### 8.0 STRUCTURAL ASPECTS OF CULVERTS

The structural design of a culvert can affect its hydraulic performance and service life and the structural integrity of the highway embankment. This section presents structural design criteria and procedures for reinforced concrete pipe (RCP), corrugated metal pipe (CMP), spiral rib steel pipe (SRSP), corrugated metal, metal arch culverts (CMMAC), corrugated aluminum pipe (CAP), corrugated aluminum pipe arch (CAPA), thermoplastic pipes including polyvinyl chloride pipe (PVCP) and polyethylene pipe (PEP), and reinforced concrete box culverts (RCB) installed in embankments. This section does not cover the design of reinforced concrete elliptical and arch pipe, or other types of pipe. It also does not cover trench installations. References listed in Section 8.5 provide technical guidance on structural design for other types of pipe and other methods of installation.

Pipe culverts may be added or replaced in existing embankments by tunneling, jacking or boring. This section does not include structural criteria for tunneling, jacking or boring because these types of installations are typically done in accordance with standards set by the industry or by other governmental agencies. A special provision is required for pipe culvert installation by tunneling, jacking or boring.

The structural adequacy of a pipe or RCB culvert may need to be considered at locations with low type surfacing and minimum cover over the top of the culvert. Culverts at these locations, such as a field entrance for agricultural purposes, may be subjected to heavy loads from large trucks and/ or agricultural equipment.

### 8.1 PIPE INSTALLATION

### 8.1.1 General Procedure

The following general procedure should be used to install pipe culverts:

1. The channel or trench is graded to the appropriate elevation.
2. A pipe bed or template is formed by shaping the bottom of the channel or by placing granular material, depending on the size of the pipe.
3. The pipe is placed in the bed.
4. The channel or trench is backfilled.

Detailed information on excavation and backfill for culverts is presented in Section 204 of KDOT's Standard Specifications for State Road and Bridge Construction.

### 8.1.2 Minimum Spacing

A minimum spacing between pipes in multiple-barrel culverts is needed to permit adequate compaction of the backfill material and to provide clearance for the end sections. Standard Drawing RD668 "Miscellaneous Pipe Culvert Details" includes information to determine minimum spacing between pipes. A width to accommodate end sections should be considered.

### 8.1.3 Pipe Lengths

For constant gradient pipe culverts and erosion pipe compute and tabulate the length in multiples of 2' for concrete pipe and to the nearest 1' for metal pipe. When multiple pipe types are acceptable for use at a site, round the length to the nearest 2'. For additional information regarding pipe lengths, see the Road Design Manual.

### 8.2 REINFORCED CONCRETE PIPE

Use Table 8.2-1 to determine the maximum height of fill for RCP installed in embankments. These maximum heights of fill are based on the AASHTO LRFD Indirect Design Method (DLoad Method) and the following design criteria:

Positive projecting embankment installation

Unit weight of the fill $=120 \mathrm{lb} / \mathrm{ft}^{3}$
Type 3 Installation Type
Settlement ratio $\mathrm{r}_{\mathrm{sd}}=0.7$
D-loads for $0.01-\mathrm{in}$. crack: $\mathrm{D}_{001}=1000 \mathrm{lb} / \mathrm{ft} / \mathrm{in}$. for Class II RCP

$$
\begin{aligned}
& D_{0.01}=1350 \mathrm{lb} / \mathrm{ft} / \mathrm{in} . \text { for Class III RCP } \\
& D_{0.01}=2000 \mathrm{lb} / \mathrm{ft} / \mathrm{in} . \text { for Class IV RCP } \\
& D_{0.01}=3000 \mathrm{lb} / \mathrm{ft} / \mathrm{in} . \text { for Class V RCP }
\end{aligned}
$$

The minimum cover for RCP and reinforced concrete horizontal elliptical pipe (RCPHE) in unpaved areas and under flexible pavements is 12 in . or one-eighth of the diameter or span, whichever is greater. Under rigid pavements, the minimum cover from the top of the pipe to the top of the subgrade is 9 in . RCPHE is intended for use where the cover over the pipe is limited. RCPHE should be used only where the available cover is insufficient for RCP.

Note: Height of fill tables for RCPHE are not included in this manual.

Table 8.2-1 Design Data for RCP

| Pipe Diameter (in.) | Wall Thickness (in.) | Maximum Height of Fill (ft) |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Class II | Class III | Class IV | Class V |
| 12 | 2.00 | 10 | 14 | 21 | 33 |
| 15 | 2.25 | 10 | 14 | 22 | 33 |
| 18 | 2.50 | 10 | 14 | 22 | 33 |
| 21 | 2.75 | 10 | 14 | 22 | 33 |
| 24 | 3.00 | 10 | 14 | 22 | 33 |
| 27 | 3.25 | 10 | 14 | 21 | 33 |
| 30 | 3.50 | 10 | 14 | 21 | 33 |
| 33 | 3.75 | 9 | 14 | 21 | 32 |
| 36 | 4.00 | 9 | 13 | 21 | 32 |
| 42 | 4.50 | 9 | 13 | 21 | 32 |
| 48 | 5.00 | 9 | 13 | 21 | 32 |
| 54 | 5.50 | 9 | 13 | 20 | 32 |
| 60 | 6.00 | 9 | 13 | 20 | 31 |
| 66 | 6.50 | 8 | 12 | 20 | 31 |
| 72 | 7.00 | 8 | 12 | 20 | 31 |
| 78 | 7.50 | 8 | 12 | 20 | 31 |
| 84 | 8.00 | 8 | 12 | 19 | 31 |
| 90 | 8.50 | 8 | 12 | 19 | 31 |
| 96 | 9.00 | 8 | 12 | 19 | 30 |
| 102 | 9.50 | 8 | 12 | 19 | 30 |
| 108 | 10.00 | 8 | 12 | 19 | 30 |

Notes: Pipe diameter is inside diameter.

### 8.3 CORRUGATED METAL PIPE

Use Tables 8.3-4 through 8.3-18 to determine the required pipe gauge, maximum height of fill and minimum cover for CSP, ACSP, SRSP, and CMMAC. The minimum cover is measured from the top of the pipe to the top of the subgrade. The maximum heights of fill are based on the Load and Resistance Factor Design (LRFD) procedure. For the LRFD Service Load condition, the five percent deflection criteria remains the same as the design procedure of Wolf and Townsend (1970). The maximum heights of fill and metal thicknesses in these tables satisfy design criteria for deflection of the pipe, buckling of the pipe wall, and handling and installation strength. Height of fill tables have been provided for the sizes and types of steel pipe most commonly specified and furnished for KDOT projects. For further information, the designer should refer to Section 12 of the "AASHTO LRFD Bridge Design Specifications, 4th Edition", to determine maximum height of fill for pipe types and/or other installation methods not shown.

Following are the specific design criteria and material properties used to compute the maximum heights of fill in Tables 8.3-4 through 8.3-18.

> Positive projecting embankment installation Unit weight of fill, w $=120 \mathrm{lb} / \mathrm{ft}^{3}$ Modulus of soil reaction, $\mathrm{E}^{\prime}: 400 \mathrm{psi}, 750 \mathrm{psi}$ or 1500 psi Deflection lag factor, $\mathrm{D}_{\mathrm{L}}: \begin{aligned} & 1.75 \text { for } \mathrm{E}^{\prime}=400 \mathrm{psi} \\ & 1.48 \text { for } \mathrm{E}^{\prime}=750 \mathrm{psi} \\ & 1.25 \text { for } \mathrm{E}^{\prime}=1500 \mathrm{psi}\end{aligned}$ Soil stiffness coefficient, $\mathrm{k}: 0.66$ for $\mathrm{E}^{\prime}=400 \mathrm{psi}$ $$
\begin{array}{l}0.42 \text { for } \mathrm{E}^{\prime}=750 \mathrm{psi} \\ 0.22 \text { for } \mathrm{E}^{\prime}=1500 \mathrm{psi}\end{array}
$$ Maximum height of fill not to exceed 50 ft Minimum metal thickness $=0.079$ in. $(14$ gauge $)$ Maximum deflection $=5 \%$ of nominal diameter Modulus of elasticity of steel, $\mathrm{E}=29 \times 10^{6} \mathrm{psi}$ Tensile strength of steel, $\mathrm{f}_{\mathrm{u}}=45,000 \mathrm{psi}$

Table 8.3-1 Properties of CMP, and CMMAC

| Corrugation | Gauge | $\begin{gathered} \mathbf{A}_{s} \\ \text { (in. }{ }^{\mathbf{2} / \mathrm{ft})} \end{gathered}$ | $\begin{gathered} \text { I } \\ \text { (in. } \left.{ }^{4} / \mathrm{in} .\right) \end{gathered}$ | $\begin{gathered} \mathbf{r} \\ \text { (in.) } \end{gathered}$ |
| :---: | :---: | :---: | :---: | :---: |
| $2-2 / 3 \times 1 / 2 \mathrm{in}$. | 14 | 0.968 | 0.00239 | 0.1721 |
|  | 12 | 1.356 | 0.00343 | 0.1741 |
|  | 10 | 1.744 | 0.00453 | 0.1766 |
|  | 8 | 2.133 | 0.00573 | 0.1795 |
| $3 \times 1 \mathrm{in}$. | 14 | 1.113 | 0.01088 | 0.3427 |
|  | 12 | 1.560 | 0.01546 | 0.3448 |
|  | 10 | 2.008 | 0.02018 | 0.3472 |
|  | 8 | 2.458 | 0.02509 | 0.3499 |
| $5 \times 1$ in. | 14 | 0.992 | 0.01109 | 0.3663 |
|  | 12 | 1.390 | 0.01565 | 0.3677 |
|  | 10 | 1.788 | 0.02032 | 0.3693 |
|  | 8 | 2.186 | 0.02509 | 0.3711 |

Table 8.3-2 Properties of SRSP

| Corrugation | Gauge | $\mathbf{A}_{\mathbf{s}}$ <br> (in. $^{2} / \mathbf{f t}$ ) | $\mathbf{I}$ <br> (in. $^{4}$ /in.) | $\mathbf{r}$ <br> (in.) |
| :---: | :---: | :---: | :---: | :---: |
| $3 / 4 \times 3 / 4 \times 7-1 / 2 \mathrm{in}$. | 16 | 0.509 | 0.0028 | 0.258 |
|  | 14 | 0.712 | 0.0037 | 0.250 |
|  | 12 | 1.184 | 0.0055 | 0.237 |
|  | 10 | 1.717 | 0.0074 | 0.228 |

The maximum height of fill for a deflection of $5 \%$ is

$$
\begin{equation*}
\mathrm{H}_{\max }=7.2\left(\frac{\mathrm{EI}+0.061 \mathrm{R}^{3} \mathrm{E}^{\prime}}{\mathrm{D}_{\mathrm{L}} K w \mathrm{R}^{3}}\right) \tag{8-1}
\end{equation*}
$$

$$
\text { where: } \begin{aligned}
\mathrm{H}_{\max } & =\text { maximum height of fill above top of pipe }(\mathrm{ft}) \\
\mathrm{E} & =\text { modulus of elasticity of pipe material }(\mathrm{psi}) \\
\mathrm{I} & \left.=\text { moment of inertia of pipe wall (in. } .^{4} / \mathrm{in} .\right) \\
\mathrm{R} & =\text { nominal radius of pipe (in.) } \\
\mathrm{E}^{\prime} & =\text { modulus of soil reaction }(\mathrm{psi}) \\
\mathrm{D}_{\mathrm{L}} & =\text { deflection lag factor } \\
\mathrm{K} & =\text { bedding constant, } 0.1 \\
\mathrm{w} & =\text { unit weight of fill }\left(\mathrm{lb} / \mathrm{ft}^{3}\right)
\end{aligned}
$$

The maximum height of fill for buckling of the pipe wall and flexibility factor may be determined from information in the AASHTO LRFD Bridge Design Specifications; 4th Edition, Section 12.

The minimum cover for CMP, and CMMAC, is 12 in . or one-eighth of the diameter or span, whichever is greater. The minimum cover for SRSP is 12 in . or one-fourth of the diameter or span, whichever is greater.

Pipe arches are intended for use where the cover over the pipe is limited. CMMAC should be used only where the available cover is insufficient for CMP.

While special bedding, vertical elongation and other practices can increase the maximum height of fill, these practices are usually not economical for highway construction. Use of these techniques should be justified by a comparison of costs.

The value of the modulus of soil reaction, E', will be recommended by the Geotechnical Section of the Bureau of Structures and Geotechnical Services, and may be found in the Soils Report or the Geotechnical Recommendations. If a value of $\mathrm{E}^{\prime}$ is not provided, it can be estimated from Table 8-3-3. The Geotechnical Section should be consulted for assistance.

Table 8.3-3 Guidance for Estimation of the Modulus of Soil Reaction, E'

| $\begin{array}{c}\text { Soil type for pipe bedding } \\ \text { material }\end{array}$ | $\mathbf{E}^{\prime}$ (psi) for Specified Compaction of Bedding |  |  |
| :--- | :---: | :---: | :---: | :---: | :---: |$\}$

${ }^{\mathrm{a}}$ Slight compaction $=<85 \%$ Proctor, $<40 \%$ relative density
${ }^{\mathrm{b}}$ Moderate compaction $=85 \%-95 \%$ Proctor, $40 \%-70 \%$ relative density
${ }^{\mathrm{c}}$ High compaction $=>95 \%$ Proctor, $>70 \%$ relative density
${ }^{\mathrm{d}} \mathrm{LL}=$ liquid limits

In certain situations, such as where existing soils have high plasticity, compacted granular backfill may be required to provide an adequate soil envelope around the pipe. In these situations the Soils Report will recommend granular material for backfill. Locations where compacted granular backfill is required should be noted on the plans.

Table 8.3-4 Design Data for CMP with 2-2/3 x $1 / 2 \mathrm{in}$. Corrugations, $\mathrm{E}^{\prime}=\mathbf{4 0 0} \mathbf{~ p s i}$

| Diameter <br> (in.) | Minimum Cover <br> (in.) | Maximum Height of Fill (ft) |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Pipe Gauge |  |  |  |
|  |  | 14 Gauge | 12 Gauge | 10 Gauge | 8 Gauge |
| 12 | 12 | 50 |  |  |  |
| 15 | 12 | 50 |  |  |  |
| 18 | 12 | 41 |  |  |  |
| 21 | 12 | 29 |  |  |  |
| 24 | 12 | 22 | 28 |  |  |
| 30 | 12 | 15 | 18 |  |  |
| 36 | 12 | 12 | 14 | 16 |  |
| 42 | 12 | 11 | 12 | 13 | 15 |
| 48 | 12 | 10 | 11 | 12 | 12 |
| 54 | 12 | 10 | 10 | 11 | 11 |
| 60 | 12 |  | 10 | 10 | 10 |
| 66 | 12 |  |  | 10 | 10 |
| 72 | 12 |  |  | 9 | 10 |
| 78 | 12 |  |  |  | 9 |
| 84 | 12 |  |  |  | 8 |

Table 8.3-5 Design Data for CMP with 2-2/3 $\times 1 / 2 \mathrm{in}$. Corrugations, $\mathrm{E}^{\prime}=750 \mathrm{psi}$

| Diameter <br> (in.) | Minimum <br> Cover <br> (in.) | Maximum Height of Fill (ft) |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Pipe Gauge |  |  |  |
|  |  | 14 Gauge | 12 Gauge | 10 Gauge | 8 Gauge |
| 12 | 12 | 50 |  |  |  |
| 15 | 12 | 50 |  |  |  |
| 18 | 12 | 50 |  |  |  |
| 21 | 12 | 43 |  |  |  |
| 24 | 12 | 35 | 42 |  |  |
| 30 | 12 | 27 | 30 |  |  |
| 36 | 12 | 23 | 25 | 28 |  |
| 42 | 12 | 22 | 23 | 24 | 26 |
| 48 | 12 | 21 | 21 | 22 | 23 |
| 54 | 12 | 20 | 21 | 21 | 22 |
| 60 | 12 |  | 20 | 21 | 21 |
| 66 | 12 |  |  | 20 | 20 |
| 72 | 12 |  |  | 20 | 20 |
| 78 | 12 |  |  |  | 20 |
| 84 | 12 |  |  |  | 19 |

Table 8.3-6 Design Data for CMP with 2-2/3 $\times 1 / 2 \mathrm{in}$. Corrugations, $\mathrm{E}^{\prime}=1500 \mathrm{psi}$

| Diameter <br> (in.) | Minimum <br> Cover <br> (in.) | Maximum Height of Fill (ft) |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Pipe Gauge |  |  |  |
|  |  | 14 Gauge | 12 Gauge | 10 Gauge | 8 Gauge |
| 12 | 12 | 50 |  |  |  |
| 15 | 12 | 50 |  |  |  |
| 18 | 12 | 50 |  |  |  |
| 21 | 12 | 50 |  |  |  |
| 24 | 12 | 50 | 50 |  |  |
| 30 | 12 | 50 | 50 |  |  |
| 36 | 12 | 50 | 50 | 50 |  |
| 42 | 12 | 48 | 49 | 50 | 50 |
| 48 | 12 | 46 | 47 | 48 | 50 |
| 54 | 12 | 46 | 46 | 47 | 48 |
| 60 | 12 |  | 46 | 46 | 47 |
| 66 | 12 |  |  | 46 | 46 |
| 72 | 12 |  |  | 45 | 46 |
| 78 | 12 |  |  |  | 45 |
| 84 | 12 |  |  |  | 45 |

Table 8.3-7 Design Data for CMP with $3 \times 1 \mathrm{in}$. Corrugations, $\mathrm{E}^{\prime}=400 \mathrm{psi}$

| Diameter <br> (in.) | Minimum Cover <br> (in.) | Maximum Height of Fill (ft) |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Pipe Gauge |  |  |  |  |
|  |  | *16 Gauge | 14 Gauge | 12 Gauge | 10 Gauge | 8 Gauge |
| 48 | 12 | 15 | 16 | 19 | 23 | 26 |
| 54 | 12 | 13 | 14 | 16 | 19 | 21 |
| 60 | 12 | 12 | 12 | 14 | 16 | 18 |
| 66 | 12 | 11 | 11 | 13 | 14 | 15 |
| 72 | 12 | 10 | 11 | 12 | 13 | 14 |
| 78 | 12 |  | 10 | 11 | 12 | 13 |
| 84 | 12 |  | 10 | 10 | 11 | 12 |
| 90 | 12 |  | 10 | 10 | 11 | 11 |
| 96 | 12 |  | 9 | 10 | 10 | 11 |
| 102 | 18 |  |  | 10 | 10 | 10 |
| 108 | 18 |  |  | 9 | 10 | 10 |
| 114 | 18 |  |  | 9 | 9 | 10 |
| 120 | 18 |  |  |  | 9 | 10 |

* ACSP Only

Table 8.3-8 Design Data for CMP with $3 \times 1 \mathrm{in}$. Corrugations, $\mathrm{E}^{\prime}=750 \mathrm{psi}$

| Diameter <br> (in.) | Minimum Cover <br> (in.) | Maximum Height of Fill (ft) |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Pipe Gauge |  |  |  |  |
|  |  | *16 Gauge | 14 Gauge | 12 Gauge | 10 Gauge | 8 Gauge |
| 48 | 12 | 26 | 28 | 32 | 36 | 40 |
| 54 | 12 | 24 | 25 | 28 | 31 | 34 |
| 60 | 12 | 22 | 23 | 25 | 27 | 29 |
| 66 | 12 | 21 | 22 | 24 | 25 | 27 |
| 72 | 12 | 21 | 21 | 22 | 24 | 25 |
| 78 | 12 |  | 21 | 22 | 23 | 24 |
| 84 | 12 |  | 20 | 21 | 22 | 23 |
| 90 | 12 |  | 20 | 21 | 21 | 22 |
| 96 | 12 |  | 20 | 20 | 21 | 21 |
| 102 | 18 |  |  | 20 | 20 | 21 |
| 108 | 18 |  |  | 20 | 20 | 20 |
| 114 | 18 |  |  | 20 | 20 | 20 |
| 120 | 18 |  |  |  | 20 | 20 |

* ACSP Only

Table 8.3-9 Design Data for CMP with $3 \times 1 \mathrm{in}$. Corrugations, $\mathrm{E}^{\prime}=1500 \mathrm{psi}$

| Diameter <br> (in.) | Minimum Cover <br> (in.) | Maximum Height of Fill (ft) |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Pipe Gauge |  |  |  |  |
|  |  | *16 Gauge | 14 Gauge | 12 Gauge | 10 Gauge | 8 Gauge |
| 48 | 12 | 50 | 50 | 50 | 50 | 50 |
| 54 | 12 | 50 | 50 | 50 | 50 | 50 |
| 60 | 12 | 48 | 50 | 50 | 50 | 50 |
| 66 | 12 | 43 | 48 | 50 | 50 | 50 |
| 72 | 12 | 40 | 47 | 49 | 50 | 50 |
| 78 | 12 |  | 46 | 48 | 49 | 50 |
| 84 | 12 |  | 43 | 47 | 48 | 49 |
| 90 | 12 |  | 40 | 46 | 47 | 48 |
| 96 | 12 |  | 37 | 46 | 46 | 47 |
| 102 | 18 |  |  | 46 | 46 | 47 |
| 108 | 18 |  |  | 45 | 46 | 46 |
| 114 | 18 |  |  | 44 | 45 | 46 |
| 120 | 18 |  |  |  | 45 | 46 |

* ACSP Only

Table 8.3-10 Design Data for CMP with $5 \times 1 \mathrm{in}$. Corrugations, $\mathrm{E}^{\prime}=400 \mathrm{psi}$

| Diameter <br> (in.) | Minimum Cover <br> (in.) | Maximum Height of Fill (ft) |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Pipe Gauge |  |  |  |  |
|  |  | *16 Gauge | 14 Gauge | 12 Gauge | 10 Gauge | 8 Gauge |
| 48 | 12 | 15 | 16 | 20 | 23 | 26 |
| 54 | 12 | 13 | 14 | 16 | 19 | 21 |
| 60 | 12 | 12 | 12 | 14 | 16 | 18 |
| 66 | 12 | 11 | 11 | 13 | 14 | 15 |
| 72 | 12 | 10 | 11 | 12 | 13 | 14 |
| 78 | 12 |  | 10 | 11 | 12 | 13 |
| 84 | 12 |  | 10 | 10 | 11 | 12 |
| 90 | 12 |  | 10 | 10 | 11 | 11 |
| 96 | 12 |  |  | 10 | 10 | 11 |
| 102 | 18 |  |  | 10 | 10 | 10 |
| 108 | 18 |  |  | 9 | 10 | 10 |
| 114 | 18 |  |  | 9 | 9 | 10 |
| 120 | 18 |  |  |  | 9 | 10 |

* ACSP Only

Table 8.3-11 Design Data for CMP with $5 \times 1 \mathrm{in}$. Corrugations, $\mathrm{E}^{\prime}=750 \mathrm{psi}$

| Diameter <br> (in.) | Minimum <br> Cover <br> (in.) | Maximum Height of Fill (ft) |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Pipe Gauge |  |  |  |  |
|  |  | *16 Gauge | 14 Gauge | 12 Gauge | 10 Gauge | 8 Gauge |
| 48 | 12 | 26 | 28 | 32 | 36 | 40 |
| 54 | 12 | 24 | 25 | 28 | 31 | 34 |
| 60 | 12 | 22 | 23 | 25 | 27 | 29 |
| 66 | 12 | 21 | 22 | 24 | 25 | 27 |
| 72 | 12 | 21 | 21 | 22 | 24 | 25 |
| 78 | 12 |  | 21 | 22 | 23 | 24 |
| 84 | 12 |  | 20 | 21 | 22 | 23 |
| 90 | 12 |  | 20 | 21 | 21 | 22 |
| 96 | 12 |  |  | 20 | 21 | 21 |
| 102 | 18 |  |  | 20 | 20 | 21 |
| 108 | 18 |  |  | 20 | 20 | 20 |
| 114 | 18 |  |  | 20 | 20 | 20 |
| 120 | 18 |  |  |  | 20 | 20 |

* ACSP Only

Table 8.3-12 Design Data for CMP with $5 \times 1 \mathrm{in}$. Corrugations, $\mathrm{E}^{\prime}=1500 \mathrm{psi}$

| Diameter <br> (in.) | Minimum Cover <br> (in.) | Maximum Height of Fill (ft) |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Pipe Gauge |  |  |  |  |
|  |  | *16 Gauge | 14 Gauge | 12 Gauge | 10 Gauge | 8 Gauge |
| 48 | 12 | 50 | 50 | 50 | 50 | 50 |
| 54 | 12 | 47 | 50 | 50 | 50 | 50 |
| 60 | 12 | 43 | 50 | 50 | 50 | 50 |
| 66 | 12 | 39 | 48 | 50 | 50 | 50 |
| 72 | 12 | 36 | 44 | 49 | 50 | 50 |
| 78 | 12 |  | 41 | 48 | 49 | 50 |
| 84 | 12 |  | 38 | 47 | 48 | 49 |
| 90 | 12 |  | 36 | 46 | 47 | 48 |
| 96 | 12 |  |  | 46 | 46 | 47 |
| 102 | 18 |  |  | 44 | 46 | 47 |
| 108 | 18 |  |  | 41 | 46 | 46 |
| 114 | 18 |  |  | 39 | 45 | 46 |
| 120 | 18 |  |  |  | 45 | 46 |

* ACSP Only

Table 8.3-13 Design Data for SRSP with $3 / 4 \times 3 / 4 \times 7-1 / 2 \mathrm{in}$. Corrugations, $\mathrm{E}^{\prime}=400 \mathrm{psi}$

| Diameter <br> (in.) | Minimum <br> Cover <br> (in.) | Maximum Height of Fill (ft) |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Pipe Gauge |  |  |  |
|  |  | *16 Gauge | 14 Gauge | 12 Gauge | 10 Gauge |
| 24 | 12 | 25 | 30 | 40 |  |
| 30 | 12 | 17 | 19 | 25 |  |
| 36 | 12 | 13 | 15 | 18 |  |
| 42 | 12 | 11 | 12 | 14 |  |
| 48 | 12 | 10 | 11 | 12 | 14 |
| 54 | 15 |  | 10 | 11 | 12 |
| 60 | 15 |  | 10 | 10 | 11 |
| 66 | 18 |  |  | 10 | 10 |
| 72 | 18 |  |  | 10 | 10 |
| 78 | 21 |  |  | 9 | 10 |
| 84 | 21 |  |  |  | 9 |
| 90 | 24 |  |  |  | 9 |

* Aluminized SRSP only

Note: Based on embankment Installation

Table 8.3-14 Design Data for SRSP with $3 / 4 \times 3 / 4 \times 7-1 / 2 \mathrm{in}$. Corrugations, $\mathrm{E}^{\prime}=750 \mathrm{psi}$

| Diameter <br> (in.) | Minimum <br> Cover <br> (in.) | Maximum Height of Fill (ft) |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Pipe Gauge |  |  |  |
|  |  | *16 Gauge | 14 Gauge | 12 Gauge | 10 Gauge |
| 24 | 12 | 38 | 44 | 50 |  |
| 30 | 12 | 28 | 31 | 38 |  |
| 36 | 12 | 24 | 26 | 30 |  |
| 42 | 12 | 22 | 23 | 26 |  |
| 48 | 12 | 21 | 22 | 23 | 25 |
| 54 | 15 |  | 21 | 22 | 23 |
| 60 | 15 |  | 20 | 21 | 22 |
| 66 | 18 |  |  | 20 | 21 |
| 72 | 18 |  |  | 20 | 20 |
| 78 | 21 |  |  | 20 | 20 |
| 84 | 21 |  |  |  | 20 |
| 90 | 24 |  |  |  | 20 |

* Aluminized SRSP only

Note: Based on embankment installation

Table 8.3-15 Design Data for SRSP with $3 / 4 \times 3 / 4 \times 7-1 / 2$ in. Corrugations, $\mathbf{E}^{\prime}=1500$ psi

| Diameter <br> (in.) | Minimum <br> Cover <br> (in.) | Maximum Height of Fill (ft) |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Pipe Gauge |  |  |  |
|  |  | *16 Gauge | 14 Gauge | 12 Gauge | 10 Gauge |
| 24 | 12 | 50 | 50 | 50 |  |
| 30 | 12 | 50 | 50 | 50 |  |
| 36 | 12 | 46 | 50 | 50 |  |
| 42 | 12 | 39 | 49 | 50 |  |
| 48 | 12 | 34 | 48 | 49 | 50 |
| 54 | 15 |  | 43 | 48 | 49 |
| 60 | 15 |  | 38 | 47 | 48 |
| 66 | 18 |  |  | 46 | 47 |
| 72 | 18 |  |  | 46 | 46 |
| 78 | 21 |  |  | 45 | 46 |
| 84 | 21 |  |  |  | 45 |
| 90 | 24 |  |  |  | 45 |

* Aluminized SRSP only

Note: Based on embankment installation

Table 8.3-16 Design Data for CMMAC with 2-2/3 x 1/2 in. Corrugations

| Span x Rise (in.) | MinimumGauge | Minimum Cover (in.) | Maximum Height of <br> Fill* (ft) |
| :---: | :---: | :---: | :---: |
| $17 \times 13$ | 14 | 12 | 13 |
| $21 \times 15$ | 14 | 12 | 12 |
| $24 \times 18$ | 14 | 12 | 13 |
| $28 \times 20$ | 14 | 12 | 12 |
| $35 \times 24$ | 14 | 12 | 12 |
| $42 \times 29$ | 14 | 12 | 12 |
| $49 \times 33$ | 12 | 12 | 12 |
| $57 \times 38$ | 10 | 12 | 12 |
| $71 \times 47$ | 8 | 12 | 12 |
| $77 \times 52$ | 8 | 12 | 12 |
| $83 \times 57$ | 12 | 12 | 12 |

*For soil bearing capacity of 2 tons $/ \mathrm{ft}^{2}$ around corners of pipe

Table 8.3-17 Design Data for CMMAC with $3 \times 1 \mathrm{in}$. Corrugations

| Span x Rise (in.) | MinimumGauge | Minimum Cover (in.) | Maximum Height of Fill* (ft) |
| :---: | :---: | :---: | :---: |
| $53 \times 41$ | 14 | 12 | 21 |
| $60 \times 46$ | 14 | 15 | 20 |
| $66 \times 51$ | 14 | 15 | 20 |
| $73 \times 55$ | 14 | 18 | 20 |
| $81 \times 59$ | 14 | 18 | 17 |
| $87 \times 63$ | 14 | 18 | 16 |
| $95 \times 67$ | 12 | 21 | 16 |
| $103 \times 71$ | 12 | 21 | 16 |
| $112 \times 75$ | 12 | 24 | 16 |
| $117 \times 79$ | 10 | 24 | 16 |
| $128 \times 83$ | 10 | 27 | 16 |
| $137 \times 87$ | 8 | $14 \times 91$ | 14 |

*For soil bearing capacity of 2 tons/ft ${ }^{2}$ around corners of pipe

Table 8.3-18 Design Data for CMMAC with $5 \times 1$ in. Corrugations

| Span x Rise (in.) | MinimumGauge | Minimum Cover (in.) | Maximum Height of Fill* (ft) |
| :---: | :---: | :---: | :---: |


| $81 \times 59$ | 12 | 18 | 17 |
| :---: | :---: | :---: | :---: |
| $87 \times 63$ | 12 | 18 | 16 |
| $95 \times 67$ | 12 | 18 | 16 |
| $103 \times 71$ | 12 | 18 | 16 |
| $112 \times 75$ | 12 | 21 | 16 |
| $117 \times 79$ | 12 | 21 | 16 |
| $128 \times 83$ | 10 | 24 | 16 |
| $137 \times 87$ | 10 | 24 | 16 |
| $142 \times 91$ | 8 | 27 | 16 |

[^0]
### 8.4 CORRUGATED ALUMINUM PIPE

Use Tables 8.4-3 through 8.4-10 to determine the required pipe gauge, maximum height of fill and minimum cover for corrugated aluminum pipe (CAP) and Corrugated Aluminum Pipe Arch (CAPA). The minimum cover is measured from the top of the pipe to the top of the subgrade. The maximum heights of fill are based on the Load and Resistance Factor Design (LRFD) procedure. For the LRFD Service Load condition, the five percent deflection criteria remains the same as the design procedure of Wolf and Townsend (1970). The maximum heights of fill and metal thicknesses in these tables satisfy design criteria for deflection of the pipe, buckling of the pipe wall, and handling and installation strength. Height of fill tables have been provided for the sizes and types of aluminum pipe most commonly specified and furnished for KDOT projects. For further information the designer should refer to Section 12 of the "AASHTO LRFD Bridge Design Specifications, 4th Edition", to determine maximum height of fill for pipe types and/or other installation methods not shown.

Following are the specific design criteria and material properties used to compute the maximum heights of fill in Tables 8.4-3 through 8.4-10.

Positive projecting embankment installation
Unit weight of fill, $w=120 \mathrm{lb} / \mathrm{ft}^{3}$
Modulus of soil reaction, E': $400 \mathrm{psi}, 750 \mathrm{psi}$ or 1500 psi
Deflection lag factor, $\mathrm{D}_{\mathrm{L}}: 1.75$ for $\mathrm{E}^{\prime}=400 \mathrm{psi}$

$$
1.48 \text { for } \mathrm{E}^{\prime}=750 \mathrm{psi}
$$

$$
1.25 \text { for } \mathrm{E}^{\prime}=1500 \mathrm{psi}
$$

Soil stiffness coefficient, $\mathrm{k}: 0.66$ for $\mathrm{E}^{\prime}=400 \mathrm{psi}$

$$
0.42 \text { for } \mathrm{E}^{\prime}=750 \mathrm{psi}
$$

0.22 for $\mathrm{E}^{\prime}=1500 \mathrm{psi}$

Maximum height of fill not to exceed 50 ft
Minimum metal thickness $=0.060 \mathrm{in}$. ( 16 gauge $)$
Maximum deflection $=5 \%$ of nominal diameter
Modulus of elasticity of aluminum, $\mathrm{E}=10 \times 10^{6} \mathrm{psi}$
Tensile strength of aluminum, $f u=27,000 \mathrm{psi}$

CAP and CAPA: Helical lockseam or continuously welded seams

Table 8.4-1 Properties of CAP

| Corrugation | Gauge | $\begin{gathered} \mathbf{A}_{s} \\ \text { (in. } \left.{ }^{\mathbf{2}} / \mathrm{ft}\right) \end{gathered}$ | $\begin{gathered} \text { I } \\ \text { (in. } \left.{ }^{4} / \mathrm{in} .\right) \end{gathered}$ | $\begin{gathered} \mathbf{r} \\ \text { (in.) } \end{gathered}$ |
| :---: | :---: | :---: | :---: | :---: |
| $2-2 / 3 \times 1 / 2 \mathrm{in}$. | 16 | 0.775 | 0.001892 | 0.1712 |
|  | 14 | 0.968 | 0.002392 | 0.1721 |
|  | 12 | 1.356 | 0.003425 | 0.1741 |
|  | 10 | 1.745 | 0.004533 | 0.1766 |
|  | 8 | 2.133 | 0.005725 | 0.1795 |
| $3 \times 1$ in. | 16 | 0.89 | 0.008659 | 0.3417 |
|  | 14 | 1.118 | 0.010883 | 0.3427 |
|  | 12 | 1.560 | 0.015459 | 0.3448 |
|  | 10 | 2.008 | 0.020183 | 0.3472 |
|  | 8 | 2.458 | 0.025091 | 0.3499 |

The maximum height of fill for a deflection of $5 \%$ is

$$
\begin{equation*}
H_{\max }=7.2\left(\frac{E I+0.061 \mathrm{R}^{3} \mathrm{E}^{\prime}}{\mathrm{D}_{\mathrm{L}} \mathrm{KwR}^{3}}\right) \tag{8-1}
\end{equation*}
$$

where: $\mathrm{H}_{\max }=$ maximum height of fill above top of pipe (ft)

$$
\begin{aligned}
& \mathrm{E}=\text { modulus of elasticity of pipe material }(\mathrm{psi}) \\
& \left.\mathrm{I}=\text { moment of inertia of pipe wall (in. }{ }^{4} / \mathrm{in} .\right) \\
& \mathrm{R}=\text { nominal radius of pipe }(\mathrm{in} .) \\
& \mathrm{E}^{\prime}=\text { modulus of soil reaction }(\mathrm{psi}) \\
& \mathrm{D}_{\mathrm{L}}=\text { deflection lag factor } \\
& \mathrm{K}=\text { bedding constant, } 0.1 \\
& \mathrm{w}=\text { unit weight of fill }\left(\mathrm{lb} / \mathrm{ft}^{3}\right)
\end{aligned}
$$

The maximum height of fill for buckling of the pipe wall and flexibility factor may be determined from information in the "AASHTO LRFD Bridge Design Specifications, 4th Edition", Section 12.

The minimum cover for CAP and CAPA is as shown on the height of fill tables.
While special bedding, vertical elongation and other practices can increase the maximum height of fill, these practices are usually not economical for highway construction. Use of these techniques should be justified by a comparison of costs.

The value of the modulus of soil reaction, $\mathrm{E}^{\prime}$, will be recommended by the Geotechnical Section of the Bureau of Structures and Geotechnical Services, and may be found in the Soils Report or the Geotechnical Recommendations. If a value of $\mathrm{E}^{\prime}$ is not provided, it can be estimated from Table 8.4-2. The Geotechnical Section should be consulted for assistance.

Table 8.4-2 Guidance for Estimation of the Modulus of Soil Reaction, $\mathbf{E}^{\prime}$

| $\begin{array}{c}\text { Soil type for pipe bedding } \\ \text { material }\end{array}$ | $\mathbf{E}^{\prime}$ (psi) for Specified Compaction of Bedding |  |  |
| :--- | :---: | :---: | :---: | :---: | :---: |$\}$

${ }^{\mathrm{a}}$ Slight compaction $=<85 \%$ Proctor, $<40 \%$ relative density
${ }^{\mathrm{b}}$ Moderate compaction $=85 \%-95 \%$ Proctor, $40 \%-70 \%$ relative density
${ }^{\mathrm{c}}$ High compaction $=>95 \%$ Proctor, $>70 \%$ relative density
${ }^{\mathrm{d}} \mathrm{LL}=$ liquid limits

In certain situations, such as where existing soils have high plasticity, compacted granular backfill may be required to provide an adequate soil envelope around the pipe. In these situations the Soils Report will recommend granular material for backfill. Locations where compacted granular backfill is required should be noted on the plans.

Table 8.4-3 Design Data for CAP with 2-2/3 $\times 1 / 2 \mathrm{in}$. Corrugations, $\mathrm{E}^{\prime}=400 \mathrm{psi}$

| Diameter <br> (in.) | Minimum Cover* <br> (in.) | Maximum Height of Fill* (ft) |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Pipe Gauge |  |  |  |  |
|  |  | 16 Gauge | 14 Gauge | 12 Gauge | 10 Gauge | 8 Gauge |
| 12 | 12 | 38 | 46 |  |  |  |
| 15 | 12 | 24 | 28 |  |  |  |
| 18 | 12 | 17 | 20 |  |  |  |
| 21 | 12 | 14 | 15 |  |  |  |
| 24 | 12 | 12 | 13 | 15 |  |  |
| 27 | 12 |  | 12 | 13 |  |  |
| 30 | 12 |  | 11 | 12 |  |  |
| 36 | 12 |  | 10 | 10 | 11 |  |
| 42 | 12 |  |  | 10 | 10 |  |
| 48 | 12 |  |  | 9 | 9 | 10 |
| 54 | 15 |  |  | 5 | 9 | 9 |
| 60 | 15 |  |  |  | 5 | 7 |
| 66 | 18 |  |  |  |  | 4 |
| 72 | 18 |  |  |  |  | 4 |

*Top of pipe to top of sub-grade

Table 8.4-4 Design Data for CAP with 2-2/3 $\times 1 / 2 \mathrm{in}$. Corrugations, $\mathrm{E}^{\prime}=750 \mathrm{psi}$

| Diameter <br> (in.) | Minimum <br> Cover* <br> (in.) | Maximum Height of Fill* (ft) |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Pipe Gauge |  |  |  |  |
|  |  | 16 Gauge | 14 Gauge | 12 Gauge | 10 Gauge | 8 Gauge |
| 12 | 12 | 50 | 50 |  |  |  |
| 15 | 12 | 37 | 42 |  |  |  |
| 18 | 12 | 29 | 32 |  |  |  |
| 21 | 12 | 25 | 27 |  |  |  |
| 24 | 12 | 23 | 24 | 27 |  |  |
| 27 | 12 |  | 22 | 24 |  |  |
| 30 | 12 |  | 21 | 23 |  |  |
| 36 | 12 |  | 20 | 21 | 22 |  |
| 42 | 12 |  |  | 20 | 21 |  |
| 48 | 12 |  |  | 20 | 20 | 20 |
| 54 | 15 |  |  | 17 | 19 | 20 |
| 60 | 15 |  |  |  | 17 | 19 |
| 66 | 18 |  |  |  |  | 16 |
| 72 | 18 |  |  |  |  | 12 |

*Top of pipe to top of sub-grade

Table 8.4-5 Design Data for CAP with 2-2/3 $\times 1 / 2 \mathrm{in}$. Corrugations, $\mathrm{E}^{\prime}=1500 \mathrm{psi}$

| Diameter <br> (in.) | Minimum <br> Cover* <br> (in.) | Maximum Height of Fill* (ft) |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Pipe Gauge |  |  |  |  |
|  |  | 16 Gauge | 14 Gauge | 12 Gauge | 10 Gauge | 8 Gauge |
| 12 | 12 | 50 | 50 |  |  |  |
| 15 | 12 | 50 | 50 |  |  |  |
| 18 | 12 | 50 | 50 |  |  |  |
| 21 | 12 | 50 | 50 |  |  |  |
| 24 | 12 | 49 | 50 | 50 |  |  |
| 27 | 12 |  | 49 | 50 |  |  |
| 30 | 12 |  | 47 | 49 |  |  |
| 36 | 12 |  | 46 | 47 | 48 |  |
| 42 | 12 |  |  | 46 | 46 |  |
| 48 | 12 |  |  | 45 | 45 | 46 |
| 54 | 15 |  |  | 45 | 45 | 45 |
| 60 | 15 |  |  |  | 45 | 45 |
| 66 | 18 |  |  |  |  | 45 |
| 72 | 18 |  |  |  |  | 44 |

*Top of pipe to top of sub-grade

Table 8.4-6 Design Data for CAP with $3 \times 1 \mathrm{in}$. Corrugations, $\mathrm{E}^{\prime}=400 \mathrm{psi}$

| Diameter <br> (in.) | Minimum <br> Cover* <br> (in.) | Maximum Height of Fill* (ft) |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Pipe Gauge |  |  |  |  |
|  |  | 16 Gauge | 14 Gauge | 12 Gauge | 10 Gauge | 8 Gauge |
| 30 | 12 | 17 | 19 |  |  |  |
| 36 | 12 | 13 | 15 |  |  |  |
| 42 | 12 | 12 | 12 | 14 |  |  |
| 48 | 12 | 11 | 11 | 12 | 13 |  |
| 54 | 15 | 10 | 10 | 11 | 12 |  |
| 60 | 15 | 9 | 10 | 10 | 11 | 12 |
| 66 | 18 | 9 | 9 | 10 | 10 | 11 |
| 72 | 18 | 6 | 9 | 10 | 10 | 10 |
| 78 | 21 |  | 6 | 9 | 10 | 10 |
| 84 | 21 |  |  | 8 | 9 | 10 |
| 90 | 24 |  |  |  | 9 | 9 |
| 96 | 24 |  |  |  | 6 | 8 |
| 102 | 24 |  |  |  |  | 6 |
| 108 | 24 |  |  |  |  |  |
| 114 | 24 |  |  |  |  |  |
| 120 | 24 |  |  |  |  |  |

*Top of pipe to top of sub-grade

Table 8.4-7 Design Data for CAP with $3 \times 1 \mathrm{in}$. Corrugations, $\mathrm{E}^{\prime}=750 \mathrm{psi}$

| Diameter <br> (in.) | Minimum <br> Cover* <br> (in.) | Maximum Height of Fill* (ft) |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Pipe Gauge |  |  |  |  |
|  |  | 16 Gauge | 14 Gauge | 12 Gauge | 10 Gauge | 8 Gauge |
| 30 | 12 | 28 | 31 |  |  |  |
| 36 | 12 | 25 | 26 |  |  |  |
| 42 | 12 | 22 | 23 | 25 |  |  |
| 48 | 12 | 21 | 22 | 23 | 24 |  |
| 54 | 15 | 20 | 21 | 22 | 23 |  |
| 60 | 15 | 20 | 20 | 21 | 22 | 22 |
| 66 | 18 | 20 | 20 | 20 | 21 | 21 |
| 72 | 18 | 18 | 19 | 20 | 20 | 21 |
| 78 | 21 |  | 18 | 20 | 20 | 20 |
| 84 | 21 |  |  | 19 | 20 | 20 |
| 90 | 24 |  |  | 17 | 19 | 20 |
| 96 | 24 |  |  | 14 | 19 | 19 |
| 102 | 24 |  |  |  | 16 | 19 |
| 108 | 24 |  |  |  | 13 | 16 |
| 114 | 24 |  |  |  |  | 13 |
| 120 | 24 |  |  |  |  | 12 |

*Top of pipe to top of sub-grade

Table 8.4-8 Design Data for CAP with $3 \times 1 \mathrm{in}$. Corrugations, $\mathrm{E}^{\prime}=1500 \mathrm{psi}$

| Diameter <br> (in.) | Minimum <br> Cover* <br> (in.) | Maximum Height of Fill* (ft) |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Pipe Gauge |  |  |  |  |
|  |  | 16 Gauge | 14 Gauge | 12 Gauge | 10 Gauge | 8 Gauge |
| 30 | 12 | 50 | 50 |  |  |  |
| 36 | 12 | 48 | 50 |  |  |  |
| 42 | 12 | 41 | 50 | 50 |  |  |
| 48 | 12 | 36 | 46 | 49 | 50 |  |
| 54 | 15 | 32 | 40 | 48 | 49 |  |
| 60 | 15 | 29 | 36 | 47 | 48 | 48 |
| 66 | 18 | 26 | 33 | 46 | 47 | 47 |
| 72 | 18 | 24 | 30 | 42 | 46 | 47 |
| 78 | 21 |  | 28 | 39 | 46 | 46 |
| 84 | 21 |  |  | 36 | 45 | 46 |
| 90 | 24 |  |  | 34 | 45 | 45 |
| 96 | 24 |  |  | 32 | 42 | 45 |
| 102 | 24 |  |  |  | 40 | 45 |
| 108 | 24 |  |  |  | 38 | 44 |
| 114 | 24 |  |  |  |  | 40 |
| 120 | 24 |  |  |  |  | 37 |

*Top of pipe to top of sub-grade

Table 8.4-9 Design Data for CAPA with 2-2/3 x 1/2 in. Corrugations

| Span x Rise (in.) | Minimum Gauge | Minimum Cover <br> (in.) | Maximum Height of <br> Fill*(ft) |
| :---: | :---: | :---: | :---: |
| $17 \times 13$ | 16 | 12 | 13 |
| $21 \times 15$ | 16 | 12 | 12 |
| $24 \times 18$ | 16 | 12 | 13 |
| $28 \times 20$ | 14 | 12 | 12 |
| $35 \times 24$ | 14 | 12 | 12 |
| $42 \times 29$ | 12 | 12 | 12 |
| $49 \times 33$ | 10 | 12 | 12 |
| $57 \times 38$ | 10 | 18 | 12 |
| $64 \times 43$ | 8 | 18 | 12 |
| $71 \times 47$ | 12 |  | 12 |

*For soil bearing capacity of 2 tons $/ \mathrm{ft}^{2}$ around corners of pipe

Table 8.4-10 Design Data for CAPA with $3 \times 1 \mathrm{in}$. Corrugations

| Span x Rise (in.) | Minimum Gauge | Minimum Cover <br> (in.) | Maximum Height of <br> Fill*(ft) |
| :---: | :---: | :---: | :---: |
| $60 \times 46$ | 14 | 15 | 20 |
| $66 \times 51$ | 14 | 18 | 20 |
| $73 \times 55$ | 14 | 21 | 18 |
| $81 \times 59$ | 12 | 21 | 16 |
| $87 \times 63$ | 12 | 24 | 16 |
| $95 \times 67$ | 12 | 24 | 15 |
| $103 \times 71$ | 10 | 24 | 16 |
| $112 \times 75$ | 8 | 24 | 15 |

*For soil bearing capacity of 2 tons $/ \mathrm{ft}^{2}$ around corners of pipe

### 8.5 THERMOPLASTIC PIPE

Table $8.5-1$ should be used to determine the maximum height of fill for thermoplastic pipes installed in embankments.
The minimum cover for thermoplastic pipes is as follows: 2.0 ft .
The minimum cover is measured from the top of the pipe to the bottom of the pavement or surface.

The maximum diameter for PEP is 60 inches.
The maximum diameter for PVCP is 36 inches.

Table 8.5-1 Thermoplastic Pipes (Maximum Fill Height (ft) for Sn-90)

| Diameter <br> (inches) | PEP | PVCP |
| :---: | :---: | :---: |
| 12 | 15.5 | 21.5 |
| 15 | 15.0 | 19.5 |
| 18 | 16.0 | 18.0 |
| 21 | 15.5 | 18.5 |
| 24 | 15.5 | 17.5 |
| 30 | 14.0 | 16.5 |
| 36 | 13.5 | 15.5 |
| 42 | 13.0 | $\mathrm{~N} / \mathrm{A}$ |
| 48 | 10.0 | $\mathrm{~N} / \mathrm{A}$ |
| $* 60$ |  | $\mathrm{~N} / \mathrm{A}$ |
| 1 |  |  |

* Fill height for 60 inch PE is not a KDOT calculated value. It is based on information from the Plastic Pipe Institute and a survey of other State DOT's.
Ground Water Table at Spring Line
Based on AASHTO Tables A12-11,12,13 in the AASHTO LRFD Bridge Design Specifications.
Minimum Fill Height $=2.0 \mathrm{ft}$.


### 8.6 REINFORCED CONCRETE BOXES

This section contains general information and procedures for the selection and design of RCB culverts. More detailed information on structural design and details of RCB culverts is presented in the Bridge Design Manual.

Standard drawing sheets for RCB details may be obtained through the Kansas Automated RCB System. Plan detail sheets, quantities and cost estimates and can be generated for one-cell, twocell and three-cell RCB culverts with cell spans from 3.0 ft to 20.0 ft . These quantities and plan detail sheets include wingwalls and aprons.

For gathering comparison information and/or estimating purposes regarding RCB size and design type (fixed or pinned) selection, external designers should log in to the KART System (http:// kart.ksdot.org), open the RCB Form, and enter the required data in the KDOT Standard RCB/RFB Detail Request Application. This procedure replaces the previous RCB request form in PDF format. The request application provides the following benefits:

- It validates the input entered
- It limits requests to available box standards drawings
- It calculates an online quantity/detail/cost summary before submitting to KDOT for creation of a CADD file in Microstation format (dgn), alternative RCB sizes may be run before final details are requested.
- It creates the input file used with the internal windows RCB program for submittal to the appropriate KDOT Section by e-mail.

When RCB size has been selected, external designers may obtain RCB details by submitting a "Standard RCB/RFB Detail Request Application" electronically to the appropriate KDOT unit within the Division of Engineering and Design.

The designer should pay particular attention to the following points:

1. The type of structure (pinned or fixed) should be specified. (See the Bridge Design Manual).
2. The height of fill should be specified. Arbitrarily adding fill height will not necessarily result in a stronger RCB.
3. A pre-cast RCB should be allowed as an option to a cast-in-place box unless conditions preclude its use. If cast-in-place construction is required, this restriction should be stated in the plan notes.
4. A culvert with a total span (as defined in the Bridge Design Manual) longer than 20.0 ft is classified as a bridge. Bridge structures are the responsibility of the State Bridge Office, and should be assigned a bridge serial number and designed in accordance with the requirements in of the Bureau of Structures and Geotechnical Services.
5. A culvert with a total span of 10.0 ft to 20.0 ft is classified as a $10^{\prime}-20^{\prime}$ structure and is assigned a culvert serial number by the KDOT Bridge Management Section. The serial number should be requested prior to final plans.

### 8.7 REFERENCES

American Concrete Pipe Association (2000). Concrete Pipe Design Manual.

American Concrete Pipe Association (1998). Concrete Pipe Handbook.

American Iron and Steel Institute (1994), Handbook of Steel Drainage and Highway Construction Products, 5th edition.

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Howard, A. K. (1977). "Modulus of Soil Reaction Values for Buried Flexible Pipe," Journal of the Geotechnical Division, American Society of Civil Engineers, Vol. 103, No. GT1, pp. 33-42.

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AASHTO, LRFD Bridge Design Specifications, 4th Edition.


[^0]:    *For soil bearing capacity of 2 tons/ft ${ }^{2}$ around corners of pipe

