  |
| Queue Delay | 0.0 | 0.0 |  | 0.0 | 0.0 |  |  | 0.0 |  |  | 0.0 |  |
| Total Delay | 7.0 | 10.6 |  | 7.0 | 10.8 |  |  | 14.1 |  |  | 12.8 |  |
| LOS | A | B |  | A | B |  |  | B |  |  | B |  |
| Approach Delay |  | 10.6 |  |  | 10.7 |  |  | 14.1 |  |  | 12.8 |  |
| Approach LOS |  | B |  |  | B |  |  | B |  |  | B |  |
| Queve Length 50th (t) | 1 | 92 |  | 1 | 95 |  |  | 3 |  |  | 9 |  |
| Queue Length 95th (fi) | 4 | 154 |  | 5 | 158 |  |  | 15 |  |  | 31 |  |
| Internal Link Dist (fi) |  | 949 |  |  | 261 |  |  | 377 |  |  | 547 |  |
| Turn Bay Length (ft) | 125 |  |  | 75 |  |  |  |  |  |  |  |  |
| Base Capacity (vph) | 441 | 986 |  | 446 | 989 |  |  | 474 |  |  | 457 |  |
| Starvation Cap Reductn | 0 | 0 |  | 0 | 0 |  |  | 0 |  |  | 0 |  |
| Baseline |  |  |  |  |  |  |  |  |  | Synchr | 10 Ligh | port |



Splits and Phases: $15:$ US-36 \& N. 14th St.


| Synchro Model 24: US-36 \& 20th St. |  |  |  |  | 2037 AM Peak (Existing Operating Conditions) |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $y$ |  |  | 1 | $\leftarrow$ | 4 | 4 | $\uparrow$ |  |  |  | $\checkmark$ |
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | 7 | $\dagger$ |  | \% | 今 |  |  | ¢ |  |  | 4 |  |
| Traffic Volume (vph) | 47 | 404 | 1 | 0 | 300 | 36 | 0 | , | 0 | 50 | 0 | 50 |
| Future Volume (vph) | 47 | 404 | 1 | 0 | 300 | 36 | 0 | 0 | 0 | 50 | 0 | 50 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Storage Length (ft) | 185 |  | 0 | 100 |  | 0 | 0 |  | 0 | 0 |  | 60 |
| Storage Lanes | 1 |  | 0 | 1 |  | 0 | 0 |  | 0 |  |  | 1 |
| Taper Length ( t ) | 25 |  |  | 25 |  |  | 25 |  |  | 25 |  |  |
| Lane Util. Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Fit |  |  |  |  | 0.984 |  |  |  |  |  |  | 0.850 |
| Fll Protected | 0.950 |  |  |  |  |  |  |  |  |  | 0.950 |  |
| Satd. Flow (prot) | 1770 | 1863 | 0 | 1863 | 1833 | 0 | 0 | 1863 | 0 | 0 | 1770 | 1583 |
| Flt Permitted | 0.544 |  |  |  |  |  |  |  |  |  | 0.889 |  |
| Satd. Flow (perm) | 1013 | 1863 | , | 1863 | 1833 | 0 | 0 | 1863 | 0 | 0 | 1656 | 1583 |
| Right Tum on Red |  |  | Yes |  |  | Yes |  |  | Yes |  |  | Yes |
| Satd. Flow (RTOR) |  |  |  |  | 14 |  |  |  |  |  |  | 68 |
| Link Speed (mph) |  | 30 |  |  | 30 |  |  | 30 |  |  | 30 |  |
| Link Distance ( ft ) |  | 971 |  |  | 3848 |  |  | 371 |  |  | 570 |  |
| Travel Time (s) |  | 22.1 |  |  | 87.5 |  |  | 8.4 |  |  | 13.0 |  |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Adj. Flow (vph) | 51 | 439 | 1 | 0 | 326 | 39 | 0 | 0 | 0 | 54 | 0 | 54 |
| Shared Lane Traffic (\%) |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane Group Flow (vph) | 51 | 440 | 0 | 0 | 365 | 0 | 0 | 0 | 0 | , | 54 | 54 |
| Turn Type | Perm | NA |  | Perm | NA |  |  |  |  | Perm | NA | Perm |
| Protected Phases |  | 4 |  |  | 8 |  |  | 2 |  |  | 6 |  |
| Permitted Phases | 4 |  |  | 8 |  |  | 2 |  |  | 6 |  | 6 |
| Detector Phase | 4 | 4 |  | 8 | 8 |  | 2 | 2 |  | 6 | 6 | 6 |
| Switch Phase |  |  |  |  |  |  |  |  |  |  |  |  |
| Minimum Initial (s) | 8.0 | 8.0 |  | 6.0 | 6.0 |  | 6.0 | 6.0 |  | 8.0 | 8.0 | 8.0 |
| Minimum Split (s) | 14.0 | 14.0 |  | 12.0 | 12.0 |  | 12.0 | 12.0 |  | 14.0 | 14.0 | 14.0 |
| Total Split (s) | 24.0 | 24.0 |  | 24.0 | 24.0 |  | 24.0 | 24.0 |  | 24.0 | 24.0 | 24.0 |
| Total Split (\%) | 50.0\% | 50.0\% |  | 50.0\% | 50.0\% |  | 50.0\% | 50.0\% |  | 50.0\% | 50.0\% | 50.0\% |
| Yellow Time (s) | 4.0 | 4.0 |  | 4.0 | 4.0 |  | 4.0 | 4.0 |  | 4.0 | 4.0 | 4.0 |
| All-Red Time (s) | 2.0 | 2.0 |  | 2.0 | 2.0 |  | 2.0 | 2.0 |  | 2.0 | 2.0 | 2.0 |
| Lost Time Adjust (s) | 0.0 | 0.0 |  | 0.0 | 0.0 |  |  | 0.0 |  |  | 0.0 | 0.0 |
| Total Lost Time (s) | 6.0 | 6.0 |  | 6.0 | 6.0 |  |  | 6.0 |  |  | 6.0 | 6.0 |
| Lead/Lag |  |  |  |  |  |  |  |  |  |  |  |  |
| Lead-Lag Optimize? |  |  |  |  |  |  |  |  |  |  |  |  |
| Recall Mode | Min | Min |  | Min | Min |  | None | None |  | None | None | None |
| Act Effit Green (s) | 23.7 | 23.7 |  |  | 23.7 |  |  |  |  |  | 8.3 | 8.3 |
| Actuated g/C Ratio | 0.68 | 0.68 |  |  | 0.68 |  |  |  |  |  | 0.24 | 0.24 |
| vic Ratio | 0.07 | 0.35 |  |  | 0.29 |  |  |  |  |  | 0.14 | 0.13 |
| Control Delay | 6.0 | 6.8 |  |  | 6.2 |  |  |  |  |  | 12.8 | 4.4 |
| Queue Delay | 0.0 | 0.0 |  |  | 0.0 |  |  |  |  |  | 0.0 | 0.0 |
| Total Delay | 6.0 | 6.8 |  |  | 6.2 |  |  |  |  |  | 12.8 | 4.4 |
| LOS | A | A |  |  | A |  |  |  |  |  | B | A |
| Approach Delay |  | 6.7 |  |  | 6.2 |  |  |  |  |  | 8.6 |  |
| Approach LOS |  | A |  |  | A |  |  |  |  |  | A |  |
| Queue Length 50th (ft) |  | 56 |  |  | 42 |  |  |  |  |  | 10 | 0 |
| Queue Length 95th (ft) | 18 | 113 |  |  | 89 |  |  |  |  |  | 28 | 15 |

Baseline
Synchro 10 Light Report
Page 11


| Synchro Model 27: US-36 \& 11th Rd. |  |  |  |  | 2037 AM Peak (Existing Operating Conditions) HCM Unsignalized Intersection Capacity Analysis |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 7 |  |  | 1 | $\leftarrow$ |  | 4 | $\uparrow$ | $p$ |  |  | $\checkmark$ |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | \% | $\dagger$ |  | \% | 今 |  |  | 4 | $\overline{7}$ |  | 4 | \% |
| Traffic Volume (veh/h) | 22 | 442 | 72 | 25 | 466 | 27 | 78 | 22 | 34 | 9 | 14 | 36 |
| Future Volume (Veh/h) | 22 | 442 | 72 | 25 | 466 | 27 | 78 | 22 | 34 | 9 | 14 | 36 |
| Sign Control |  | Free |  |  | Free |  |  | Stop |  |  | Stop |  |
| Grade |  | 0\% |  |  | 0\% |  |  | 0\% |  |  | 0\% |  |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Hourly flow rate (vph) | 24 | 480 | 78 | 27 | 507 | 29 | 85 | 24 | 37 | 10 | 15 | 39 |
| Pedestrians |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane Width (tt) |  |  |  |  |  |  |  |  |  |  |  |  |
| Walking Speed (fts) |  |  |  |  |  |  |  |  |  |  |  |  |
| Percent Blockage |  |  |  |  |  |  |  |  |  |  |  |  |
| Right turn flare (veh) |  |  |  |  |  |  |  |  | 3 |  |  | 4 |
| Median type |  | TWLTL |  |  | TWLTL |  |  |  |  |  |  |  |
| Median storage veh) |  | 2 |  |  | 2 |  |  |  |  |  |  |  |
| Upstream signal (ft) |  |  |  |  |  |  |  |  |  |  |  |  |
| pX, platoon unblocked |  |  |  |  |  |  |  |  |  |  |  |  |
| vC, conflicting volume | 536 |  |  | 558 |  |  | 1155 | 1157 | 519 | 1134 | 1182 | 522 |
| vC1, stage 1 conf vol |  |  |  |  |  |  | 567 | 567 |  | 576 | 576 |  |
| $\mathrm{vC2}$, stage 2 conf vol |  |  |  |  |  |  | 588 | 590 |  | 558 | 606 |  |
| vCu , unblocked vol | 536 |  |  | 558 |  |  | 1155 | 1157 | 519 | 1134 | 1182 | 522 |
| tC, single (s) | 4.1 |  |  | 4.1 |  |  | 7.1 | 6.5 | 6.2 | 7.1 | 6.5 | 6.2 |
| tC, 2 stage (s) |  |  |  |  |  |  | 6.1 | 5.5 |  | 6.1 | 5.5 |  |
| tF (s) | 2.2 |  |  | 2.2 |  |  | 3.5 | 4.0 | 3.3 | 3.5 | 4.0 | 3.3 |
| po queue free \% | 98 |  |  | 97 |  |  | 75 | 94 | 93 | 97 | 96 | 93 |
| cM capacity (veh/h) | 1032 |  |  | 1013 |  |  | 339 | 370 | 557 | 342 | 363 | 555 |
| Direction, Lane \# | EB 1 | EB 2 | WB 1 | WB 2 | NB 1 | SB 1 |  |  |  |  |  |  |
| Volume Total | 24 | 558 | 27 | 536 | 146 | 64 |  |  |  |  |  |  |
| Volume Left | 24 | 0 | 27 | 0 | 85 | 10 |  |  |  |  |  |  |
| Volume Right | 0 | 78 | 0 | 29 | 37 | 39 |  |  |  |  |  |  |
| cSH | 1032 | 1700 | 1013 | 1700 | 463 | 907 |  |  |  |  |  |  |
| Volume to Capacity | 0.02 | 0.33 | 0.03 | 0.32 | 0.32 | 0.07 |  |  |  |  |  |  |
| Queue Length 95th (ft) | 2 | 0 | 2 | 0 | 33 | 6 |  |  |  |  |  |  |
| Control Delay (s) | 8.6 | 0.0 | 8.7 | 0.0 | 18.1 | 13.5 |  |  |  |  |  |  |
| Lane LOS | A |  | A |  | c | B |  |  |  |  |  |  |
| Approach Delay (s) | 0.4 |  | 0.4 |  | 18.1 | 13.5 |  |  |  |  |  |  |
| Approach LOS |  |  |  |  | c | B |  |  |  |  |  |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |
| Average Delay |  |  | 2.9 |  |  |  |  |  |  |  |  |  |
| Intersection Capacity Utilization |  |  | 46.4\% |  | CU Level | Service |  |  | A |  |  |  |
| Analysis Period (min) |  |  | 15 |  |  |  |  |  |  |  |  |  |


| Baseline | Synchro 10 Light Report |
| ---: | ---: |
| Page 5 |  |

## C. 42037 PM PEAK HOUR (EXISTING OPERATING CONDITIONS)

| Synchro Model 3: US-36 \& N. 6th St. |  |  |  | 2037 PM Peak (Existing Operating Conditions) HCM Unsignalized Intersection Capacity Analysis |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $\lambda$ |  |  | 7 | $\leftarrow$ |  | 4 | $\uparrow$ |  | $\stackrel{\rightharpoonup}{*}$ |  | $\downarrow$ |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations |  | ¢ |  |  | ¢ |  |  | ¢ |  |  | ¢ |  |
| Traffic Volume (veh/h) | 11 | 290 | 19 | 48 | 498 | 34 | 35 | 20 | 57 | 22 | 4 | 5 |
| Future Volume (Veh/h) | 11 | 290 | 19 | 48 | 498 | 34 | 35 | 20 | 57 | 22 | 4 | 5 |
| Sign Control |  | Free |  |  | Free |  |  | Stop |  |  | Stop |  |
| Grade |  | 0\% |  |  | 0\% |  |  | 0\% |  |  | 0\% |  |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Hourly flow rate (vph) | 12 | 315 | 21 | 52 | 541 | 37 | 38 | 22 | 62 | 24 | 4 | 5 |
| Pedestrians |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane Width (fi) |  |  |  |  |  |  |  |  |  |  |  |  |
| Walking Speed (t/s) |  |  |  |  |  |  |  |  |  |  |  |  |
| Percent Blockage |  |  |  |  |  |  |  |  |  |  |  |  |
| Right tum flare (veh) |  |  |  |  |  |  |  |  |  |  |  |  |
| Median type |  | None |  |  | None |  |  |  |  |  |  |  |
| Median storage veh) |  |  |  |  |  |  |  |  |  |  |  |  |
| Upstream signal (fi) |  |  |  |  | 694 |  |  |  |  |  |  |  |
| pX, platoon unblocked | 0.90 |  |  |  |  |  | 0.90 | 0.90 |  | 0.90 | 0.90 | 0.90 |
| VC, conflicting volume | 578 |  |  | 336 |  |  | 1020 | 1032 | 326 | 1086 | 1024 | 560 |
| VC1, stage 1 conf vol |  |  |  |  |  |  |  |  |  |  |  |  |
| VC2, stage 2 conf vol |  |  |  |  |  |  |  |  |  |  |  |  |
| vCu , unblocked vol | 476 |  |  | 336 |  |  | 967 | 980 | 326 | 1040 | 971 | 455 |
| IC, single (s) | 4.1 |  |  | 4.1 |  |  | 7.1 | 6.5 | 6.2 | 7.1 | 6.5 | 6.2 |
| IC, 2 stage (s) |  |  |  |  |  |  |  |  |  |  |  |  |
| IF (s) | 2.2 |  |  | 2.2 |  |  | 3.5 | 4.0 | 3.3 | 3.5 | 4.0 | 3.3 |
| po queve free \% | 99 |  |  | 96 |  |  | 81 | 90 | 91 | 84 | 98 | 99 |
| cM capacity (veh h ) | 978 |  |  | 1223 |  |  | 197 | 213 | 716 | 151 | 215 | 545 |
| Direction, Lane\# | EB 1 | WB1 | NB 1 | SB 1 |  |  |  |  |  |  |  |  |
| Volume Total | 348 | 630 | 122 | 33 |  |  |  |  |  |  |  |  |
| Volume Left | 12 | 52 | 38 | 24 |  |  |  |  |  |  |  |  |
| Volume Right | 21 | 37 | 62 | 5 |  |  |  |  |  |  |  |  |
| cSH | 978 | 1223 | 319 | 177 |  |  |  |  |  |  |  |  |
| Volume to Capacity | 0.01 | 0.04 | 0.38 | 0.19 |  |  |  |  |  |  |  |  |
| Queue Length 95th (t) | 1 | 3 | 43 | 17 |  |  |  |  |  |  |  |  |
| Control Delay (s) | 0.4 | 1.1 | 23.1 | 29.9 |  |  |  |  |  |  |  |  |
| Lane LOS | A | A | c | D |  |  |  |  |  |  |  |  |
| Approach Delay (s) | 0.4 | 1.1 | 23.1 | 29.9 |  |  |  |  |  |  |  |  |
| Approach LOS |  |  | C | D |  |  |  |  |  |  |  |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |
| Average Delay |  |  | 4.1 |  |  |  |  |  |  |  |  |  |
| Intersection Capacity Utilization |  |  | 61.9\% |  | ULevel | Service |  |  | B |  |  |  |
| Analysis Period (min) |  |  | 15 |  |  |  |  |  |  |  |  |  |


| Synchro Model 6: US-36 \& N. 8th St. |  |  |  |  | 2037 PM Peak (Existing Operating Conditions) Lanes, Volumes, Timings |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $\gamma$ |  | 7 | 7 | $\longleftarrow$ | $\pm$ | 4 | $\uparrow$ | $p$ |  |  | 4 |
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | $\dagger$ | ¢ |  | \% | $\uparrow$ | $\overline{7}$ |  | ¢ |  |  | ¢ |  |
| Traffic Volume (vph) | 31 | 357 | 22 | 46 | 446 | 31 | 23 | 46 | 66 | 54 | 38 | 69 |
| Future Volume (vph) | 31 | 357 | 22 | 46 | 446 | 31 | 23 | 46 | 66 | 54 | 38 | 69 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Storage Length (ft) | 85 |  | 0 | 75 |  | 75 | 0 |  | 0 | 0 |  | 0 |
| Storage Lanes | 1 |  | 0 | 1 |  | 1 | 0 |  | 0 | 0 |  | 0 |
| Taper Length ( $t$ ) | 25 |  |  | 25 |  |  | 25 |  |  | 25 |  |  |
| Lane Util. Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Fit |  | 0.991 |  |  |  | 0.850 |  | 0.934 |  |  | 0.942 |  |
| Fil Protected | 0.950 |  |  | 0.950 |  |  |  | 0.992 |  |  | 0.983 |  |
| Satd. Flow (prot) | 1770 | 1846 | 0 | 1770 | 1863 | 1583 | 0 | 1726 | 0 | 0 | 1725 | 0 |
| Fll Permitted | 0.388 |  |  | 0.453 |  |  |  | 0.936 |  |  | 0.860 |  |
| Satd. Flow (perm) | 723 | 1846 | 0 | 844 | 1863 | 1583 | 0 | 1628 | 0 | 0 | 1509 | 0 |
| Right Tum on Red |  |  | Yes |  |  | Yes |  |  | Yes |  |  | Yes |
| Satd. Flow (RTOR) |  | 7 |  |  |  | 36 |  | 72 |  |  | 68 |  |
| Link Speed (mph) |  | 30 |  |  | 30 |  |  | 20 |  |  | 20 |  |
| Link Distance (f) |  | 694 |  |  | 680 |  |  | 497 |  |  | 526 |  |
| Travel Time (s) |  | 15.8 |  |  | 15.5 |  |  | 16.9 |  |  | 17.9 |  |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Adj. Flow (vph) | 34 | 388 | 24 | 50 | 485 | 34 | 25 | 50 | 72 | 59 | 41 | 75 |
| Shared Lane Traffic (\%) |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane Group Flow (vph) | 34 | 412 | 0 | 50 | 485 | 34 | 0 | 147 | 0 | 0 | 175 | 0 |
| Turn Type | Perm | NA |  | Perm | NA | Perm | Perm | NA |  | Perm | NA |  |
| Protecled Phases |  | 4 |  |  | 8 |  |  | 2 |  |  | 6 |  |
| Permitted Phases | 4 |  |  | 8 |  | 8 | 2 |  |  | 6 |  |  |
| Minimum Split (s) | 23.0 | 23.0 |  | 23.0 | 23.0 | 23.0 | 23.0 | 23.0 |  | 23.0 | 23.0 |  |
| Total Split (s) | 35.0 | 35.0 |  | 35.0 | 35.0 | 35.0 | 25.0 | 25.0 |  | 25.0 | 25.0 |  |
| Total Split (\%) | 58.3\% | 58.3\% |  | 58.3\% | 58.3\% | 58.3\% | 41.7\% | 41.7\% |  | 41.7\% | 41.7\% |  |
| Maximum Green (s) | 30.0 | 30.0 |  | 30.0 | 30.0 | 30.0 | 20.0 | 20.0 |  | 20.0 | 20.0 |  |
| Yellow Time (s) | 4.0 | 4.0 |  | 4.0 | 4.0 | 4.0 | 3.0 | 3.0 |  | 3.0 | 3.0 |  |
| All-Red Time (s) | 1.0 | 1.0 |  | 1.0 | 1.0 | 1.0 | 2.0 | 2.0 |  | 2.0 | 2.0 |  |
| Lost Time Adjust (s) | 0.0 | 0.0 |  | 0.0 | 0.0 | 0.0 |  | 0.0 |  |  | 0.0 |  |
| Total Lost Time (s) | 5.0 | 5.0 |  | 5.0 | 5.0 | 5.0 |  | 5.0 |  |  | 5.0 |  |
| Lead/lag |  |  |  |  |  |  |  |  |  |  |  |  |
| Lead-Lag Optimize? |  |  |  |  |  |  |  |  |  |  |  |  |
| Walk Time (s) | 7.0 | 7.0 |  | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 |  | 7.0 | 7.0 |  |
| Flash Dont Walk (s) | 11.0 | 11.0 |  | 11.0 | 11.0 | 11.0 | 11.0 | 11.0 |  | 11.0 | 11.0 |  |
| Pedestrian Cals (\#hrr) | 0 | 0 |  | 0 | 0 | 0 | 0 | 0 |  | . | 0 |  |
| Act Efflt Green (s) | 30.0 | 30.0 |  | 30.0 | 30.0 | 30.0 |  | 20.0 |  |  | 20.0 |  |
| Actuatedg/C Ratio | 0.50 | 0.50 |  | 0.50 | 0.50 | 0.50 |  | 0.33 |  |  | 0.33 |  |
| v/c Ratio | 0.09 | 0.44 |  | 0.12 | 0.52 | 0.04 |  | 0.25 |  |  | 0.32 |  |
| Control Delay | 8.8 | 11.4 |  | 8.9 | 12.7 | 3.2 |  | 9.4 |  |  | 11.2 |  |
| Queue Delay | 0.0 | 0.0 |  | 0.0 | 0.0 | 0.0 |  | 0.0 |  |  | 0.0 |  |
| Total Delay | 8.8 | 11.4 |  | 8.9 | 12.7 | 3.2 |  | 9.4 |  |  | 11.2 |  |
| LOS | A | B |  | A | B | A |  | A |  |  | B |  |
| Approach Delay |  | 11.2 |  |  | 11.8 |  |  | 9.4 |  |  | 11.2 |  |
| Approach LOS |  | B |  |  | B |  |  | A |  |  | B |  |
| Queue Length 50th (ft) | 6 | 87 |  | 9 | 109 | 0 |  | 19 |  |  | 27 |  |
| Queue Length 95th (ft) | 19 | 148 |  | 25 | 183 | 11 |  | 54 |  |  | 68 |  |
| Baseline |  |  |  |  |  |  |  |  |  | Synchro | 10 Ligh | Report $\text { Page } 2$ |



Synchro Model 2037 PM Peak (Existing Operating Conditions) 9: US-36 \& N. 10th St. Lanes, Volumes, Timings

|  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |

## Baseline

Synchro 10 Light Report
Page 4

9: US-36 \& N. 10th St. Lanes, Volumes, Timings

|  |  |  |  |  |  |  | 4 | 4 | $p$ | $\checkmark$ | $\downarrow$ | $\downarrow$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Intemal Link Dist (ft) |  | 600 |  |  | 269 |  |  | 398 |  |  | 473 |  |
| Turn Bay Length ( ft ) | 65 |  |  | 60 |  |  |  |  |  |  |  |  |
| Base Capacity (vph) | 388 | 737 |  | 414 | 744 |  |  | 503 |  |  | 459 |  |
| Starvation Cap Reductn | 0 | 0 |  | 0 | 0 |  |  | 0 |  |  | 0 |  |
| Spillback Cap Reductn | 0 | 0 |  | 0 | 0 |  |  | 0 |  |  | 0 |  |
| Storage Cap Reductn | 0 | 0 |  | 0 | 0 |  |  | 0 |  |  | 0 |  |
| Reduced v/c Ratio | 0.03 | 0.74 |  | 0.40 | 0.78 |  |  | 0.56 |  |  | 0.08 |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |
| Area Type: Other |  |  |  |  |  |  |  |  |  |  |  |  |
| Cycle Length: 75 |  |  |  |  |  |  |  |  |  |  |  |  |
| Actuated Cycle Length: 75 |  |  |  |  |  |  |  |  |  |  |  |  |
| Offset: $0(0 \%)$, Referenced to phase 2:NBTL and 6:SBTL, Start of Green |  |  |  |  |  |  |  |  |  |  |  |  |
| Natural Cycle: 60 |  |  |  |  |  |  |  |  |  |  |  |  |
| Control Type: Pretimed |  |  |  |  |  |  |  |  |  |  |  |  |
| Maximum v/c Ratio: 0.78 |  |  |  |  |  |  |  |  |  |  |  |  |
| Intersection Signal Delay: 23.4 |  |  |  | Intersection LOS: C |  |  |  |  |  |  |  |  |
| Intersection Capacity Utilization 69.6\% |  |  |  | ICU Level of Service C |  |  |  |  |  |  |  |  |
| Analysis Period (min) 15 |  |  |  |  |  |  |  |  |  |  |  |  |
| \# 95th percentile volume exceeds capacity, queue may be longer. |  |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |



| Synchro Model 15: US-36 \& N. 14th St. |  |  |  |  | 2037 PM Peak (Existing Operating Conditions) Lanes, Volumes, Timings |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $y$ |  |  | $\checkmark$ |  |  | 4 | $\uparrow$ |  |  |  | $\downarrow$ |
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | \% | $\dagger$ |  | 7 | ¢ |  |  | ¢ |  |  | ¢ |  |
| Traffic Volume (vph) | 12 | 614 | 26 | 15 | 673 | 15 | 19 | , | 27 | 28 | 16 | 15 |
| Future Volume (vph) | 12 | 614 | 26 | 15 | 673 | 15 | 19 | 9 | 27 | 28 | 16 | 15 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Storage Length $(f)$ | 125 |  | 0 | 75 |  | 0 | 0 |  | 0 | 0 |  | 0 |
| Storage Lanes | 1 |  | 0 | 1 |  | 0 | 0 |  | 0 | 0 |  | 0 |
| Taper Length ( t ) | 25 |  |  | 25 |  |  | 25 |  |  | 25 |  |  |
| Lane Uill. Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Fit |  | 0.994 |  |  | 0.997 |  |  | 0.935 |  |  | 0.966 |  |
| Flt Protected | 0.950 |  |  | 0.950 |  |  |  | 0.983 |  |  | 0.977 |  |
| Sald. Flow (prot) | 1770 | 1852 | 0 | 1770 | 1857 | 0 | 0 | 1712 | 0 | 0 | 1758 | 0 |
| Fit Permitted | 0.212 |  |  | 0.252 |  |  |  | 0.909 |  |  | 0.871 |  |
| Satd. Flow (perm) | 395 | 1852 | 0 | 469 | 1857 | 0 | 0 | 1583 | 0 | 0 | 1567 | 0 |
| Right Turn on Red |  |  | Yes |  |  | Yes |  |  | Yes |  |  | Yes |
| Satd. Flow (RTOR) |  | 5 |  |  | 3 |  |  | 29 |  |  | 16 |  |
| Link Speed (mph) |  | 30 |  |  | 30 |  |  | 20 |  |  | 30 |  |
| Link Distance ( t ) |  | 1029 |  |  | 341 |  |  | 457 |  |  | 627 |  |
| Travel Time (s) |  | 23.4 |  |  | 7.8 |  |  | 15.6 |  |  | 14.3 |  |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Adj. Flow (vph) | 13 | 667 | 28 | 16 | 732 | 16 | 21 | 10 | 29 | 30 | 17 | 16 |
| Shared Lane Traffic (\%) |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane Group Flow (vph) | 13 | 695 | 0 | 16 | 748 | 0 | 0 | 60 | 0 | 0 | 63 | 0 |
| Tum Type | Perm | NA |  | Perm | NA |  | Perm | NA |  | Perm | NA |  |
| Protected Phases |  | 4 |  |  | 8 |  |  | 2 |  |  | 6 |  |
| Permitted Phases | 4 |  |  | 8 |  |  | 2 |  |  | 6 |  |  |
| Minimum Split (s) | 24.0 | 24.0 |  | 24.0 | 24.0 |  | 23.0 | 23.0 |  | 23.0 | 23.0 |  |
| Total Split (s) | 39.0 | 39.0 |  | 39.0 | 39.0 |  | 23.0 | 23.0 |  | 23.0 | 23.0 |  |
| Total Split (\%) | 62.9\% | 62.9\% |  | 62.9\% | 62.9\% |  | 37.1\% | 37.1\% |  | 37.1\% | 37.1\% |  |
| Maximum Green (s) | 33.0 | 33.0 |  | 33.0 | 33.0 |  | 18.0 | 18.0 |  | 18.0 | 18.0 |  |
| Yellow Time (s) | 4.0 | 4.0 |  | 4.0 | 4.0 |  | 4.0 | 4.0 |  | 4.0 | 4.0 |  |
| All-Red Time (s) | 2.0 | 2.0 |  | 2.0 | 2.0 |  | 1.0 | 1.0 |  | 1.0 | 1.0 |  |
| Lost Time Adjust (s) | 0.0 | 0.0 |  | 0.0 | 0.0 |  |  | 0.0 |  |  | 0.0 |  |
| Total Lost Time (s) | 6.0 | 6.0 |  | 6.0 | 6.0 |  |  | 5.0 |  |  | 5.0 |  |
| Lead/lag |  |  |  |  |  |  |  |  |  |  |  |  |
| Lead-Lag Optimize? |  |  |  |  |  |  |  |  |  |  |  |  |
| Walk Time (s) | 7.0 | 7.0 |  | 7.0 | 7.0 |  | 7.0 | 7.0 |  | 7.0 | 7.0 |  |
| Flash Dont Walk (s) | 11.0 | 11.0 |  | 11.0 | 11.0 |  | 11.0 | 11.0 |  | 11.0 | 11.0 |  |
| Pedestrian Calls (\#/hr) | 0 | 0 |  | 0 | 0 |  | 0 | 0 |  | , | 0 |  |
| Act Eflict Green (s) | 33.0 | 33.0 |  | 33.0 | 33.0 |  |  | 18.0 |  |  | 18.0 |  |
| Actuatedg/C Ratio | 0.53 | 0.53 |  | 0.53 | 0.53 |  |  | 0.29 |  |  | 0.29 |  |
| vic Ratio | 0.06 | 0.70 |  | 0.06 | 0.76 |  |  | 0.12 |  |  | 0.14 |  |
| Control Delay | 8.0 | 15.6 |  | 7.9 | 17.7 |  |  | 11.0 |  |  | 14.0 |  |
| Queve Delay | 0.0 | 0.0 |  | 0.0 | 0.0 |  |  | 0.0 |  |  | 0.0 |  |
| Total Delay | 8.0 | 15.6 |  | 7.9 | 17.7 |  |  | 11.0 |  |  | 14.0 |  |
| LOS | A | B |  | A | B |  |  | B |  |  | B |  |
| Approach Delay |  | 15.5 |  |  | 17.5 |  |  | 11.0 |  |  | 14.0 |  |
| Approach LOS |  | B |  |  | B |  |  | B |  |  | B |  |
| Queue Length 50th (ft) | 2 | 176 |  | 3 | 199 |  |  | 8 |  |  | 13 |  |
| Queue Length 95th (ft) | 10 | 292 |  | 11 | 332 |  |  | 32 |  |  | 37 |  |
| Baseline |  |  |  |  |  |  |  |  |  | Synchro | 10 Ligh | Report <br> Page 7 |



| Synchro Model 18: US-36 \& N. 15th S |  |  |  |  | 2037 PM Peak (Existing Operating Conditions) HCM Unsignalized Intersection Capacity Analysis |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $\lambda$ |  |  | $\checkmark$ |  |  | 4 | $\uparrow$ |  |  |  | $\downarrow$ |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | 7 | 今 |  | \% | 今 |  |  | ¢ |  |  | ¢ |  |
| Traffic Volume (veh/h) | 66 | 576 | 15 | 27 | 672 | 46 | 4 | 15 | 11 | 12 | 5 | 65 |
| Future Volume (Veh/h) | 66 | 576 | 15 | 27 | 672 | 46 | 4 | 15 | 11 | 12 | 5 | 65 |
| Sign Control |  | Free |  |  | Free |  |  | Stop |  |  | Stop |  |
| Grade |  | 0\% |  |  | 0\% |  |  | 0\% |  |  | 0\% |  |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Hourly flow rate (vph) | 72 | 626 | 16 | 29 | 730 | 50 | 4 | 16 | 12 | 13 | 5 | 71 |
| Pedestrians |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane Width (fi) |  |  |  |  |  |  |  |  |  |  |  |  |
| Walking Speed (t/s) |  |  |  |  |  |  |  |  |  |  |  |  |
| Percent Blockage |  |  |  |  |  |  |  |  |  |  |  |  |
| Right turn flare (veh) |  |  |  |  |  |  |  |  |  |  |  |  |
| Median type |  | TWLTL |  |  | TWLTL |  |  |  |  |  |  |  |
| Median storage veh) |  | 2 |  |  | 2 |  |  |  |  |  |  |  |
| Upstream signal (ft) |  | 341 |  |  |  |  |  |  |  |  |  |  |
| pX, platoon unblocked |  |  |  | 0.73 |  |  | 0.73 | 0.73 | 0.73 | 0.73 | 0.73 |  |
| VC , conflicting volume | 780 |  |  | 642 |  |  | 1640 | 1616 | 634 | 1603 | 1599 | 755 |
| VC1, stage 1 conf vol |  |  |  |  |  |  | 778 | 778 |  | 813 | 813 |  |
| vC2, stage 2 conf vol |  |  |  |  |  |  | 862 | 838 |  | 790 | 786 |  |
| vCu , unblocked vol | 780 |  |  | 317 |  |  | 1692 | 1660 | 306 | 1642 | 1637 | 755 |
| IC, single (s) | 4.1 |  |  | 4.1 |  |  | 7.1 | 6.5 | 6.2 | 7.1 | 6.5 | 6.2 |
| IC, 2 stage (s) |  |  |  |  |  |  | 6.1 | 5.5 |  | 6.1 | 5.5 |  |
| IF (s) | 2.2 |  |  | 2.2 |  |  | 3.5 | 4.0 | 3.3 | 3.5 | 4.0 | 3.3 |
| po queue free \% | 91 |  |  | 97 |  |  | 98 | 93 | 98 | 94 | 98 | 83 |
| cM capacity (veh/h) | 837 |  |  | 902 |  |  | 176 | 231 | 532 | 230 | 248 | 409 |
| Direction, Lane\# | EB1 | EB2 | WB 1 | WB2 | NB 1 | SB 1 |  |  |  |  |  |  |
| Volume Total | 72 | 642 | 29 | 780 | 32 | 89 |  |  |  |  |  |  |
| Volume Left | 72 | 0 | 29 | 0 | 4 | 13 |  |  |  |  |  |  |
| Volume Right | 0 | 16 | 0 | 50 | 12 | 71 |  |  |  |  |  |  |
| CSH | 837 | 1700 | 902 | 1700 | 279 | 355 |  |  |  |  |  |  |
| Volume to Capacity | 0.09 | 0.38 | 0.03 | 0.46 | 0.11 | 0.25 |  |  |  |  |  |  |
| Queue Length 95th (f) | 7 | 0 | 2 | 0 | 10 | 24 |  |  |  |  |  |  |
| Control Delay (s) | 9.7 | 0.0 | 9.1 | 0.0 | 19.6 | 18.5 |  |  |  |  |  |  |
| Lane LOS | A |  | A |  | c | C |  |  |  |  |  |  |
| Approach Delay (s) | 1.0 |  | 0.3 |  | 19.6 | 18.5 |  |  |  |  |  |  |
| Approach LOS |  |  |  |  | C | C |  |  |  |  |  |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |
| Average Delay |  |  | 2.0 |  |  |  |  |  |  |  |  |  |
| Intersection Capacity Utilization |  |  | 58.6\% |  | CU Level | Service |  |  | B |  |  |  |
| Analysis Period (min) |  |  | 15 |  |  |  |  |  |  |  |  |  |


| Baseline | Synchro 10 Light Report |
| ---: | ---: |
| Page 3 |  |


| Synchro Model 21: US-36 \& N. 17ths |  |  |  |  | 2037 PM Peak (Existing Operating Conditions) HCM Unsignalized Intersection Capacity Analysis |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $\lambda$ |  |  | $\checkmark$ | $\leftarrow$ | 4 | 4 | $\uparrow$ |  |  |  | $\downarrow$ |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | 7 | 今 |  |  | ¢ |  |  | ¢ |  |  | ¢ |  |
| Traffic Volume (veh/h) | 13 | 664 | 9 | 20 | 703 | 7 | 22 | 1 | 16 | 9 | 1 | 18 |
| Future Volume (Veh/h) | 13 | 664 | 9 | 20 | 703 | 7 | 22 | 1 | 16 | 9 | 1 | 18 |
| Sign Control |  | Free |  |  | Free |  |  | Stop |  |  | Stop |  |
| Grade |  | 0\% |  |  | 0\% |  |  | 0\% |  |  | 0\% |  |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Hourly flow rate (vph) | 14 | 722 | 10 | 22 | 764 | , | 24 | 1 | 17 | 10 | 1 | 20 |
| Pedestrians |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane Width (fi) |  |  |  |  |  |  |  |  |  |  |  |  |
| Walking Speed (t/s) |  |  |  |  |  |  |  |  |  |  |  |  |
| Percent Blockage |  |  |  |  |  |  |  |  |  |  |  |  |
| Right turn flare (veh) |  |  |  |  |  |  |  |  |  |  |  |  |
| Median type |  | TWLTL |  |  | None |  |  |  |  |  |  |  |
| Median storage veh) |  | 2 |  |  |  |  |  |  |  |  |  |  |
| Upstream signal (ft) |  | 1068 |  |  | 971 |  |  |  |  |  |  |  |
| pX, platoon unblocked |  |  |  | 0.78 |  |  | 0.78 | 0.78 | 0.78 | 0.78 | 0.78 |  |
| VC , conflicting volume | 772 |  |  | 732 |  |  | 1588 | 1571 | 727 | 1580 | 1572 | 768 |
| VC1, stage 1 conf vol |  |  |  |  |  |  | 755 | 755 |  | 812 | 812 |  |
| vC2, stage 2 conf vol |  |  |  |  |  |  | 832 | 816 |  | 768 | 760 |  |
| vCu , unblocked vol | 772 |  |  | 513 |  |  | 1612 | 1591 | 506 | 1602 | 1593 | 768 |
| IC, single (s) | 4.1 |  |  | 4.1 |  |  | 7.1 | 6.5 | 6.2 | 7.1 | 6.5 | 6.2 |
| IC, 2 stage (s) |  |  |  |  |  |  | 6.1 | 5.5 |  | 6.1 | 5.5 |  |
| IF (s) | 2.2 |  |  | 2.2 |  |  | 3.5 | 4.0 | 3.3 | 3.5 | 4.0 | 3.3 |
| po queue free \% | 98 |  |  | 97 |  |  | 90 | 100 | 96 | 96 | 100 | 95 |
| cM capacity (veh/h) | 843 |  |  | 819 |  |  | 250 | 274 | 440 | 254 | 272 | 402 |
| Direction, Lane\# | EB 1 | EB2 | WB1 | NB1 | SB1 |  |  |  |  |  |  |  |
| Volume Total | 14 | 732 | 794 | 42 | 31 |  |  |  |  |  |  |  |
| Volume Left | 14 | 0 | 22 | 24 | 10 |  |  |  |  |  |  |  |
| Volume Right | 0 | 10 | 8 | 17 | 20 |  |  |  |  |  |  |  |
| cSH | 843 | 1700 | 819 | 304 | 334 |  |  |  |  |  |  |  |
| Volume to Capacity | 0.02 | 0.43 | 0.03 | 0.14 | 0.09 |  |  |  |  |  |  |  |
| Queue Length 95th (f) | , | 0 | 2 | 12 | 8 |  |  |  |  |  |  |  |
| Control Delay (s) | 9.3 | 0.0 | 0.7 | 18.8 | 16.9 |  |  |  |  |  |  |  |
| Lane LOS | A |  | A | C | c |  |  |  |  |  |  |  |
| Approach Delay (s) | 0.2 |  | 0.7 | 18.8 | 16.9 |  |  |  |  |  |  |  |
| Approach LOS |  |  |  | C | C |  |  |  |  |  |  |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |
| Average Delay |  |  | 1.2 |  |  |  |  |  |  |  |  |  |
| Intersection Capacity Utilization |  |  | 64.1\% |  | CU Level | Service |  |  | C |  |  |  |
| Analysis Period (min) |  |  | 15 |  |  |  |  |  |  |  |  |  |


| Baseline | Synchro 10 Light Report |
| ---: | ---: |
| Page 4 |  |


| Synchro Model 27: US-36 \& 11th Rd. |  |  |  |  | 2037 PM Peak (Existing Operating Conditions) HCM Unsignalized Intersection Capacity Analysis |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 7 |  |  | 1 |  |  | 4 | $\uparrow$ | $p$ |  | $\downarrow$ | $\downarrow$ |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | 7 | $\dagger$ |  | $\dagger$ | 今 |  |  | $\uparrow$ | 1 |  | 4 | F |
| Traffic Volume (veh/h) | 25 | 583 | 101 | 31 | 583 | 52 | 49 | 7 | 45 | 25 | 5 | 11 |
| Future Volume (Veh/h) | 25 | 583 | 101 | 31 | 583 | 52 | 49 | 7 | 45 | 25 | 5 | 11 |
| Sign Control |  | Free |  |  | Free |  |  | Stop |  |  | Stop |  |
| Grade |  | 0\% |  |  | 0\% |  |  | 0\% |  |  | 0\% |  |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Hourly flow rate (vph) | 27 | 634 | 110 | 34 | 634 | 57 | 53 | 8 | 49 | 27 | 5 | 12 |
| Pedestrians |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane Width (fi) |  |  |  |  |  |  |  |  |  |  |  |  |
| Walking Speed (ff/s) |  |  |  |  |  |  |  |  |  |  |  |  |
| Percent Blockage |  |  |  |  |  |  |  |  |  |  |  |  |
| Right turn flare (veh) |  |  |  |  |  |  |  |  | 3 |  |  | 4 |
| Median type |  | WLTL |  |  | TWLTL |  |  |  |  |  |  |  |
| Median storage veh) |  | 2 |  |  | 2 |  |  |  |  |  |  |  |
| Upstream signal (tt) |  |  |  |  |  |  |  |  |  |  |  |  |
| pX , platoon unblocked |  |  |  |  |  |  |  |  |  |  |  |  |
| vC, conflicting volume | 691 |  |  | 744 |  |  | 1454 | 1502 | 689 | 1447 | 1528 | 662 |
| vC1, stage 1 conf vol |  |  |  |  |  |  | 743 | 743 |  | 730 | 730 |  |
| vC2, stage 2 conf vol |  |  |  |  |  |  | 710 | 759 |  | 716 | 798 |  |
| vCu, unblocked vol | 691 |  |  | 744 |  |  | 1454 | 1502 | 689 | 1447 | 1528 | 662 |
| tC, single (s) | 4.1 |  |  | 4.1 |  |  | 7.1 | 6.5 | 6.2 | 7.1 | 6.5 | 6.2 |
| tC, 2 stage (s) |  |  |  |  |  |  | 6.1 | 5.5 |  | 6.1 | 5.5 |  |
| tF (s) | 2.2 |  |  | 2.2 |  |  | 3.5 | 4.0 | 3.3 | 3.5 | 4.0 | 3.3 |
| po queue free \% | 97 |  |  | 96 |  |  | 81 | 97 | 89 | 90 | 98 | 97 |
| cM capacity (veh/h) | 904 |  |  | 864 |  |  | 279 | 290 | 446 | 259 | 281 | 462 |
| Direction, Lane \# | EB 1 | EB 2 | WB 1 | WB 2 | NB 1 | SB 1 |  |  |  |  |  |  |
| Volume Total | 27 | 744 | 34 | 691 | 110 | 44 |  |  |  |  |  |  |
| Volume Left | 27 | 0 | 34 | 0 | 53 | 27 |  |  |  |  |  |  |
| Volume Right | 0 | 110 | 0 | 57 | 49 | 12 |  |  |  |  |  |  |
| cSH | 904 | 1700 | 864 | 1700 | 505 | 361 |  |  |  |  |  |  |
| Volume to Capacity | 0.03 | 0.44 | 0.04 | 0.41 | 0.22 | 0.12 |  |  |  |  |  |  |
| Queue Length 95th (tt) | 2 | 0 | 3 | 0 | 21 | 10 |  |  |  |  |  |  |
| Control Delay (s) | 9.1 | 0.0 | 9.3 | 0.0 | 18.1 | 18.5 |  |  |  |  |  |  |
| Lane LOS | A |  | A |  | c | C |  |  |  |  |  |  |
| Approach Delay (s) | 0.3 |  | 0.4 |  | 18.1 | 18.5 |  |  |  |  |  |  |
| Approach LOS |  |  |  |  | c | C |  |  |  |  |  |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |
| Average Delay |  |  | 2.0 |  |  |  |  |  |  |  |  |  |
| Intersection Capacity Utilization |  |  | 53.5\% |  | U Level | Service |  |  | A |  |  |  |
| Analysis Period (min) |  |  | 15 |  |  |  |  |  |  |  |  |  |

[^0]
## C. 5 REMOVAL OF SIGNALS AT $8^{\text {TH }}$ STREET SCENARIO

| Synchro Model 6: US-36 \& N. 8th St. |  |  |  |  |  | AM P | eak HCN | xistin | Op ed inte |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 7 | $\rightarrow$ |  | $\checkmark$ |  |  | 4 | $\uparrow$ | $p$ |  | $\downarrow$ | $\downarrow$ |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | 7 | $\dagger$ |  | $\dagger$ | $\uparrow$ | F |  | ¢ |  |  | $\dagger$ |  |
| Traffic Volume (veh/h) | 33 | 248 | 30 | 16 | 172 | 12 | 7 | 11 | 2 | 21 | 22 | 16 |
| Future Volume (Veh/h) | 33 | 248 | 30 | 16 | 172 | 12 | 7 | 11 | 2 | 21 | 22 | 16 |
| Sign Control |  | Free |  |  | Free |  |  | Stop |  |  | Stop |  |
| Grade |  | 0\% |  |  | 0\% |  |  | 0\% |  |  | 0\% |  |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Hourly flow rate (vph) | 36 | 270 | 33 | 17 | 187 | 13 | 8 | 12 | 2 | 23 | 24 | 17 |
| Pedestrians |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane Width (ti) |  |  |  |  |  |  |  |  |  |  |  |  |
| Walking Speed (ft/s) |  |  |  |  |  |  |  |  |  |  |  |  |
| Percent Blockage |  |  |  |  |  |  |  |  |  |  |  |  |
| Right turn flare (veh) |  |  |  |  |  |  |  |  |  |  |  |  |
| Median type |  | None |  |  | TWLTL |  |  |  |  |  |  |  |
| Median storage veh) |  |  |  |  | 2 |  |  |  |  |  |  |  |
| Upstream signal (ft) |  |  |  |  | 680 |  |  |  |  |  |  |  |
| pX, platoon unblocked |  |  |  |  |  |  |  |  |  |  |  |  |
| vC, conficting volume | 200 |  |  | 303 |  |  | 608 | 592 | 286 | 571 | 596 | 187 |
| vC1, stage 1 conf vol |  |  |  |  |  |  | 358 | 358 |  | 221 | 221 |  |
| vC2, stage 2 conf vol |  |  |  |  |  |  | 250 | 234 |  | 350 | 375 |  |
| vCu , unblocked vol | 200 |  |  | 303 |  |  | 608 | 592 | 286 | 571 | 596 | 187 |
| tC, single (s) | 4.1 |  |  | 4.1 |  |  | 7.1 | 6.5 | 6.2 | 7.1 | 6.5 | 6.2 |
| tC, 2 stage (s) |  |  |  |  |  |  | 6.1 | 5.5 |  | 6.1 | 5.5 |  |
| tF (s) | 2.2 |  |  | 2.2 |  |  | 3.5 | 4.0 | 3.3 | 3.5 | 4.0 | 3.3 |
| p0 queue free \% | 97 |  |  | 99 |  |  | 99 | 98 | 100 | 96 | 96 | 98 |
| cM capacity (veh/h) | 1372 |  |  | 1258 |  |  | 548 | 544 | 753 | 568 | 538 | 855 |
| Direction, Lane\# | EB 1 | EB2 | WB 1 | WB2 | WB3 | NB 1 | SB 1 |  |  |  |  |  |
| Volume Total | 36 | 303 | 17 | 187 | 13 | 22 | 64 |  |  |  |  |  |
| Volume Left | 36 | 0 | 17 | 0 | 0 | 8 | 23 |  |  |  |  |  |
| Volume Right | 0 | 33 | 0 | 0 | 13 | 2 | 17 |  |  |  |  |  |
| cSH | 1372 | 1700 | 1258 | 1700 | 1700 | 559 | 609 |  |  |  |  |  |
| Volume to Capacity | 0.03 | 0.18 | 0.01 | 0.11 | 0.01 | 0.04 | 0.11 |  |  |  |  |  |
| Queue Length 95th (ft) | 2 | . | 1 | 0 | 0 | 3 | 9 |  |  |  |  |  |
| Control Delay (s) | 7.7 | 0.0 | 7.9 | 0.0 | 0.0 | 11.7 | 11.6 |  |  |  |  |  |
| Lane LOS | A |  | A |  |  | B | B |  |  |  |  |  |
| Approach Delay (s) | 0.8 |  | 0.6 |  |  | 11.7 | 11.6 |  |  |  |  |  |
| Approach LOS |  |  |  |  |  | B | B |  |  |  |  |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |
| Average Delay |  |  | 2.2 |  |  |  |  |  |  |  |  |  |
| Intersection Capacity Utilization |  |  | 32.5\% |  | CU Level | Service |  |  | A |  |  |  |
| Analysis Period (min) |  |  | 15 |  |  |  |  |  |  |  |  |  |

## Baseline

Synchro Model

| 6: US-36 \& N. 8th St. |  |  |  |  |  |  | HCM Unsignalized Intersection Capacity Analysis |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 7 | $\rightarrow$ | $\checkmark$ | 7 |  | 4 | 4 | 4 | $p$ | $\downarrow$ | $\downarrow$ | 4 |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | ${ }^{7}$ | $\dagger$ |  | 7 | $\uparrow$ | 7 |  | $\pm$ |  |  | $\dagger$ |  |
| Traffic Volume (veh/h) | 23 | 265 | 16 | 34 | 331 | 23 | 17 | 34 | 49 | 40 | 28 | 51 |
| Future Volume (Veh/h) | 23 | 265 | 16 | 34 | 331 | 23 | 17 | 34 | 49 | 40 | 28 | 51 |
| Sign Control |  | Free |  |  | Free |  |  | Stop |  |  | Stop |  |
| Grade |  | 0\% |  |  | 0\% |  |  | 0\% |  |  | 0\% |  |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Hourly flow rate (vph) | 25 | 288 | 17 | 37 | 360 | 25 | 18 | 37 | 53 | 43 | 30 | 55 |
| Pedestrians |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane Width ( ft ) |  |  |  |  |  |  |  |  |  |  |  |  |
| Walking Speed (ft/s) |  |  |  |  |  |  |  |  |  |  |  |  |
| Percent Blockage |  |  |  |  |  |  |  |  |  |  |  |  |
| Right turn flare (veh) |  |  |  |  |  |  |  |  |  |  |  |  |
| Median type |  | None |  |  | TWLTL |  |  |  |  |  |  |  |
| Median storage veh) |  |  |  |  | 2 |  |  |  |  |  |  |  |
| Upstream signal (ft) |  |  |  |  | 680 |  |  |  |  |  |  |  |
| pX , platoon unblocked | 0.92 |  |  |  |  |  | 0.92 | 0.92 |  | 0.92 | 0.92 | 0.92 |
| vC , conflicting volume | 385 |  |  | 305 |  |  | 850 | 806 | 296 | 844 | 789 | 360 |
| $\mathrm{vC1}$, stage 1 conf vol |  |  |  |  |  |  | 346 | 346 |  | 434 | 434 |  |
| VC 2 , stage 2 conf vol |  |  |  |  |  |  | 504 | 459 |  | 410 | 355 |  |
| vCu , unblocked vol | 294 |  |  | 305 |  |  | 797 | 749 | 296 | 790 | 731 | 267 |
| tC, single (s) | 4.1 |  |  | 4.1 |  |  | 7.1 | 6.5 | 6.2 | 7.1 | 6.5 | 6.2 |
| tC, 2 stage (s) |  |  |  |  |  |  | 6.1 | 5.5 |  | 6.1 | 5.5 |  |
| tF (s) | 2.2 |  |  | 2.2 |  |  | 3.5 | 4.0 | 3.3 | 3.5 | 4.0 | 3.3 |
| p0 queue free \% | 98 |  |  | 97 |  |  | 96 | 92 | 93 | 90 | 94 | 92 |
| cM capacity (veh/h) | 1172 |  |  | 1256 |  |  | 411 | 465 | 743 | 425 | 473 | 714 |
| Direction, Lane \# | EB 1 | EB 2 | WB 1 | WB 2 | WB 3 | NB 1 | SB 1 |  |  |  |  |  |
| Volume Total | 25 | 305 | 37 | 360 | 25 | 108 | 128 |  |  |  |  |  |
| Volume Left | 25 | 0 | 37 | 0 | 0 | 18 | 43 |  |  |  |  |  |
| Volume Right | 0 | 17 | 0 | 0 | 25 | 53 | 55 |  |  |  |  |  |
| cSH | 1172 | 1700 | 1256 | 1700 | 1700 | 555 | 530 |  |  |  |  |  |
| Volume to Capacity | 0.02 | 0.18 | 0.03 | 0.21 | 0.01 | 0.19 | 0.24 |  |  |  |  |  |
| Queue Length 95th (t) | 2 | 0 | 2 | 0 | 0 | 18 | 23 |  |  |  |  |  |
| Control Delay (s) | 8.1 | 0.0 | 8.0 | 0.0 | 0.0 | 13.1 | 13.9 |  |  |  |  |  |
| Lane LOS | A |  | A |  |  | B | B |  |  |  |  |  |
| Approach Delay (s) | 0.6 |  | 0.7 |  |  | 13.1 | 13.9 |  |  |  |  |  |
| Approach LOS |  |  |  |  |  | B | B |  |  |  |  |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |
| Average Delay |  |  | 3.7 |  |  |  |  |  |  |  |  |  |
| Intersection Capacity Utilization |  |  | 43.1\% |  | CU Level | Service |  |  | A |  |  |  |
| Analysis Period (min) |  |  | 15 |  |  |  |  |  |  |  |  |  |

Analysis Period (min) 15

| Synchro Model 6: US-36 \& N. 8th St. |  |  |  |  |  | AM F | eak HCN | $\begin{aligned} & \text { xistin } \\ & \text { Unsigna } \end{aligned}$ | Ope zed Inte |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 7 | $\rightarrow$ |  | 1 |  |  | 4 | $\uparrow$ | $p$ |  | $\downarrow$ | $\downarrow$ |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | 1 | $\stackrel{1}{ }$ |  | $\dagger$ | $\uparrow$ | F |  | ¢ |  |  | \$ |  |
| Traffic Volume (veh/h) | 44 | 334 | 40 | 22 | 232 | 16 | 9 | 15 | 3 | 28 | 30 | 22 |
| Future Volume (Veh/h) | 44 | 334 | 40 | 22 | 232 | 16 | 9 | 15 | 3 | 28 | 30 | 22 |
| Sign Control |  | Free |  |  | Free |  |  | Stop |  |  | Stop |  |
| Grade |  | 0\% |  |  | 0\% |  |  | 0\% |  |  | 0\% |  |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Hourly flow rate (vph) | 48 | 363 | 43 | 24 | 252 | 17 | 10 | 16 | 3 | 30 | 33 | 24 |
| Pedestrians |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane Width (ti) |  |  |  |  |  |  |  |  |  |  |  |  |
| Walking Speed (ft/s) |  |  |  |  |  |  |  |  |  |  |  |  |
| Percent Blockage |  |  |  |  |  |  |  |  |  |  |  |  |
| Right turn flare (veh) |  |  |  |  |  |  |  |  |  |  |  |  |
| Median type |  | None |  |  | TWLTL |  |  |  |  |  |  |  |
| Median storage veh) |  |  |  |  | 2 |  |  |  |  |  |  |  |
| Upstream signal (ft) |  |  |  |  | 680 |  |  |  |  |  |  |  |
| pX, platoon unblocked |  |  |  |  |  |  |  |  |  |  |  |  |
| vC, conflicting volume | 269 |  |  | 406 |  |  | 821 | 798 | 384 | 770 | 802 | 252 |
| vC1, stage 1 conf vol |  |  |  |  |  |  | 480 | 480 |  | 300 | 300 |  |
| vC2, stage 2 conf vol |  |  |  |  |  |  | 340 | 317 |  | 470 | 502 |  |
| vCu , unblocked vol | 269 |  |  | 406 |  |  | 821 | 798 | 384 | 770 | 802 | 252 |
| tC, single (s) | 4.1 |  |  | 4.1 |  |  | 7.1 | 6.5 | 6.2 | 7.1 | 6.5 | 6.2 |
| tC, 2 stage (s) |  |  |  |  |  |  | 6.1 | 5.5 |  | 6.1 | 5.5 |  |
| tF (s) | 2.2 |  |  | 2.2 |  |  | 3.5 | 4.0 | 3.3 | 3.5 | 4.0 | 3.3 |
| po queue free \% | 96 |  |  | 98 |  |  | 98 | 97 | 100 | 94 | 93 | 97 |
| cM capacity (veh/h) | 1295 |  |  | 1153 |  |  | 443 | 462 | 663 | 464 | 453 | 787 |
| Direction, Lane \# | EB 1 | EB 2 | WB 1 | WB 2 | WB3 | NB 1 | SB 1 |  |  |  |  |  |
| Volume Total | 48 | 406 | 24 | 252 | 17 | 29 | 87 |  |  |  |  |  |
| Volume Left | 48 | 0 | 24 | 0 | 0 | 10 | 30 |  |  |  |  |  |
| Volume Right | 0 | 43 | 0 | 0 | 17 | 3 | 24 |  |  |  |  |  |
| cSH | 1295 | 1700 | 1153 | 1700 | 1700 | 470 | 518 |  |  |  |  |  |
| Volume to Capacity | 0.04 | 0.24 | 0.02 | 0.15 | 0.01 | 0.06 | 0.17 |  |  |  |  |  |
| Queue Length 95th (tt) | 3 | 0 | 2 | 0 | 0 | 5 | 15 |  |  |  |  |  |
| Control Delay (s) | 7.9 | 0.0 | 8.2 | 0.0 | 0.0 | 13.2 | 13.3 |  |  |  |  |  |
| Lane LOS | A |  | A |  |  | B | B |  |  |  |  |  |
| Approach Delay (s) | 0.8 |  | 0.7 |  |  | 13.2 | 13.3 |  |  |  |  |  |
| Approach LOS |  |  |  |  |  | B | B |  |  |  |  |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |
| Average Delay |  |  | 2.5 |  |  |  |  |  |  |  |  |  |
| Intersection Capacity Utilization |  |  | 39.3\% |  | CU Level | Service |  |  | A |  |  |  |
| Analysis Period (min) |  |  | 15 |  |  |  |  |  |  |  |  |  |

Baseline Synchro 10 Light Report
Page 1

| Synchro Model 6: US-36 \& N. 8th St. |  |  |  | 2037 PM Peak (Proposed Operating Conditions) HCM Unsignalized Intersection Capacity Analysis |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 7 | $\rightarrow$ |  | 1 |  |  | 4 | $\uparrow$ | $p$ |  |  | $\checkmark$ |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | \% | F |  | 7 | $\uparrow$ | 7 |  | ¢ |  |  | ¢ |  |
| Traffic Volume (veh/h) | 31 | 357 | 22 | 46 | 446 | 31 | 23 | 46 | 66 | 54 | 38 | 69 |
| Future Volume (Veh/h) | 31 | 357 | 22 | 46 | 446 | 31 | 23 | 46 | 66 | 54 | 38 | 69 |
| Sign Control |  | Free |  |  | Free |  |  | Stop |  |  | Stop |  |
| Grade |  | 0\% |  |  | 0\% |  |  | 0\% |  |  | 0\% |  |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Hourly flow rate (vph) | 34 | 388 | 24 | 50 | 485 | 34 | 25 | 50 | 72 | 59 | 41 | 75 |
| Pedestrians |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane Width (ti) |  |  |  |  |  |  |  |  |  |  |  |  |
| Walking Speed (fts) |  |  |  |  |  |  |  |  |  |  |  |  |
| Percent Blockage |  |  |  |  |  |  |  |  |  |  |  |  |
| Right turn flare (veh) |  |  |  |  |  |  |  |  |  |  |  |  |
| Median type |  | None |  |  | TWLTL |  |  |  |  |  |  |  |
| Median storage veh) |  |  |  |  | 2 |  |  |  |  |  |  |  |
| Upstream signal (ft) |  |  |  |  | 680 |  |  |  |  |  |  |  |
| pX, platoon unblocked | 0.86 |  |  |  |  |  | 0.86 | 0.86 |  | 0.86 | 0.86 | 0.86 |
| vC, conflicting volume | 519 |  |  | 412 |  |  | 1148 | 1087 | 400 | 1138 | 1065 | 485 |
| vC1, stage 1 conf vol |  |  |  |  |  |  | 468 | 468 |  | 585 | 585 |  |
| vC2, slage 2 conf vol |  |  |  |  |  |  | 680 | 619 |  | 553 | 480 |  |
| vCu, unblocked vol | 357 |  |  | 412 |  |  | 1090 | 1019 | 400 | 1078 | 993 | 317 |
| tC , single (s) | 4.1 |  |  | 4.1 |  |  | 7.1 | 6.5 | 6.2 | 7.1 | 6.5 | 6.2 |
| tC, 2 stage (s) |  |  |  |  |  |  | 6.1 | 5.5 |  | 6.1 | 5.5 |  |
| tF (s) | 2.2 |  |  | 2.2 |  |  | 3.5 | 4.0 | 3.3 | 3.5 | 4.0 | 3.3 |
| po queue free \% | 97 |  |  | 96 |  |  | 91 | 86 | 89 | 81 | 89 | 88 |
| cM capacity (veh/h) | 1031 |  |  | 1147 |  |  | 283 | 366 | 650 | 303 | 377 | 621 |
| Direction, Lane \# | EB 1 | EB 2 | WB 1 | WB 2 | WB 3 | NB 1 | SB 1 |  |  |  |  |  |
| Volume Total | 34 | 412 | 50 | 485 | 34 | 147 | 175 |  |  |  |  |  |
| Volume Left | 34 | 0 | 50 | 0 | 0 | 25 | 59 |  |  |  |  |  |
| Volume Right | 0 | 24 | 0 | 0 | 34 | 72 | 75 |  |  |  |  |  |
| cSH | 1031 | 1700 | 1147 | 1700 | 1700 | 438 | 412 |  |  |  |  |  |
| Volume to Capacity | 0.03 | 0.24 | 0.04 | 0.29 | 0.02 | 0.34 | 0.42 |  |  |  |  |  |
| Queue Length 95th (tt) | 3 | 0 | 3 | 0 | 0 | 36 | 52 |  |  |  |  |  |
| Control Delay (s) | 8.6 | 0.0 | 8.3 | 0.0 | 0.0 | 17.3 | 20.0 |  |  |  |  |  |
| Lane LOS | A |  | A |  |  | C | C |  |  |  |  |  |
| Approach Delay (s) | 0.7 |  | 0.7 |  |  | 17.3 | 20.0 |  |  |  |  |  |
| Approach LOS |  |  |  |  |  | C | c |  |  |  |  |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |
| Average Delay |  |  | 5.1 |  |  |  |  |  |  |  |  |  |
| Intersection Capacity Utilization |  |  | 52.7\% |  | CU Level | Service |  |  | A |  |  |  |
| Analysis Period (min) |  |  | 15 |  |  |  |  |  |  |  |  |  |

Baseline Synchro 10 Light Report
Page 1

## C. 6 SIGNALIZING $11^{\text {TH }}$ ROAD

| Synchro Model 27: US-36 \& 11th |  |  |  |  | 2017 PM Peak (Proposed Operating Conditions) Lanes, Volumes, Timings |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $\checkmark$ |  |  |  |  | 4 | $4$ | $\uparrow$ | $p$ |  | $\downarrow$ | 4 |
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | \% | $\uparrow$ | 7 | 7 | $\uparrow$ | 1 | ${ }^{*}$ | $\uparrow$ | 7 | 7 | $\uparrow$ | 「 |
| Traffic Volume (vph) | 14 | 323 | 56 | 17 | 323 | 29 | 27 | 4 | 25 | 14 | 3 | 6 |
| Future Volume (vph) | 14 | 323 | 56 | 17 | 323 | 29 | 27 | 4 | 25 | 14 | 3 | 6 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Storage Length (fi) | 200 |  | 200 | 200 |  | 200 | 100 |  | 100 | 100 |  | 100 |
| Storage Lanes | 1 |  | 1 | 1 |  | 1 | 1 |  | 1 | 1 |  | 1 |
| Taper Length ( f ) | 25 |  |  | 25 |  |  | 25 |  |  | 25 |  |  |
| Lane Util. Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Fit |  |  | 0.850 |  |  | 0.850 |  |  | 0.850 |  |  | 0.850 |
| Fil Protected | 0.950 |  |  | 0.950 |  |  | 0.950 |  |  | 0.950 |  |  |
| Satd. Flow (prot) | 1770 | 1863 | 1583 | 1770 | 1863 | 1583 | 1770 | 1863 | 1583 | 1770 | 1863 | 1583 |
| Fll Permitted | 0.406 |  |  | 0.406 |  |  | 0.756 |  |  | 0.755 |  |  |
| Satd. Flow (perm) | 756 | 1863 | 1583 | 756 | 1863 | 1583 | 1408 | 1863 | 1583 | 1406 | 1863 | 1583 |
| Right Tum on Red |  |  | Yes |  |  | Yes |  |  | Yes |  |  | Yes |
| Satd. Flow (RTOR) |  |  | 109 |  |  | 109 |  |  | 109 |  |  | 109 |
| Link Speed (mph) |  | 45 |  |  | 45 |  |  | 30 |  |  | 30 |  |
| Link Distance (ft) |  | 3848 |  |  | 1647 |  |  | 1088 |  |  | 1216 |  |
| Travel Time (s) |  | 58.3 |  |  | 25.0 |  |  | 24.7 |  |  | 27.6 |  |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Adj. Flow (vph) | 15 | 351 | 61 | 18 | 351 | 32 | 29 | 4 | 27 | 15 | 3 | 7 |
| Shared Lane Traffic (\%) |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane Group Flow (vph) | 15 | 351 | 61 | 18 | 351 | 32 | 29 | 4 | 27 | 15 | 3 | 7 |
| Turn Type | pm+pt | NA | Perm | pm+pt | NA | Perm | Perm | NA | Perm | Perm | NA | Perm |
| Protected Phases | 7 | 4 |  | 3 | 8 |  |  | 2 |  |  | 6 |  |
| Permitted Phases | 4 |  | 4 | 8 |  | 8 | 2 |  | 2 | 6 |  | 6 |
| Detector Phase | 7 | 4 | 4 | 3 | 8 | 8 | 2 | 2 | 2 | 6 | 6 | 6 |
| Switch Phase |  |  |  |  |  |  |  |  |  |  |  |  |
| Minimum Initial ( $s$ ) | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 |
| Minimum Split (s) | 9.5 | 22.5 | 22.5 | 9.5 | 22.5 | 22.5 | 22.5 | 22.5 | 22.5 | 22.5 | 22.5 | 22.5 |
| Total Split (s) | 10.0 | 40.0 | 40.0 | 10.0 | 40.0 | 40.0 | 10.0 | 10.0 | 10.0 | 10.0 | 10.0 | 10.0 |
| Total Split (\%) | 16.7\% | 66.7\% | 66.7\% | 16.7\% | 66.7\% | 66.7\% | 16.7\% | 16.7\% | 16.7\% | 16.7\% | 16.7\% | 16.7\% |
| Maximum Green (s) | 5.5 | 35.5 | 35.5 | 5.5 | 35.5 | 35.5 | 5.5 | 5.5 | 5.5 | 5.5 | 5.5 | 5.5 |
| Yellow Time (s) | 3.5 | 3.5 | 3.5 | 3.5 | 3.5 | 3.5 | 3.5 | 3.5 | 3.5 | 3.5 | 3.5 | 3.5 |
| All-Red Time (s) | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 |
| Lost Time Adjust (s) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Lost Time (s) | 4.5 | 4.5 | 4.5 | 4.5 | 4.5 | 4.5 | 4.5 | 4.5 | 4.5 | 4.5 | 4.5 | 4.5 |
| Lead/Lag | Lead | Lag | Lag | Lead | Lag | Lag |  |  |  |  |  |  |
| Lead-Lag Optimize? | Yes | Yes | Yes | Yes | Yes | Yes |  |  |  |  |  |  |
| Vehicle Extension (s) | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 |
| Recall Mode | None | None | None | None | None | None | Max | Max | Max | Max | Max | Max |
| Walk Time (s) |  | 7.0 | 7.0 |  | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 |
| Flash Dont Walk (s) |  | 11.0 | 11.0 |  | 11.0 | 11.0 | 11.0 | 11.0 | 11.0 | 11.0 | 11.0 | 11.0 |
| Pedestrian Calls (\#/hr) |  | 0 | 0 |  | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Act Effct Green (s) | 14.0 | 13.2 | 13.2 | 14.0 | 13.2 | 13.2 | 18.6 | 18.6 | 18.6 | 18.6 | 18.6 | 18.6 |
| Actuated g/C Ratio | 0.33 | 0.31 | 0.31 | 0.33 | 0.31 | 0.31 | 0.44 | 0.44 | 0.44 | 0.44 | 0.44 | 0.44 |
| v/c Ratio | 0.04 | 0.61 | 0.11 | 0.05 | 0.61 | 0.06 | 0.05 | 0.00 | 0.04 | 0.02 | 0.00 | 0.01 |
| Control Delay | 7.9 | 17.6 | 1.5 | 8.0 | 17.6 | 0.2 | 10.9 | 11.0 | 0.1 | 11.0 | 11.0 | 0.0 |
| Queue Delay | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Delay | 7.9 | 17.6 | 1.5 | 8.0 | 17.6 | 0.2 | 10.9 | 11.0 | 0.1 | 11.0 | 11.0 | 0.0 |
| Baseline |  |  |  |  |  |  |  |  |  | Synchr | 10 Ligh | Report <br> Page 1 |

Synchro Model
2017 PM Peak (Proposed Operating Conditions)
27: US-36 \& 11th Rd.
Lanes, Volumes, Timings

|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |

## Intersection Summary

| Area Type: $\quad$ Other |  |
| :--- | :--- |
| Cycle Length: $60 \quad$ |  |
| Actuated Cycle Length: 42.6 |  |
| Natural Cycle: 55 |  |
| Control Type: Actuated-Uncoordinated |  |
| Maximum v/c Ratio: 0.61 | Intersection LOS: B |
| Intersection Signal Delay: 14.5 | ICU Level of Service A |
| Intersection Capacity Utilization 36.6\% |  |
| Analysis Period (min) 15 |  |

Splits and Phases: 27: US-36 \& 11th Rd.


Synchro Model
2037 PM Peak (Proposed Operating Conditions)
27: US-36 \& 11th Rd.
Lanes, Volumes, Timings

|  | $y$ |  |  |  |  | 4 | 4 | $\uparrow$ | $p$ | $\downarrow$ | $\downarrow$ | 4 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | \% | $\uparrow$ | $\overline{7}$ | 7 | $\uparrow$ | $\overline{7}$ | ${ }^{\prime}$ | $\uparrow$ | $\overline{7}$ | 7 | $\uparrow$ | $\overline{7}$ |
| Traffic Volume (vph) | 25 | 583 | 101 | 31 | 583 | 52 | 49 | 7 | 45 | 25 | 5 | 11 |
| Future Volume (vph) | 25 | 583 | 101 | 31 | 583 | 52 | 49 | 7 | 45 | 25 | 5 | 11 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Storage Length (fi) | 200 |  | 200 | 200 |  | 200 | 100 |  | 100 | 100 |  | 100 |
| Storage Lanes | 1 |  | 1 | 1 |  | 1 | 1 |  | 1 | 1 |  | 1 |
| Taper Length ( ft ) | 25 |  |  | 25 |  |  | 25 |  |  | 25 |  |  |
| Lane Util. Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Frt |  |  | 0.850 |  |  | 0.850 |  |  | 0.850 |  |  | 0.850 |
| Fil Protected | 0.950 |  |  | 0.950 |  |  | 0.950 |  |  | 0.950 |  |  |
| Satd. Flow (prot) | 1770 | 1863 | 1583 | 1770 | 1863 | 1583 | 1770 | 1863 | 1583 | 1770 | 1863 | 1583 |
| Fll Permitted | 0.300 |  |  | 0.257 |  |  | 0.754 |  |  | 0.752 |  |  |
| Satd. Flow (perm) | 559 | 1863 | 1583 | 479 | 1863 | 1583 | 1405 | 1863 | 1583 | 1401 | 1863 | 1583 |
| Right Tum on Red |  |  | Yes |  |  | Yes |  |  | Yes |  |  | Yes |
| Satd. Flow (RTOR) |  |  | 110 |  |  | 109 |  |  | 109 |  |  | 109 |
| Link Speed (mph) |  | 45 |  |  | 45 |  |  | 30 |  |  | 30 |  |
| Link Distance ( ft ) |  | 3848 |  |  | 1647 |  |  | 1088 |  |  | 1216 |  |
| Travel Time (s) |  | 58.3 |  |  | 25.0 |  |  | 24.7 |  |  | 27.6 |  |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Adj. Flow (vph) | 27 | 634 | 110 | 34 | 634 | 57 | 53 | 8 | 49 | 27 | 5 | 12 |
| Shared Lane Traffic (\%) |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane Group Flow (vph) | 27 | 634 | 110 | 34 | 634 | 57 | 53 | 8 | 49 | 27 | 5 | 12 |
| Turn Type | pm+pt | NA | Perm | pm+pt | NA | Perm | Perm | NA | Perm | Perm | NA | Perm |
| Protected Phases | 7 | 4 |  | 3 | 8 |  |  | 2 |  |  | 6 |  |
| Permitted Phases | 4 |  | 4 | 8 |  | 8 | 2 |  | 2 | 6 |  | 6 |
| Detector Phase | 7 | 4 | 4 | 3 | 8 | 8 | 2 | 2 | 2 | 6 | 6 | 6 |
| Switch Phase |  |  |  |  |  |  |  |  |  |  |  |  |
| Minimum Initial (s) | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 |
| Minimum Split (s) | 9.5 | 22.5 | 22.5 | 9.5 | 22.5 | 22.5 | 22.5 | 22.5 | 22.5 | 22.5 | 22.5 | 22.5 |
| Total Split (s) | 10.0 | 40.0 | 40.0 | 10.0 | 40.0 | 40.0 | 10.0 | 10.0 | 10.0 | 10.0 | 10.0 | 10.0 |
| Total Split (\%) | 16.7\% | 66.7\% | 66.7\% | 16.7\% | 66.7\% | 66.7\% | 16.7\% | 16.7\% | 16.7\% | 16.7\% | 16.7\% | 16.7\% |
| Maximum Green (s) | 5.5 | 35.5 | 35.5 | 5.5 | 35.5 | 35.5 | 5.5 | 5.5 | 5.5 | 5.5 | 5.5 | 5.5 |
| Yellow Time (s) | 3.5 | 3.5 | 3.5 | 3.5 | 3.5 | 3.5 | 3.5 | 3.5 | 3.5 | 3.5 | 3.5 | 3.5 |
| All-Red Time (s) | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 |
| Lost Time Adjust (s) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Lost Time (s) | 4.5 | 4.5 | 4.5 | 4.5 | 4.5 | 4.5 | 4.5 | 4.5 | 4.5 | 4.5 | 4.5 | 4.5 |
| Lead/Lag | Lead | Lag | Lag | Lead | Lag | Lag |  |  |  |  |  |  |
| Lead-Lag Optimize? | Yes | Yes | Yes | Yes | Yes | Yes |  |  |  |  |  |  |
| Vehicle Extension (s) | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 |
| Recall Mode | None | None | None | None | None | None | Min | Min | Min | Min | Min | Min |
| Walk Time (s) |  | 7.0 | 7.0 |  | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 |
| Flash Dont Walk (s) |  | 11.0 | 11.0 |  | 11.0 | 11.0 | 11.0 | 11.0 | 11.0 | 11.0 | 11.0 | 11.0 |
| Pedestrian Calls (\#/hr) |  | 0 | 0 |  | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Act Effct Green (s) | 20.4 | 18.8 | 18.8 | 21.0 | 20.3 | 20.3 | 6.2 | 6.2 | 6.2 | 6.2 | 6.2 | 6.2 |
| Actuated g/C Ratio | 0.54 | 0.50 | 0.50 | 0.55 | 0.54 | 0.54 | 0.16 | 0.16 | 0.16 | 0.16 | 0.16 | 0.16 |
| v/c Ratio | 0.05 | 0.69 | 0.13 | 0.07 | 0.63 | 0.06 | 0.23 | 0.03 | 0.14 | 0.12 | 0.02 | 0.03 |
| Control Delay | 2.7 | 11.9 | 2.0 | 2.7 | 9.2 | 0.6 | 22.9 | 21.3 | 1.8 | 22.0 | 21.4 | 0.2 |
| Queue Delay | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Delay | 2.7 | 11.9 | 2.0 | 2.7 | 9.2 | 0.6 | 22.9 | 21.3 | 1.8 | 22.0 | 21.4 | 0.2 |

Baseline
Synchro 10 Light Report
Page 1

Synchro Model
2037 PM Peak (Proposed Operating Conditions)
27: US-36 \& 11th Rd.
Lanes, Volumes, Timings

|  | 4 |  | $\checkmark$ | 1 |  | 4 | 4 | 4 | $p$ |  | $\downarrow$ | 4 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| LOS | A | B | A | A | A | A | C | C | A | C | C | A |
| Approach Delay |  | 10.1 |  |  | 8.2 |  |  | 13.4 |  |  | 16.0 |  |
| Approach LOS |  | B |  |  | A |  |  | B |  |  | B |  |
| Queue Length 50th ( ft ) | 2 | 57 | 0 | 2 | 57 | 0 | 7 | 1 | 0 | 3 | 1 | 0 |
| Queue Length 95th (ft) | 5 | 207 | 15 | 6 | 207 | 4 | 47 | 14 | 5 | 29 | 10 | 0 |
| Internal Link Dist ( t ) |  | 3768 |  |  | 1567 |  |  | 1008 |  |  | 1136 |  |
| Turn Bay Length (ft) | 200 |  | 200 | 200 |  | 200 | 100 |  | 100 | 100 |  | 100 |
| Base Capacity (vph) | 497 | 1611 | 1384 | 476 | 1611 | 1384 | 228 | 303 | 349 | 228 | 303 | 349 |
| Starvation Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Spillback Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Storage Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Reduced v/c Ratio | 0.05 | 0.39 | 0.08 | 0.07 | 0.39 | 0.04 | 0.23 | 0.03 | 0.14 | 0.12 | 0.02 | 0.03 |

## Intersection Summary

| Area Type: $\quad$ Other |  |
| :--- | :--- |
| Cycle Length: 60 |  |
| Actuated Cycle Length: 37.9 |  |
| Natural Cycle: 60 |  |
| Control Type: Actuated-Uncoordinated |  |
| Maximum v/c Ratio: 0.69 Intersection LOS: A <br> Intersection Signal Delay: 9.7 ICU Level of Service A <br> Intersection Capacity Utilization $50.3 \%$  <br> Analysis Period (min) 15  |  |

Splits and Phases: 27: US-36 \& 11th Rd.



[^0]:    Baseline Synchro 10 Light Report
    Page 5

